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**Citation:** Kechagias-Stamatis, O., Aouf, N. & Dubanchet, V. (2020). Evaluating 3D local descriptors and recursive filtering schemes for LIDAR-based uncooperative relative space navigation. Journal of Field Robotics, 37(5), pp. 848-888. doi: 10.1002/rob.21904

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# Evaluating 3D Local Descriptors and Recursive Filtering schemes for LIDAR based Uncooperative Relative Space Navigation

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### Abstract

We propose a Light Detection and Ranging (LIDAR) based relative navigation scheme that is 6 appropriate for uncooperative relative space navigation applications. Our technique combines the 7 encoding power of the 3D local descriptors that are matched exploiting a correspondence grouping 8 scheme, with the robust rigid transformation estimation capability of the proposed adaptive 9 recursive filtering techniques. Trials evaluate several current state-of-the-art 3D local descriptors 10 and recursive filtering techniques on a number of both real and simulated scenarios that involve 11 various space objects including satellites and asteroids. Results demonstrate that the proposed 12 architecture affords a 50% odometry accuracy improvement over current solutions, while also 13 14 affording a low computational burden. From our trials we conclude that HoD-S combined with the adaptive  $\alpha\beta$  filtering poses the most appealing combination for the majority of the scenarios 15 evaluated, as it combines high quality odometry with a low processing burden. 16

### 17 **1. Introduction**

Autonomous ego-motion estimation, i.e. odometry, for space platforms is currently of high interest 18 due to the increasing number of spacecrafts deployed. Specifically, great research interest is in the 19 field of relative space odometry of a *Source* spacecraft platform in relation to a non-cooperative 20 Target platform, i.e. with unknown attitude. The aim of space odometry is to estimate the six 21 Degrees of Freedom (DoF) relative motion between the Source and the Target, with three DoF 22 representing the relative translation and three the relative rotation. Applications utilizing the 23 autonomous relative Source - Target motion estimation involve close-proximity operations where 24 the distance of the two space platforms is such that possible communication loss or delay between 25 the ground station and the *Source* may lead to a *Source – Target* platform impact. Typical distances 26 for close-proximity operations range from a few meters up to tens of meters and depend on the 27 sensors employed, the type of operation and the target size (Fehse, 2003). The need for autonomous 28 navigation extends to a wide range of tasks such as controlled orbiting, docking and close range 29 rendezvous that are required for space missions such as active debris removal (Bonnal, Ruault, & 30 Desjean, 2013; Yılmaz, Aouf, Majewski, Sanchez-Gestido, & Ortega, 2017), celestial body 31 exploration, e.g. comets and asteroids (Cheng, 2002) and on-orbit servicing (Flores-Abad, Ma, 32

**33** Pham, & Ulrich, 2014).

In the context of close-proximity space navigation, the sensors typically used are electro-optical 1 with the majority of current solutions relying on passive sensors using visual or Infrared (thermal) 2 sensing devices in a monocular or stereo camera configuration, or alternatively 3D LIDAR for 3 active systems (Opromolla, Fasano, Rufino, & Grassi, 2017). Indeed, current space relative 4 navigation solutions involve 2D visual data in a monocular (Krämer, Hardt, & Kuhnert, 2018; C. 5 Liu & Hu, 2014) or a stereo camera configuration (Li, Lian, Guo, & Wang, 2013; Maimone, 6 Cheng, & Matthies, 2007; Tykkala & Comport, 2011; Yang Cheng, Maimone, & Matthies, 2006), 7 2D Infrared (IR) data (Yılmaz et al., 2017) and 3D Light Detection and Ranging (LIDAR) data 8 (Galante et al., 2012; Gómez Martínez, Giorgi, & Eissfeller, 2017; Naasz & Moreau, 2012; 9 Opromolla, Di Fraia, Fasano, Rufino, & Grassi, 2017; Opromolla, Fasano, Rufino, & Grassi, 2014, 10 2015a; Sell, Rhodes, Woods, Christian, & Evans, 2014; Song, 2017; Volpe, Palmerini, & Sabatini, 11 2017; Woods & Christian, 2016). For a comprehensive review on spaceborne sensors for 12 spacecraft pose determination the reader is referred to (Opromolla, Fasano, et al., 2017). 13

Utilizing sensors that exploit passive data, i.e. visual or IR, can be an effective solution that is 14 characterized by low hardware complexity, cost and power consumption due to neglecting a 15 transmitting device. Using visual and IR sensors can be an effective solution, however, IR has 16 several advantages over the visual domain such as operating during day and night under several 17 harsh illumination conditions like eclipse and solar glare (Yılmaz et al., 2017). Despite these 18 advantages, the performance of IR odometry depends on the temperature of the Target platform, 19 which is affected by both internal parameters, e.g. heat dissipation of the platform's components, 20 and external parameters, e.g. reflection of sun's radiation. This temperature fluctuation can affect 21 22 the robustness of the IR based local feature detection and matching technique presented in current literature (Yılmaz et al., 2017). On the contrary, 3D LIDAR based odometry outmatches its 2D 23 counterparts (visual and IR) as it operates during day and night, is independent of the Target's 24 25 thermal properties, is capable of revealing the underlying structure of an object (Guo, Sohel, Bennamoun, Lu, & Wan, 2013a), can provide full Target pose estimation (6-DoF), can 26 discriminate the target from the background, is robust in poor visibility conditions and has a greater 27 operating distance compared to the maximum stereo odometry range that poses acceptable 28 accuracy (Opromolla, Fasano, et al., 2017). Despite these advantages, LIDAR sensors and the 29 associated software that exploits the 3D Target information acquired, impose higher hardware 30 requirements compared to the visual and IR sensors that in principle produce 2D data. However, 31 due to the advantages of LIDAR sensors against visual / IR sensors and given that the former have 32 already been placed on space platforms (Kornfeld et al., 2003a), it is clear that LIDAR based 33 navigation is an overall appealing and affordable option. An open case is the processing recourses 34 required for 3D data manipulation. Space platforms use space-graded field programmable gate 35 arrays (FPGA) and recent work (Estébanez Camarena, Feetham, Scannapieco, & Aouf, 2018) 36 demonstrated that it is feasible FPGA boards to perform 2D computer vision based navigation. 37 Hence, there is the potential for FPGA boards to perform complex 3D navigation utilizing LIDAR 38 data. However, the aim of this work is to evaluate the conceptual validity and performance of 39 several 3D local descriptors and recursive filtering schemes rather than suggesting a readily 40 available navigation system. 41

On that basis and driven by the advantages of LIDAR, current literature suggests quite a few
LIDAR based relative navigation solutions (Galante et al., 2012; Gómez Martínez et al., 2017;
Naasz & Moreau, 2012; Opromolla, Di Fraia, et al., 2017; Opromolla et al., 2014, 2015a; Sell et

al., 2014; Song, 2017; Volpe et al., 2017; Woods & Christian, 2016). However, these present a
 number of deficiencies:

a. Registration of the two sequential point clouds current methods mostly relies on the
Iterative Closest Point (ICP) method (Besl & McKay, 1992) that may settle in a local rather than
a global optimum solution.

b. Current algorithms involve an off-line training process that uses a 3D model of the
expected *Target* platform (A. B. Dietrich & McMahon, 2018; A. P. Rhodes, Christian, & Evans,
2017). However, these models are not available for unknown *Targets* such as unexplored comets,
asteroids or space debris, or for known *Target* space platforms that are corrupted with an unknown
level of corruption.

11 c. Current space navigation solutions that rely on computer vision concepts involve 12 regional 3D feature description and not local description (A. Rhodes, Kim, Christian, & Evans, 13 2016; A. P. Rhodes et al., 2017), neglecting the state-of-the-art performance afforded by the latter 14 type. It should be noted that (A. Rhodes et al., 2016) made an attempt using the local feature 15 descriptor Spin Images (Andrew Edie Johnson & Hebert, 1998), however the research concluded 16 that this descriptor is not optimal for space navigation. To the best our knowledge none other local 17 descriptor has been used to date.

d. The majority of current proposals is evaluated on fully simulated scenarios (Gómez Martínez et al., 2017; Opromolla et al., 2014, 2015a; A. P. Rhodes et al., 2017; Song, 2017; Volpe et al., 2017; Woods & Christian, 2016), while only a few algorithms are tested on real but rather simplistic scenarios (Galante et al., 2012; Sell et al., 2014). Recently, orbit determination around small bodies using LIDAR has been proposed (A. B. Dietrich & McMahon, 2018), however this architecture uses a shape model of the *Target* restricting this technique to known *Targets* (deficiency (b) ).

e. Space related odometry literature does not involve any type of feature matching
refinement schemes, such as a correspondence grouping technique (Yang, Xian, Xiao, & Cao,
2018).

In contrast to space robotics odometry, terrestrial odometry (ground and aerial) is more mature 28 spreading over several data domains. A few examples are 2D visual in a monocular or stereo 29 camera configuration (Cvišić, Ćesić, Marković, & Petrović, 2018; Nemra & Aouf, 2009), 2D IR 30 (Mouats, Aouf, Chermak, & Richardson, 2015), fusion of visual with IR data (Mouats, Aouf, 31 Sappa, Aguilera, & Toledo, 2015), fusion of 3D LIDAR with visual data (Graeter, Wilczynski, & 32 Lauer, 2018; Zhang & Singh, 2015b), 3D LIDAR fused with inertial data (Neuhaus, Koß, Kohnen, 33 & Paulus, 2019; Zhang & Singh, 2015a), odometry that solely relies on LIDAR data (Deschaud, 34 2018; Ji et al., 2018) and methods that are based on RGB-D data (Jaimez & Gonzalez-Jimenez, 35 2015; Kim & Kim, 2016; Zhou, Li, & Kneip, 2019). An extensive review on the odometry methods 36 for terrestrial applications is presented in (Agel, Marhaban, Saripan, & Ismail, 2016). 37

38 Simply extending current algorithms designed for terrestrial LIDAR based robotics odometry into

39 the field of space robotics odometry is not an optimum solution for the following reasons:

a. The space environment lacks surrounding objects forcing space odometry to rely
on a limited number of vertices that belong to a single object. Typical terrestrial point cloud scenes
comprise of a few hundreds of thousands of vertices and involve many objects, while a space
odometry scene has at least one order of magnitude fewer vertices and encloses a single object.

b. Space objects are typically less complex than terrestrial scenes further increasing
the already challenging space odometry estimation. The advantage of complex scenes is affording
sufficiently unique and non-degenerated geometries enforcing odometry to converge to acceptable
solutions.

c. Methods that solely use LIDAR data may also not be appealing as these exploit the
hardware properties of terrestrial LIDAR sensors that differ from the spaceborne ones. For
example, the method in (Deschaud, 2018) uses the continuous spinning effect of the LIDAR
sensor, which for spaceborne LIDAR sensors this is not applicable as either scanning or flash
LIDAR sensors are used.

d. Terrestrial odometry that exploits LIDAR data may involve fusing information
from additional sensors such as visual data or inertial data (Graeter et al., 2018; Neuhaus et al.,
2019; Zhang & Singh, 2015b, 2015a). However, a spaceborne sensor suite selection is constrained
by the size, weight and power consumption of each sensor and thus involving two different sensor
types, e.g. LIDAR and visual camera, may not be payload efficient.

Additional challenges preventing directly utilizing algorithms for terrestrial applications on space 19 navigation scenarios are the differences between the earth-based point cloud data and the space-20 based point cloud data, which are linked to the device that they were generated from. Considering 21 point clouds originating from LIDAR, as is the case in this work, the LIDAR earth-based point 22 cloud would be in general denser as its mapping covering area is much focused and smaller than 23 24 the general LIDAR space-based point clouds. However, the later from a farther range would be mapping a large area on orbit to detect the satellite and the satellite sub-part of interest. In terms 25 of noise, the space-based data would be less affected than their earth counterpart since the space 26 LIDAR would have less noisy returns. This is because the background around the target satellite 27 is empty, while on earth applications, i.e. autonomous cars, the background contains several 28 objects. In terms of range accuracy, the space-based point cloud data would be more accurate than 29 30 the earth-based point cloud data.

Spurred by the advantages of 3D LIDAR odometry and the deficiencies of the current solutions for space navigation, we suggest a LIDAR based relative navigation architecture appropriate for space applications. The contributions and innovations of this work can be summarized to:

a. We suggest an odometry architecture that combines the concepts of 3D local feature
 description, feature matching refinement and recursive filtering for the rigid body transformation
 estimation.

b. The recursive filtering process is adaptive and linked to the quality of the matchedfeatures.

c. Opposed to current space-oriented odometry solutions, this architecture does not require
any prior knowledge of the *Target* platform extending significantly the usability of the proposed
solution.

d. We evaluate the suggested technique on seven scenarios that involve one real and four
simulated space objects of various complexity.

e. On each scenario, we evaluate six current 3D local feature descriptors and four recursive
filtering schemes that are tested in all possible combinations.

f. We also evaluate the performance of the proposed architecture against five variations of
 ICP that is widely used for space robotics odometry, and also against two techniques used for
 registration application in the computer vision domain. To the best of our knowledge such an
 extensive evaluation is unique in the space-related odometry literature.

12 It is expected the proposed method to achieve lower odometry errors compared to current ICP 13 based methods, because the feature matching and the geometric correspondence grouping schemes 14 shall provide to the recursive filter only well-established correspondences. These correspondences 15 combined with the adaptive nature infused in the recursive filter affords further improvement and 16 optimization of the odometry performance.

The rest of the paper is organized as follows; Section 2 presents the suggested odometry architecture, while Section 3 compares the accuracy of the proposed pipeline involving several 3D descriptors and recursive filtering combinations against current registration methods on a variety of scenarios. Section 4 analyses the contribution of each module within our architecture, compares our method against a mainstream computer vision-based registration method and also presents the interaction between the number of iterations and the odometry performance for each competitor ICP variant. Finally, Section 5 concludes this paper.

# 24 2. Proposed odometry architecture

### 25 2.1 LIDAR odometry

26 The suggested LIDAR relative navigation architecture considers a two-platform setup, i.e. a

27 Source platform that incorporates a 3D LIDAR sensor and an uncooperative *Target* platform. The 28 aim of the proposed technique is to estimate the relative position of the *Source* platform to the

29 *Target* platform.

Given two sequential point clouds  $P_k = \{p_k^1, ..., p_k^a\}$  and  $P_{k+1} = \{p_{k+1}^1, ..., p_{k+1}^b\}$  of the *Target* that are captured from the LIDAR device placed on the *Source* platform at instance k and k+1, with each

captured from the LIDAR device placed on the *Source* platform at instance k and k+1, with each vertex being in the form  $p_k = (x_k, y_k, z_k)$  and  $p_{k+1} = (x_{k+1}, y_{k+1}, z_{k+1})$ , aim of the odometry process is to

33 calculate a rigid body transformation:

$$R^* = \begin{bmatrix} R & | T \\ 0 & | 1 \end{bmatrix}$$
(1)

35 with *R* the rotation and *T* the translation component that remap point cloud  $P_k$  to  $P_{k+1}$ :

Figure 1: Suggested relative navigation architecture

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Typically,  $R^*$  is estimated by employing a global registration technique such as the ICP, the ICP 9 variants or the Super 4-point Congruent Sets (S4PCS) (Mellado, Aiger, & Mitra, 2014), involving 10

11 
$$P_k$$
 and  $P_{k+1}$ .

#### **Recursive Filtered 3D Local Features based LIDAR odometry** 2.2

12 Driven by the need of a high performing uncooperative relative navigation architecture for relative 13 space navigation, we suggest an architecture that estimates  $R^*$  by combining the concepts of 3D 14 local feature description, geometrical correspondence refinement and adaptive recursive filtering. 15 For the former, we evaluate several current state-of-the-art 3D local feature descriptors (Section 16 2.2.1) while for the latter we evaluate both linear and non-linear filters (Section 2.2.3). The 17 suggested architecture is presented in Figure 1. It is worth noting that current odometry literature 18 for terrestrial applications suggests global pose-graph optimization, i.e. finding feature matches 19 between non-adjacent frames or exploiting the loop closure technique. Despite that, in this work 20 21 we do not adopt these concepts and push the limits by investigating the performance attained by exploiting only sequential point clouds. Preliminary work is presented in (Kechagias-stamatis & 22 Aouf 2019) without though involving in that work any geometric consistency checks and limiting 23 24

*Target* platform is given by:

$$R_u^* = \prod_{\mu=1}^u R_\mu^*$$

$$R_{\mu}^{*} = \prod_{i=1}^{n} R_{\mu}^{*} \tag{4}$$

Then at instance *u*, the position of the *Source* moving platform relatively to the uncooperative

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(2) $p_{k+1} = Rp_k + T$  $\begin{bmatrix} x_{k+1} \\ y_{k+1} \\ z_{k+1} \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \begin{bmatrix} x_k \\ y_k \\ z_k \end{bmatrix} + \begin{bmatrix} T_x \\ T_y \\ T_z \end{bmatrix}$ 

(3)

# 2 2.2.1 3D local feature description

- 3 Local feature description techniques describe local patches around a point of interest, i.e. keypoint,
- 4 by encoding the geometric properties and the underlying structure of the local patch (O. Kechagias-
- Stamatis et al., 2018). Their major advantages are affording robust feature description to partially
  visible objects (Odysseas Kechagias-Stamatis, Aouf, & Nam, 2017) and being less affected by
- visible objects (Odysseas Kechagias-Stamatis, Aouf, & Nam, 2017) and being less affected by
  illumination variation and pose changes (Lei Yunqi, Lai Haibin, & Jiang Xutuan, 2010; Mian,
- 8 Bennamoun, & Owens, 2006).
- 9 Current literature suggests quite a few handcrafted 3D local descriptors with representative ones
- 10 being the Signatures of Histograms of Orientations (SHOT) (Salti, Tombari, & Di Stefano, 2014),
- 11 Spin Images (Andrew E. Johnson & Hebert, 1999), Rotational Projection Statistics (RoPS) (Guo
- 12 et al., 2013a), Tri-Spin Images (TriSI) (Guo, Sohel, Bennamoun, Lu, & Wan, 2013b), Fast Point
- 13 Feature Histograms (FPFH) (Rusu, Blodow, & Beetz, 2009), 3D Shape Context (3DSC) (Frome,
- Huber, Kolluri, Bülow, & Malik, 2004), Unique Shape Context (USC) (Tombari, Salti, & Di
   Stefano, 2010), Histogram of Distances (HoD) (Odysseas Kechagias-Stamatis & Aouf, 2016),
- HoD-Short (HoD-S) (Odysseas Kechagias-Stanatis & Aouf, 2010),
   HoD-Short (HoD-S) (Odysseas Kechagias-Stanatis & Aouf, 2017, 2018), Local Feature Statistics
- 17 Histogram (LFSH) (Yang, Cao, & Zhang, 2016), Multi-attribute Statistics Histograms (MaSH)
- 18 (Yang, Zhang, & Cao, 2017), Statistic of Deviation Angles on Subdivided Space (SDASS) (Zhao,
- 19 Le, & Xi, 2019) and Binary Rotational Projection Histogram (BRoPH) (Zou et al., 2018). It is
- worth noting that lately except from handcrafted local feature descriptors, learned 3D feature
  descriptors have also been used. Examples are the Point Pair Feature Network (Deng, Birdal, &
- 22 Ilic, 2018) and the Compact Geometric Features descriptor (Khoury, Zhou, & Koltun, 2017). A
- downside of both methods is the requirement of offline training prohibiting their usage for
- 24 odometry that involves an uncooperative and unknown *Target* platform.
- In this work we use within our odometry architecture several commonly used 3D feature descriptors and specifically SHOT, TriSI, HoD-S, HoD, FPFH and RoPS. A common principle of all these 3D descriptors is encoding a spherical volume V of radius r that is centered on a keypoint p(x,y,z). For completeness, a short description of the 3D descriptors evaluated is presented.

# 29 **2.2.1.1 HoD and HoD-S**

HoD and HoD-S calculate the probability mass density of the normalized point-pair L2-norm 30 distance distributions within V. The difference between these two 3D descriptors is that HoD 31 32 encodes the distance distributions in a coarse and a fine manner, while HoD-S only in a coarse manner. Main advantages of both these descriptors over the current ones are neglecting the 33 requirement of a Local Reference Frame or Axis (LRF/A), being robust to nuisance factors such 34 as noise and being fast to compute. Indeed, HoD and HoD-S are robust to Gaussian noise, 35 occlusion, clutter and point cloud resolution variation (Odysseas Kechagias-Stamatis & Aouf, 36 37 2016, 2017, 2018; Odysseas Kechagias-Stamatis et al., 2017).

# 38 2.2.1.2 SHOT

SHOT divides the support volume *V* into a pre-defined number of sub-volumes along the azimuth, the elevation and the radius. For each sub-volume, a 1D histogram is calculated based on the normal variation between the keypoint p(x, y, z) (including its surrounding vertices) and the vertices 1 that lie in each sub-volume. SHOT is robust to Gaussian noise and Shot noise, and sensitive to

2 occlusion and clutter (Guo et al., 2016).

# 3 2.2.1.3 FPFH

FPFH establishes on V a *Darboux* LRF. Then for each point belonging to V, FPFH encodes the angular relationship between the keypoint p(x,y,z) and its neighbors as provided by the LRF. Finally, this angular relationship is transformed into a histogram. FPFH is robust to resolution

7 variation and sensitive to Gaussian noise, Shot noise, occlusion and clutter (Guo et al., 2016).

# 8 2.2.1.4 RoPS

9 RoPS establishes on V a LRF. Then V is rotated around each axis of the LRF and is projected on
10 each of the coordinate planes. Finally, each projection undergoes a statistical analysis based on
11 low order moments and entropy, and all the results are concatenated into a histogram. RoPS is

12 robust to Gaussian noise and sensitive to Shot noise, occlusion and clutter (Guo et al., 2016).

# 13 2.2.1.5 TriSI

TriSI is an extension of the 3D descriptor Spin Images (SI). For the latter, given a support volume 14 V centered at point p(x,y,z), a LRA is aligned with the normal vector of the plane fitted to the 15 vertices within V. Then a 2D array accumulator of user defined dimensions is placed on the LRA 16 and the SI descriptor is generated by accumulating the neighboring points into each bin of the 2D 17 array as the array rotates around the LRA. TriSI uses the same technique as the SI but substitutes 18 the LRA with an LRF and calculates a SI descriptor for each axis of the reference frame. Finally, 19 the three SI descriptors are concatenated to from a single descriptor. TriSI is robust to Gaussian 20 noise, Shot noise and resolution variation, while it is sensitive to occlusion and clutter (Guo et al., 21 22 2016).

# 23 2.2.2 Local feature matching

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Let  $F_k = \{f_k^1, ..., f_k^{N_i}\}$  and  $F_{k+1} = \{f_{k+1}^1, ..., f_{k+1}^{N_j}\}$  be two sets of 3D features for point clouds  $P_k$  and  $P_{k+1}$  respectively that are the output of a 3D descriptor. We match feature  $f_k^i$  from  $F_k$  with its nearest feature  $f_{k+1}^j$  from  $F_{k+1}$  based on an L2-norm Nearest Neighbor metric (Mikolajczyk & Schmid, 2005):

$$f_k^i \triangleq f_{k+1}^j \longleftarrow \arg\min_{n=1,2,\dots,N_j} \left( \left\| f_k^i - f_{k+1}^j \right\|_2 \right) < \tau$$

$$(5)$$

29 where i, j are the feature indexes and the threshold  $\tau$  is set to 1 to reduce the dependency between the threshold value and the metric used (O. Kechagias-Stamatis et al., 2018). We speedup the 30 feature correspondence process of Eq. (5) by employing the Fast Library for Approximate Nearest 31 Neighbors (FLANN) technique (Muja & Lowe, 2009). FLANN is a widely used library that 32 performs fast approximate nearest neighbor searches in high dimensional spaces. It uses either a 33 hierarchical k-means tree search with a priority search order scheme, or a multiple randomized kd-34 trees scheme. The search scheme and the optimum FLANN parameters are automatically chosen 35 from the FLANN library and depend on the dataset. 36

1 Feature matching is then performed by using geometric consistency checks (GCC) (Chen &

2 Bhanu, 2007). Specifically, the correspondences obtained from FLANN (Eq. (5)) are clustered into

3 hypotheses, using their true physical geometric consistency. Geometric consistency aims at

4 reducing mismatches by grouping correspondences into clusters that are geometrically consistent.

5 For the latter, a list of descriptor correspondences is created  $H_u = \{p_k^u, p_{k+1}^u\}$ , where  $p_k^u$  and  $p_{k+1}^u$ 

6 are the *Target* correspondences at instance k and k+1 from the FLANN matching stage (Eq. (5)):

7

$$H_{u} = \left\{ p_{k}^{u}, p_{k+1}^{u} \right\} \longleftarrow f_{k}^{i} \triangleq f_{k+1}^{j}$$

$$\tag{6}$$

8 Given a seed correspondence from  $H_u$ , the first cluster is initialized and all correspondences 9  $H_v = \{p_k^m, p_{k+1}^m\}, v \le u$  not yet grouped that are geometrically consistent with the cluster are added 10 to it. The consistency check for a pair of correspondences  $H_u$ ,  $H_v$  is valid if the following distance 11 relation holds:

$$\left\| p_{k}^{u} - p_{k}^{m} \right\|_{2} - \left\| p_{k+1}^{u} - p_{k+1}^{m} \right\|_{2} \right| < \varepsilon$$
(7)

13  $\varepsilon$  being the threshold tolerance for their consensus set that is experimentally set during tuning. 14 Finally, the matched feature pairs  $\{f_k^i, f_{k+1}^j\}$  belonging to the cluster with the largest cardinality 15 are considered as feature matches, while their associated vertices  $\Omega = \{p_k^i, p_{k+1}^j\}$  are considered as

16 point correspondences.

It is worth noting that we use a GCC module instead of the popular Random Sample and Consensus
(RANSAC) (Fischler & Bolles, 1981) because the latter has a longer execution time than GCC,
which can be up to two orders of magnitude (Yang et al., 2018) and thus is inappropriate for
odometry applications examined in this work. For completeness, in Section 4 we demonstrate the
efficiency of GCC by substituting in the proposed odometry method the GCC module with
RANSAC.

### 23 2.2.3 Recursive filtering

The aim of the recursive filtering is to remove the noise from a signal while retaining useful 24 information. Hence, in the context of odometry, given the correspondences  $\Omega$  we solve Eq. (2) by 25 suggesting an adaptive recursive filtering scheme based on the quality of the correspondences  $\Omega$ . 26 The proposed architecture is based on a recursive optimal state estimation of the state variable 27  $x_k = [r_{11} r_{12} r_{13} r_{21} r_{22} r_{23} r_{31} r_{32} r_{33} t_x t_y t_z]^T$  that encompasses the rigid transformation between  $P_k$ 28 and  $P_{k+1}$  by exploiting the correspondences  $\Omega$ . For our trials, we consider an initialization value 29 for  $x_k = [1 \ 0 \ 0 \ 1 \ 0 \ 0 \ 1 \ 0 \ 0 \ 0]^T$ . It should be noted that in contrast to our solution, (A. P. Rhodes 30 et al., 2017) uses a Multiplicative Extended Kalman Filter (MEKF) to smooth R\* rather than 31 estimating  $R^*$  as done in this work. The adaptive recursive filters evaluated in this paper are: 32

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#### 1 2.2.3.1 Adaptive $H\infty$ Filter

2 The  $H\infty$  filter is a recursive optimal state estimator with  $x_k$  the state variable vector and 3  $\psi_k = [x^k, y^k, z^k]^T$  the measurement vector that contains the 3D coordinates of the point 4 correspondences  $p_{k+1}^j$  belonging to  $P_{k+1}$ , which are included in  $\Omega$ . The adaptive  $H\infty$  filter is given 5 by:

$$x_k = \Phi \ x_{k-1} + w_{k-1} \tag{8}$$

6

 $\psi_k = H_k x_k + v_k \tag{9}$ 

8 where  $\Phi$  is the state transition matrix and *H* the measurement model matrix. We set 9  $\Phi = R_0^* = [I | T_0]$  with *I* the identity matrix and  $T_0 = [0 \ 0 \ 0]^T$ , *w* and *v* are the model and the 10 measurement noise factors respectively with covariance matrices  $W \sim N(0, \sigma_w^2 J_{12})$  and 11  $V \sim N(0, M \sigma_v^2 J_3)$  where  $\sigma_w$  and  $\sigma_v$  are small positive values and *J* is the unity matrix.  $H_k$ 12 contains the actual measured 3D coordinates of  $p_k^i$  belonging to  $P_k$  that are included in  $\Omega$ :

13 
$$H_{k} = M \begin{bmatrix} x_{k+1} & y_{k+1} & z_{k+1} & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & x_{k+1} & y_{k+1} & z_{k+1} & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & x_{k+1} & y_{k+1} & z_{k+1} & 0 & 0 & 1 \end{bmatrix}$$
(10)

with *M* an adaptive coefficient that aims at adjusting the measurement noise covariance based on the quality of the matched features  $\{f_k^i, f_{k+1}^j\}$  defined as:

16

$$M = 10 \cdot \sum \left( \left| f_k^i - f_{k+1}^j \right| \right)$$
(11)

17 In contrast to the typical  $H\infty$  filter (Simon, 2000), in this work we suggest an adaptive measurement 18 model matrix  $H_k$ . The constant in Eq. (11) is experimentally estimated to fine tune the overall filter 19 performance. The problem that the  $H\infty$  filter is trying to solve is the min<sub> $\hat{x}$ </sub> max<sub>w,v</sub> *G* where G is 20 defined as:

21 
$$G = \frac{average(\|x_k - \hat{x}_k\|)_Q}{average(\|w_k\|)_W + average(\|v_k\|)_V}$$
(12)

subject to 
$$G < 1/\gamma$$
, with Q being a weighting matrix and  $\gamma$  a small constant number representing  
the required accuracy of the filter. The  $H\infty$  filter equations solving Eq. (12) are:

24 
$$L_{k} = \left(I - gQP_{k-1} + H_{k}^{T}V^{-1}H_{k}P_{k-1}\right)^{-1}$$
(13)

25 
$$K_k = \Phi P_{k-1} L_k H_k^T V^{-1}$$
 (14)

$$P_k = \Phi P_{k-1} L_k \Phi^T + W \tag{15}$$

$$\hat{x}_{k+1} = \Phi \hat{x}_k + K_k \left( \psi_k - H \hat{x}_k \right)$$
(16)

where Q = Idt with  $dt = 10^{-5}$  and g = 0.1 being regulating parameters. The number of iterations of the  $H\infty$  filter is the cardinality of  $\Omega$  and ultimately the final  $\hat{x}$  after all iterations is transformed into  $R^*$ , which is input to Eq. (4) in order to estimate the LIDAR odometry. The parameters of the adaptive  $H\infty$  filter as well as of the rest adaptive filters evaluated in this work are tuned based on

7 scenario 1.

### 8 2.2.3.2 Adaptive *Kalman* Filter

9 Using the same notation as for the  $H\infty$  filter, the *Kalman* filter is given by (Simon, 2001):

10 
$$x_k = \Phi x_{k-1} + Bq_k + w_{k-1}$$
 (17)

$$\psi_k = H_k x_k + v_k \tag{18}$$

12 with *B* a matrix and *q* a known input to the system. The *Kalman* filter equations are:

13 
$$K_{k} = AP_{k}H_{k}^{T} \left(H_{k}P_{k}H_{k}^{T} + VM\right)^{-1}$$
(19)

14 
$$\hat{x}_{k+1} = \left(\Phi \hat{x}_k + Bu_k\right) + K_k \left(\psi_k - H_k \hat{x}_k\right)$$
(20)

15 
$$P_k = \Phi P_{k-1} \Phi^T + W - \Phi P_k H_k^T V^{-1} H_k P_k \Phi^T$$
(21)

where *K* is the Kalman gain and *P* the estimation error covariance, with  $\sigma_v = 1$  and  $\sigma_w = 5 \cdot 10^{-3}$ that are experimentally defined to gain optimum odometry performance.

#### 18 **2.2.3.3** Adaptive $\alpha\beta$ Filter

19 Using the same notation as for the  $H\infty$  filter, the  $\alpha\beta$  filter is given by (Penoyer, 1993):

$$x_k = x_{k-1} + V_k \Delta t \tag{22}$$

21 
$$r_k = x_{k-1} - x_k$$
 (23)

$$x_k = x_k + \alpha r_k \tag{24}$$

23 
$$V_k = V_k - \frac{\beta}{\Delta t} x_k$$
(25)

24 where  $r_k$  is the residual error,  $V_k = 1$ ,  $\Delta t = 10^{-5}$ ,  $\alpha = 10^{-6}$  and  $\beta = M$  as computed by Eq. (11).

# 2.2.3.4 Adaptive State-Dependent Riccati Equation (SDRE) Filter

2 This is a non-linear filter (Arnold & Laub, 1984) that solves the equation:

$$A^{T}XA - X - A^{T}XB(B^{T}XB + R)^{-1}B^{T}XA = 0$$
(26)

4 where  $A = Q = I \cdot \sigma_w$  and B = IM.

5

3

# 6 3. Experiments

### 7 3.1 Experimental setup

8 We evaluate the proposed architecture for LIDAR based uncooperative relative navigation on 9 seven scenarios that consider as the *Target* platform one real space platform mock-up and four 10 simulated space objects. We assume that the *Target* is not rotating in any significant way and the 11 reference frame where odometry is searched for is fixed on the *Source* and rotating with it. 12 However, for the scenarios involving real data, the Source platform has a minor tumbling during 13 data acquisition.

The first two scenarios consider a moving *Source* platform that utilizes a VLP-16 Velodyne Puck 14 Lite LIDAR to capture the point cloud of a scaled EnviSat mock-up Target. The ground truth of 15 the Source is estimated by capturing its position via an Optitrack device ("Optitrack," 2018). 16 Optitrack can provide in sub-millimeter accuracy the position of objects that are within its field of 17 view and are visible in the Near Infrared (NIR) band. Therefore, we placed on the VLP-16 highly 18 NIR reflective markers. The real data scenarios involve a straightforward – backward trajectory 19 (*Real-FB*) and a highly curved forward – backward trajectory (*Real-Curved*). Both scenarios are 20 challenging as they involve real point clouds and are presented in Figure 2 along with the point 21 cloud cardinality per frame. 22

Main characteristics of these scenarios are the poor features on the *Target* point cloud that is mostly presented by flat surfaces. This is because the original Envisat, and thus our scaled mock-up, comprises of flat surfaces, on top of which several antennas are placed. The mock-up is acquired by the 16 vertical beams of the VLP-16, constraining the vertical vertex cardinality to 16 vertices per acquisition instance neglecting the fine details of the mock-up. However, this situation can be considered as a simulation of a low-resolution point cloud that is acquired by a space graded LIDAR sensor at greater distances or by a low-cost low-resolution space-graded LIDAR device.

It is worth noting that the VLP-16 we used in our trials is not an optimum choice for spaceborne 30 platforms mainly due the 360° horizontal field of view (FoV), the 16 vertical beams limiting the 31 *Target* details per sweep in the vertical axis, and finally, due to the relatively short operating range 32 compared to the majority of currently available space graded LIDAR sensors. Table 1 compares a 33 number of space graded LIDAR sensors against the VLP-16 we use in our trials. From Table 1 it 34 35 is obvious that for a short operating distance, the accuracy provided by space graded LIDAR sensors is higher compared to the commercial VLP-16. However, we believe that using the VLP-36 16 to acquire real data is both valid and valuable for the following reasons: First, we evaluate the 37 38 performance of our architecture against the competitor odometry methods on real data that contain

arbitrary minor Source tumbling. Second, we limit the 360° horizontal FoV by post processing the 1 point cloud acquired and discard vertices that do not belong to the Target. Third, the low point 2

cloud resolution may resemble a scenario of a space graded LIDAR at a great distance or utilizing

3 a low-cost low-resolution sensor. Overall and given that e VLP-16 poses a decent cost-effective 4

alternative to validate space navigation algorithms that has already been used by the relevant 5

community (Opromolla, Di Fraia, et al., 2017), we believe that the quality of the acquired point 6

- clouds is sufficient for conceptual verification of the proposed architecture. 7
- 8

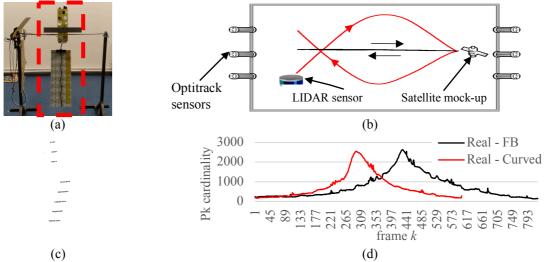


Figure 2: Real -FB and Real-Curved scenarios (a) Scaled EnviSat satellite mock-up (b) top view of the acquisition setup and the trajectory plots of the LIDAR sensor, i.e. Source, moving along the black trajectory for the Real-FB and the red trajectory for the *Real-Curved* scenarios, (c)  $P_k$  point cloud example (d)  $P_k$  cardinality per frame k (colored arrows indicate the corresponding trajectory direction)

9

10 The simulation and the test data used in this paper present a few differences, without causing loss in performance, to the real space scenarios in terms of the LIDAR sensor characteristics used and 11 in terms of the operation range. The LIDAR sensor technology envisaged/ used in space (NEPTEC, 12 Jena-Optronik used on ESA programs) are denser, more accurate comparing to the technology 13 used to generate our data in this paper. In space the close-range operation for this relative 14 navigation problem could be from 100m down to 2m close to the target and the LIDAR technology 15 mentioned above and used in space would cover up well to that range. All the experiments for 16 relative navigation available in the literature are of similar range (few meters) as we proposed in 17 our simulation and real data. The accuracy achieved by our algorithm in our tests is optimal and 18 we strongly believe that it would be kept similar if we went for real space scenarios as in this case 19 the sensor would be of better quality (range of operation, accuracy although with less or similar 20 density as our LIDAR system we used in our experiment is not of great quality in terms of density) 21 22 and the noise is much less than that of our experimental data since in space the background is quite obscure and no noisy returns are expected comparing to our lab testbed. 23

24

Table 1: Comparison of existing space-graded LIDAR sensors and VLP-16

| Sensor   | FoV<br>(H x V) <sup>1</sup> | Points              | Maximum<br>Range (m) | acquisition<br>mode                         | refresh rate<br>(Hz) | range<br>accuracy at<br>max range<br>(cm) | angular<br>resolution<br>(rad)                   | power (W) | weight<br>(kg) |
|--|-----------------------------|---------------------|----------------------|---|----------------------|---|--|-----------|----------------|
| LAMP<br>(Kornfeld et al.,<br>2003b; Liebe et<br>al., 2003) | 10°x10°                     | n/a                 | 2500                 | scanning<br>beam                            | 10,000               | ≤ 2.6                                     | 10-3   | 33        | 6.4            |
| RVS-3000<br>(Jena Optronik,<br>2019)                       | 40°x40°                     | n/a                 | 100                  | scanning<br>beam                            | 1-4                  | n/a                                       | n/a  | 50        | 8              |
| DragonEye<br>(ASC, 2019a)                                  | 45°x45°                     | 32,768              | 1500                 | flash LIDAR                                 | 5-30                 | 15  | n/a  | 35        | 3              |
| GoldenEye<br>(ASC, 2019b)                                  | 45°x45°                     | 32,768              | 3000                 | flash LIDAR                                 | 5-10                 | 10  | n/a  | 50        | 6.5            |
| VLP-16   | 360°x30°                    | 37,500 <sup>2</sup> | 100                  | 16 vertical<br>laser beams<br>spinning 360° | 5-20                 | ≤ 3                                       | H: ≤7x10 <sup>-3</sup><br>V:35 x10 <sup>-3</sup> | 8         | 0.59           |

2 Scenario three studies the odometry performance of a simulated Ellipse of Inspection (Sim-EoI) trajectory of the Source platform around the Target. The latter space platform is developed by 3 4 Thales Alenia Space (France) and is inspired from the Globalstar-2 and Iridium constellations. The 5 *Sim-EoI* trajectory is a realistic space-oriented scenario that considers the influence of the Earth's mass, the Sun's sunlight power with respect to each spectral band and the typical physical size of 6 the Target and the Source platform. In the Sim-EoI trajectory the Source platform performs a 7 complete translational motion along the ellipsoid. Figure 3 presents the satellite model, the Sim-8 *EoI* trajectory and the point cloud cardinality per frame. 9

Scenario four named *Sim-Helical* is presented in Figure 4 and simulates a 3D helical trajectory of the *Source* platform that is approaching the Thales Alenia Space model acting as the *Target*. We create self-occluded point cloud views of the *Target* platform emulating realistic views of the virtual LIDAR placed on the *Source* platform by exploiting the Hidden Point Removal (HPR) algorithm (Katz, Tal, & Basri, 2007). The challenge in this scenario is the sparse  $P_k$  and complex trajectory as we want to push the limits of 3D space odometry and investigate the performance of the suggested pipeline.

The following scenarios five to seven simulate the *Source* platform orbiting around the *Target*platform in an Ellipsoidal trajectory. Compared to the *Sim-EoI* trajectory, here the *Source* platform
performs 2.5 times a complete translation along the ellipsoid aiming at evaluating the performance
of the competitor methods on repetitive trajectories. Additionally, in scenarios five to seven
consider as the *Target* platform the *Voyager* satellite, the *Orion* space capsule and the *Bennu*

22 asteroid respectively. Computer Aided Design (CAD) models for all three space objects are

obtained from (NASA, 2019), while the corresponding point clouds are created by applying the

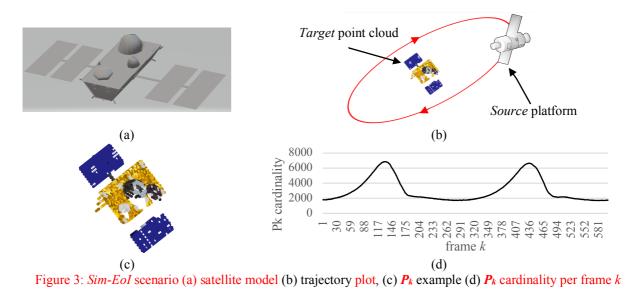
<sup>&</sup>lt;sup>1</sup> Nomenclature: H stands for Horizontal, V for Vertical and n/a for not available

<sup>&</sup>lt;sup>2</sup> In the single return mode VLP-16 generates approx. 300,000 points per second for a 360° x 30° FoV. For comparison reasons, for a hypothetical 45° x 30° FoV the points per second generated by VLP 16 would be 37 500

<sup>45°</sup> x 30° FoV the points per second generated by VLP-16 would be 37,500

code of (Aldomà, 2011) with 800 views. Finally, similarly to scenario four, we use the HPR 1 algorithm to create self-occluded point cloud views of the Target platform. The challenge in 2 scenarios five to seven is multi-fold. First, opposing to the large size of the simulated Envisat 3 Target platform evaluated in scenario three, the Voyager and the Orion space platforms are smaller 4 providing a smaller point cloud cardinality. Second, Bennu, lacks distinctive features making the 5 6 evaluation of the local feature descriptors evaluated quite challenging. Third, the Orion and Bennu point clouds are quite sparse. It should be noted that we intentionally tuned HPR to create sparse 7 point clouds as we want to investigate the performance of the suggested pipeline in low resolution 8 9 conditions simulating large *Source – Target* distances, which is the norm as the *Source* approaches 10 the *Target*, or alternatively we simulate exploiting a low-cost low-resolution LIDAR sensor. The simulated scenarios five to seven namely the Sim-Voyager, Sim-Orion and Sim-Bennu are 11

12 presented in Figure 5.



13

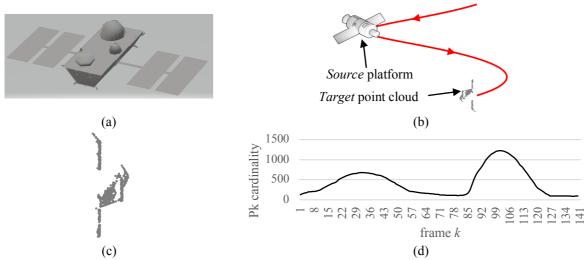


Figure 4: *Sim-Helical* scenario (a) satellite model (b) trajectory plot, (c)  $P_k$  example based on HPR simulation (d)  $P_k$  cardinality per frame k

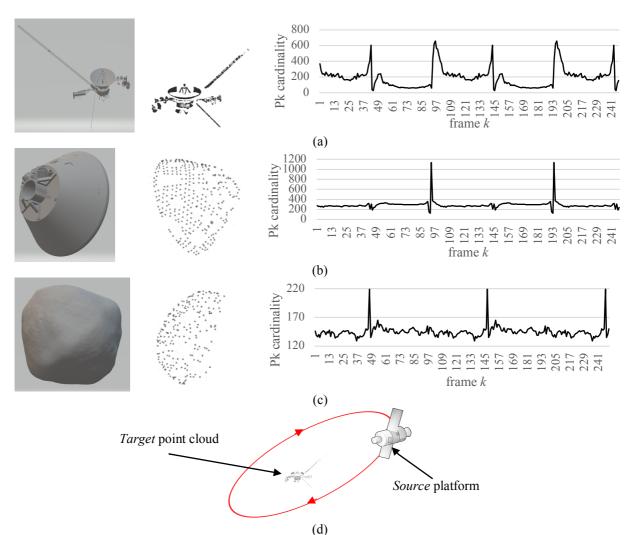


Figure 5: Simulated scenarios presenting the space object model,  $P_k$  based on HPR simulation and  $P_k$  cardinality per frame k respectively for the (a) Sim-Voyager scenario, (b) Sim-Orion scenario and (c) Sim-Bennu scenario, along with the generic Ellipsoidal trajectory of all three scenarios is presented in (d). For better readability we visualize in (d) only the Voyager model.

2 It should be noted that the CAD models we use to generate the *Target* point clouds are accurate,

3 but the point clouds created are not ideal. This is because the method of (Aldomà, 2011) we use to

4 generate the point clouds from CAD models and the HPR algorithm we employ to generate

5 viewing dependent point clouds, affect the point cloud accuracy during reconstruction.

6 The differences between the real and the simulated *Target* point clouds of our trials can be summarized as follows. First, the vertical cardinality of the real LIDAR data is fixed to 16 vertices, 7 while for the synthetic there is not such a constraint. Second, the level of details of the real data is 8 lower compared to the simulated. Third, real data during acquisition involve minor Source 9 tumbling. Fourth, due to the real data acquisition setup, i.e. high LIDAR refresh rate and slow-10 moving *Source* platform, the inter-motion between  $P_k$  and  $P_{k+1}$  is lower compared to the simulated 11 data where the fictitious dynamics of the Source and Target platforms are greater. However, 12 despite these differences, both scenario classes are useful for evaluation. Except from these 13

14 differences, both real and simulated data are sparse aiming at simulating large Source - Target

distances or spaceborne LIDAR sensors that are less expensive and less accurate. Despite these
 differences, we believe that in the context of conceptual validation of our odometry method and in
 terms of comparing its performance against current solutions, both data modalities are acceptable.

Figure 6 shows the ground truth trajectory of each scenario along with the most accurate trajectory 4 obtained by the proposed method, i.e. best performing feature description and filtering 5 combination. In our trials we describe all vertices belonging to each point cloud  $P_k$  and  $P_{k+1}$  with 6 the 3D descriptors introduced in Section 2.2.1. The proposed pipeline is in MATLAB while 7 descriptors are implemented either in MATLAB or in C++/PCL using a MEX wrapper. The 8 parameters of each descriptor are fixed either to the ones originally proposed by their authors or to 9 their PCL implementation (Alexandre, 2012; Guo et al., 2016; Odysseas Kechagias-Stamatis & 10 Aouf, 2016). An exception is the support radius r that we tune individually for each descriptor 11 12 during the Real-FB scenario.

13

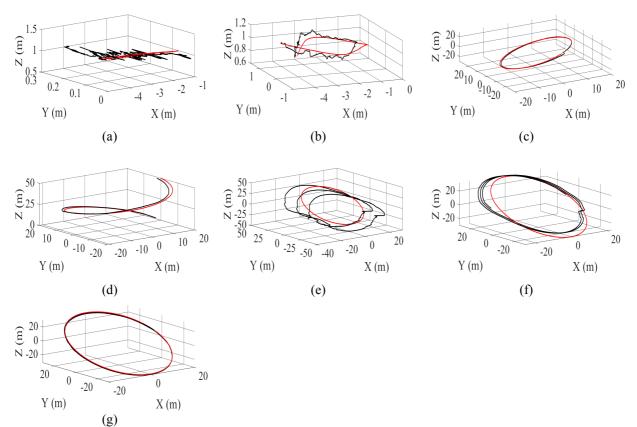


Figure 6: Ground truth trajectories (in red) along with the top performing method (in black) per the scenario (a) *Real – FB* scenario with HoD-S/  $\alpha\beta$  (b) *Real – Curved* scenario with HoD-S/  $\alpha\beta$  (c) *Sim – EoI* scenario with HoD-S/  $\alpha\beta$  (d) *Sim-Helical* scenario with HoD-S/  $\alpha\beta$  (e) *Sim – Voyager* scenario with HoD-S/ *SDRE* (f) *Sim – Orion* scenario with SHOT/ *Kalman* (g) *Sim – Bennu* scenario with HoD-S/  $\alpha\beta$ . The *Real-FB* scenario considers a forward – backward motion, while the *Sim – Voyager*, *Sim – Orion* scenario and *Sim – Bennu* scenarios involve 2.5 times a complete motion translation along the elliptical trajectory.

Indeed, we use the *Real-FB* scenario 1 not only to evaluate the odometry performance of each 1 method but also to tune the free parameters of every module of the proposed architecture and the 2 parameters of the competitor methods presented shortly. Regarding the proposed method, we tune 3 the encoding radius r of each descriptor, the geometric consistency threshold tolerance  $\varepsilon$  of eq. (7) 4 and the regulating parameters of each adaptive filtering scheme. Tuning is performed via a try and 5 evaluation scheme aiming to achieve the lowest possible translational and rotational error and also 6 the lowest possible processing time. It should be noted that during tuning, odometry accuracy and 7 computational burden are of equal importance. Regarding the sensitivity of each method to these 8

9 parameters:

a. Encoding radius: We confirm that SHOT is fairly stable and is less affected by the encoding 10 radius, while TriSI, FPFH and RoPS gain a peak performance and then drop (Guo et al., 2016, 11 2015). During tuning, we identified this peak performance at  $20 \times Tr$ , with Tr the average  $P_{k+1}$ 12 resolution. Regarding HoD and HoD-S, as the encoding radius increases these tend to increase 13 their encoding capability and provide more distinctive features. However, regardless of the 14 descriptor, as the encoding radius increases the processing time to compute the descriptor increases 15 exponentially (Guo et al., 2016). Thus, the encoding radius of HoD and HoD-S is set to  $80 \times Tr$  to 16 balance odometry performance with computational burden. Table 2 presents the parameters of 17 each descriptor evaluated in this work along with the main traits per method. It is worth noting that 18 even though USC and 3DSC are widely used, our initial results during the tuning process of each 19 descriptor showed that both failed to provide valid correspondences due to the highly sparse Target 20 point cloud where USC and 3DSC are quite sensitive confirming (Guo et al., 2016). 21

| 2 | h |
|---|---|
| Z | Z |

| Descriptor | Descriptor<br>Length | radius $r$ of volume $V$ | Implement<br>ation<br>platform | Operating<br>principle   | Robustness   | Sensitivity  |
|------------|----------------------|--------------------------|--------------------------------|--|--|--|
| SHOT       | 352                  | $20 \times Tr$           | C++<br>(MEX wrapper)           | Angular variations   | Gaussian noise, Shot<br>noise                          | occlusion, clutter                                   |
| TriSI      | 675                  | $20 \times Tr$           | MATLAB                         | Accumulating points  | Gaussian noise, Shot<br>noise, resolution<br>variation | occlusion, clutter                                   |
| HoD-S      | 40                   | $80 \times Tr$           | MATLAB                         | L <sub>2</sub> -norm distances with<br>coarse encoding             | Gaussian noise, Shot<br>noise, resolution<br>variation | occlusion, clutter                                   |
| HoD        | 240                  | $80 \times Tr$           | MATLAB                         | L <sub>2</sub> -norm distances with<br>coarse and fine<br>encoding | Gaussian noise, Shot<br>noise, resolution<br>variation | occlusion, clutter                                   |
| FPFH       | 33                   | $20 \times Tr$           | C++<br>(MEX wrapper)           | Angular variations   | resolution variation                                   | Gaussian noise,<br>Shot noise,<br>occlusion, clutter |
| RoPS       | 135                  | $20 \times Tr$           | MATLAB                         | Low order statistics   | Gaussian noise   | Shot noise,<br>occlusion, clutter                    |

b. Geometric consistency threshold: This defines how strict the geometric point-pair distance comparisons are (eq. (7)). The threshold dependents on the encoding quality of the 3D descriptor and on the characteristics of the  $P_k$  such as being sparse. Hence, to increase the robustness of our method to sparse *Target* point clouds and to potential feature description mismatches, we use an adaptive threshold that is set to  $2 \times Tr$ , with Tr the average  $P_{k+1}$  resolution. Due to its adaptive nature, the sensitivity of the geometric consistency threshold is relatively low.

c. Adaptive filtering regulating parameters: These define for each iteration how much the
measurements, i.e. the feature correspondence coordinates for our odometry architecture, affect
the prediction step, i.e. the updated *R*\*. These require to be finely tuned as the output of the filter
is quite sensitive to these parameters. Tuning is performed based on the *Real-FB* scenario.

Opposing to current literature (Opromolla et al., 2014, 2015a; Opromolla, Fasano, Rufino, & Grassi, 2015b; Woods & Christian, 2016) we compare the accuracy of the suggested architecture not only against an optimally tuned ICP point-to-point registration process, but also against pointto-plane ICP, point-to-point and point-to-plane Sparse ICP (Bouaziz, Tagliasacchi, & Pauly, 2013), x84 ICP (Fusiello, Castellani, Ronchetti, & Murino, 2002) and S4PCS (Mellado, 2017). To the best of our knowledge such an extended comparison has not been presented yet in the current literature.

For completeness, the ICP point-to-point variant aims at aligning  $P_k$  and  $P_{k+1}$ , where  $P_k$  is kept fixed and  $P_{k+1}$  is transformed via the  $R^*$  to match  $P_k$ . During each transformation, ICP iteratively revises  $R^*$  (eq. (1)) to minimize the Euclidean point-pair distances between  $P_k$  and  $P_{k+1}$ . The pointto-point ICP, presented thereafter as ICP point, is a 4-step process:

22 a. Each vertex  $p_{k+1} = (x_{k+1}, y_{k+1}, z_{k+1})$  belonging to  $P_{k+1}$  is matched to its closest point in  $P_k$ 23 using a Euclidean distance metric. A match (inlier) is considered if the absolute Euclidean 24 translational distance is less than 0.01.

b. The matrices *R* and *T* of  $R^*$  (eq. (1)) are estimated using a root mean square point-to-point distance metric minimization method that will best align each  $p_{k+1} = (x_{k+1}, y_{k+1}, z_{k+1})$  with its matched vertex in  $P_k$ .

28 c. The estimated  $R^*$  from step (b) is applied on  $P_{k+1}$ .

d. If for the three latest consecutive iterations the average absolute translational and rotational difference between  $P_k$  and the transformed  $P_{k+1}$  of step (c) is less than 0.01 and 0.009 respectively, or the number of iterations has reached a pre-defined number, then ICP stops iterating. The output  $R^*$  from ICP is the latest estimated  $R^*$ . If these thresholds are not met, then ICP re-iterates starting

33 from step (a).

Current literature proposes various numbers of ICP iterations ranging from as few as 12 34 (Opromolla et al., 2014), up to 20 (L. Liu, Zhao, & Bo, 2016) or 30 (Opromolla et al., 2015b), 35 aiming at balancing the odometry accuracy and the computational burden imposed by ICP. Spurred 36 by the current literature trends, in this work the number of iterations for ICP is set to 20. We also 37 evaluate a second variant of ICP, namely the point-to-plane (presented thereafter as ICP plane), 38 39 that estimates the  $P_k$  and  $P_{k+1}$  point correspondences and then calculates the error metric based on the distance of the tangent plane of the corresponding point. For this ICP variant we use the same 40 thresholds as for the ICP point, while the number of maximum iterations is increased to 1000. To 41

compensate the sparse nature of the *Target* point cloud, we also compare the proposed architecture
 against Sparse ICP (Bouaziz et al., 2013) in a point-to-point and a point-to-plane scheme, presented

3 in the evaluation section as S-ICP point and S-ICP plane respectively. We use the code of

4 (Langlois, 2018) with 20 iterations. For completeness, an analysis between the interaction of the

5 number of iterations for all ICP variants with the odometry performance and processing time is

6 presented in Section 4.

Furthermore, in our experimental section we also evaluate the x84 ICP variant (Fusiello et al., 7 2002). The difference between ICP and x84 ICP is that the former uses as a threshold to reject 8 9 outliers based on the standard deviation of the point pair distances, while x84 ICP the median absolute deviation. For the x84 ICP we use the code of (Birdal, 2015) that is properly modified to 10 facilitate the x84 ICP outlier rejection scheme. The maximum number of iterations is set to 20. We 11 12 also challenge our proposed method against S4PCS which is an optimized version of the 4PCS global registration technique (Aiger, Mitra, & Cohen-Or, 2008). 4PCS is an iterative process that 13 extracts all coplanar 4-point sets from  $P_{k+1}$  that are approximately related by a rigid transformation 14 to a given planar 4-points from  $P_k$ . The operating principle of 4PCS is that under rigid motion 15 between  $P_k$  and  $P_{k+1}$  a number of coplanar 4-point sets from  $P_{k+1}$  remain invariant under affine 16 transformations. Thus, 4PCS estimates  $R^*$  between the randomly chosen coplanar 4-point sets 17 from  $P_k$  and  $P_{k+1}$  and retains the optimum  $R^*$  based on a similarity score. S4PCS affords a speedup 18 over 4PCS by eliminating redundant 4-point congruent sets, i.e. sets that are related by a rigid 19 transformation, and by indexing the coplanar 4-point sets for fast retrieval. In this work we use the 20 S4PCS code of (Mellado, 2017). Based on the tuning scenario Real-FB, we set an estimated 21 22 overlap ratio of 70% between  $P_k$  and  $P_{k+1}$  and a registration accuracy  $\delta = 0.01$ , while the rest of the

23 parameters are the default ones.

Finally, we also challenge our technique against the global/ local inlier voting (Buch, Yang,
Kruger, & Petersen, 2014) that involves a dual layer correspondence check comprising of GCC
and RANSAC followed by a singular value decomposition scheme. However, for better readability
comparison is presented in a compact form in Section 4.

Alternatively, current literature also suggests employing computer vision concepts (A. Rhodes et 28 al., 2016; A. P. Rhodes et al., 2017) and specifically proposes applying coarse Target pose 29 estimation utilizing the Oriented Unique and Repeatable Clustered Viewpoint Feature Histogram 30 (OUR-CVFH) regional descriptor (Aldoma, Tombari, Rusu, & Vincze, 2012) or the local feature 31 descriptor Spin Images (Andrew Edie Johnson & Hebert, 1998), that are then followed by a fine 32 registration process based on ICP point-to-point. Regarding OUR-CVFH, in our preliminary trials 33 we observed that it is not able to cluster the sparse Target point clouds of our scenarios and 34 considered the entire Target point cloud as a single cluster. This inevitably degraded OUR-CVFH 35 36 to the inferior VFH descriptor that did not manage to provide any feature matches. Additionally, in our preliminary trials, we confirmed (A. Rhodes et al., 2016) stating that the Spin Images 37 descriptor is affected by the low resolution of  $P_k$  and thus is not an optimum solution for space 38 odometry. In fact, we identified that Spin Images suffer from an ambiguous local reference axis 39 (LRA), the estimation of which is affected by a sparse *Target* point cloud. Due to the drawbacks 40 of Spin Images and OUR-CVFH on sparse point clouds, in our experimental section we will not 41

42 evaluate these two descriptors.

1 It should be noted that in any case, i.e. evaluating the proposed odometry architecture or the ones

- 2 suggested by the literature, we consider that the initial position and pose  $R^*$  of the *Source* is known
- 3 and that all methods aim to build-up an accurate odometry solution. It is assumed that this prior
- 4 knowledge is obtained before commencement of any of the methods examined in this work and
- can be based on Earth-based range and Doppler measurements or spacecraft-based optical images
  (A. B. Dietrich & McMahon, 2018). Additionally, it is worth noting that changing the point cloud
- resolution, accuracy and adding noise presents an additional challenge to the already challenging
- scenarios. However, the impact of each of these nuisances is related to their severity and to the
- 9 robustness of the 3D feature descriptors and GCC module. For better readability and to keep the
- 10 paper in a reasonable length, we will not involve any robustness to nuisance factors evaluation.

#### 11 **3.2** Evaluation criteria

16

12 Odometry performance metrics are based on the average and the maximum tri-axial translational

- 13 error between the ground truth (GT) position of the moving platform as tracked by the Optitrack
- 14 and the estimated one as provided by the proposed architecture:

15 
$$e_{avg}^{T} = \sqrt{\frac{1}{N} \sum_{k=1}^{N} \left( \left\| avg(T_{k}^{GT}) - avg(T_{k}^{opt}) \right\|^{2} \right)}$$
(27)

$$e_{\max}^{T} = \sqrt{\max\left(\left\|avg(T_{k}^{GT}) - avg(T_{k}^{opt})\right\|^{2}\right)}$$
(28)

17 where *N* is the number of point cloud instances per scenario,  $T_k^{opt} = T_{LIDAR}^{opt} \cdot T_k^{LIDAR}$  is the 18 transformed translation at instance *k* from the LIDAR reference frame to the Optitrack reference 19 frame in order to make its comparison with the GT translation applicable, and  $avg(\cdot)$  averages the 20 tri-axial translation into a single value. In addition to these metrics, we also calculate the drift, i.e. 21 RMSE, between the estimated endpoint and the GT endpoint, the corresponding translational error 22  $T_{error}$  as a percentage over the distance travelled and the average processing time *t* per *Target* scene.

23 Similarly to eq. (27) and eq. (28), we calculate the average rotational error:

24 
$$e_{avg}^{R} = \sqrt{\frac{1}{N} \sum_{k=1}^{N} \left( \left\| avg(R_{k}^{GT}) - avg(R_{k}^{opt}) \right\|^{2} \right)}$$
(29)

25 
$$e_{\max}^{R} = \sqrt{\max\left(\left\|avg(R_{k}^{GT}) - avg(R_{k}^{opt})\right\|^{2}\right)}$$
(30)

### Additionally, we also use the pose-graph comparison method of (Burgard et al., 2009)

27 
$$e^{RT} = \frac{1}{N} \sum_{k=1}^{N} \left( trans \left( R_{GT}^* \circ R_k^* \right)^2 + rot \left( R_{GT}^* \circ R_k^* \right)^2 \right)$$
(31)

28 where  $trans(\cdot)$  is the translational and  $rot(\cdot)$  the rotational part of the  $R^*$  and  $R^*_{GT}$  transformation

29 matrices respectively between  $P_k$  and  $P_{k+1}$  and  $\circ$  is the inverse motion composition operator as

1 defined in (Lu & Milios, 1997). The advantage of using the  $e^{RT}$  metric is two-fold. First, it uses

- 2 only relative relations between the  $R^*$  and  $R_{GT}^*$ , and thus it is more objective as it is not influenced
- 3 by any reference frame. Second, it encompasses in a single value both translational and rotational
- 4 errors affording an easy but complete comparison between the competitor methods. Note that the
- 5 GT translation  $T_i^{opt}$  and GT rotation  $R_i^{opt}$  are provided by the Optitrack. Thus, for the synthetic
- 6 scenarios the corresponding GT translation and rotation is the fictitious position per instance k of
- 7 the *Source* platform. Each of these performance metrics presented next are averaged over 20
- simulations with a standard deviation that is in the order of 10% the average value. However, for
  better readability and to preserve the number of figures and tables to a reasonable amount, we will
- 9 better readability and to preserve the number of figures and tal10 only present the averaged performance metrics.

Given the large amount of feature description and recursive filtering combinations evaluated in our odometry architecture, challenging our method against six methods offered by current literature and utilizing a large number of performance metrics, for the sake of readability, all scenarios will be analyzed based on the  $e^{RT}$  metric. We prefer  $e^{RT}$  against the other metrics as is encompasses both translational and rotational errors in a single metric. However, for the sake of

16 completeness, all error metrics are presented in the corresponding tables.

### 17 **3.3** Odometry trials on real LIDAR data

### 18 3.3.1 *Real-FB* trajectory

19 This scenario considers a straight-line forward - backward motion of the Source with respect to the *Target*. Point clouds are acquired by a LIDAR device that is placed on the *Source* platform. 20 The average point cloud size per *Target* platform comprises of 882 vertices demonstrating the 21 sparse nature and the limited structure of the EnviSat Target point cloud (Figure 2 (c)). 22 23 Performance metrics are presented in Table 3 with the top performing method per error being highlighted in red. Additionally, Figure 7 presents the corresponding odometry trajectory obtained 24 per 3D descriptor and recursive filtering method along with all competitor methods. For better 25 readability, methods with large errors are discarded and not presented in the corresponding plots. 26

From Table 3 it is evident that quite a few 3D local description and recursive filtering combinations 27 are more accurate compared to the majority of the competitor methods. Top performance affording 28 lowest  $e^{RT}$  at a low processing time, is provided by the combination of HoD-S with the adaptive 29  $\alpha\beta$  filter, i.e. HoD-S/ $\alpha\beta$ . It should be noted that in terms of error. SHOT/ $\alpha\beta$  is slightly more 30 accurate than HoD-S/  $\alpha\beta$ . However, the latter is three times faster to execute than SHOT/  $\alpha\beta$  and 31 thus HoD-S/ $\alpha\beta$  is considered as an overall more appealing option. This is because HoD-S neglects 32 estimating a LRF/A and thus is more robust to sparse point clouds. Additionally, neglecting a 33 LRF/A and relying on a small description length, makes HoD-S the most processing efficient 34 descriptor among the ones evaluated. In terms of pure odometry accuracy, SHOT attains the lowest 35  $e^{RT}$  error, but interestingly, from Table 3 it is evident that HoD-S is the most accurate descriptor 36 in terms of translational error, and TriSI in terms of rotational error. This reveals that SHOT 37 achieves the best balance between the translational and the rotational error. It is worth noting that 38 39 current literature offers several evaluations on the robustness of 3D local feature descriptors to mesh/point cloud resolution variations (Guo et al., 2016, 2015, 2013a; Salti et al., 2014). However, 40

41 these papers examine the case where the features from a dense point cloud, e.g. Source, are

matched against the features of a sparse point cloud, e.g. Target. In contrast to this, here we involve 1

a Source and a Target point cloud that present some variation and are both sparse. Finally, FPFH 2

presents the largest errors due to its short feature descriptor (33 elements) and its sensitive LRF to 3

low resolution point clouds. Interestingly, Table 3 presents TriSI as the optimum descriptor for the 4

adaptive SDRE filter. However, from Table 3 and Figure 7, is it clear that TrISI provides one of 5 the largest translational errors indicating that the  $e^{RT}$  metric is biased by the very low rotational

6 errors of TriSI. In fact, that sparse nature of  $P_k$  and  $P_{k+1}$  forces TriSI to fail providing enough

7 geometrically consistent feature matches to the recursive filtering module, and thus the latter does 8

not iterate properly, forcing the estimated  $R^*$  to preserve its initialization value.

9

Table 3: Performance metrics for the *Real-FB* scenario

| Descriptor  | drift                                      | Terror | $e_{\max}^{T}$ | $e_{avg}^{T}$ | max         | k Error        | (m)            | Avera          | age erro | or (m) | $e_{avg}^{T}$ | $e_{\max}^R$  | $e^{RT}$    | $t(m_{c})$ |
|-------------|--|--------|----------------|---------------|-------------|----------------|----------------|----------------|----------|--------|---------------|---------------|-------------|------------|
| Descriptor  | (m)  | (%)    | $e_{\rm max}$  | $e_{avg}$     | Х           | Y              | Ζ              | Х              | Y        | Ζ      | eavg          | $e_{\rm max}$ | е           | t (ms)     |
|             |  |        |                |               | a           | daptiv         | e <i>H</i> ∞ r | ecursiv        | ve filte | ring   |               |               |             |            |
| HoD-S       | 0.16                                       | 2.11   | <i>0.17</i>    | 0.09          | 0.05        | 0.13           | 0.09           | 0.05           | 0.03     | 0.05   | 9.12          | 13.58         | 9.91        | 560        |
| FPFH        | 3.56                                       | 48.02  | 3.56           | 2.32          | 0.91        | 3.19           | 1.28           | 0.62           | 1.91     | 0.76   | 9.11          | 13.57         | 13.38       | 687        |
| SHOT        | 0.58                                       | 7.77   | 0.59           | 0.23          | 0.56        | 0.15           | 0.09           | 0.12           | 0.09     | 0.10   | 8.61          | 12.77         | 9.89        | 1794       |
| HoD         | 0.15                                       | 2.00   | 0.36           | 0.17          | 0.34        | 0.07           | 0.01           | 0.12           | 0.04     | 0.03   | 9.12          | 13.57         | 10.05       | 950        |
| RoPS        | 0.84                                       | 11.39  | 0.85           | 0.25          | 0.19        | 0.68           | 0.48           | 0.05           | 0.15     | 0.13   | 9.13          | 13.57         | 10.26       | 2376       |
| TriSI       | 0.26                                       | 3.56   | 3.13           | 1.69          | 3.13        | 0.01           | 0.01           | 1.39           | 0.03     | 0.04   | 3.35          | 4.55          | 6.32        | 1536       |
|             |  |        |                |               | ada         | ptive <i>I</i> | Kalman         | <i>i</i> recur | sive fil | tering |               |               |             |            |
| HoD-S       | 0.84                                       | 11.29  | 1.29           | 0.79          | 1.12        | 0.08           | 0.64           | 0.50           | 0.03     | 0.41   | 2.34          | 4.90          | 4.48        | 557        |
| FPFH        | 2.41                                       | 32.49  | 2.82           | 1.78          | 0.70        | 2.37           | 1.36           | 0.56           | 1.24     | 0.73   | 2.48          | 4.55          | 6.04        | 687        |
| SHOT        | 0.58                                       | 7.84   | 0.59           | 0.23          | 0.57        | 0.16           | 0.06           | 0.12           | 0.10     | 0.11   | 0.27          | 0.51          | 1.56        | 1794       |
| HoD         | 0.26                                       | 3.52   | 0.35           | 0.21          | 0.30        | 0.06           | 0.16           | 0.12           | 0.04     | 0.12   | 0.91          | 1.83          | 2.09        | 946        |
| RoPS        | 1.64                                       | 22.09  | 1.64           | 0.81          | 0.64        | 0.65           | 1.37           | 0.29           | 0.13     | 0.53   | 2.60          | 4.66          | 4.45        | 2375       |
| TriSI       | 0.26                                       | 3.57   | 3.13           | 1.69          | 3.13        | 0.01           | 0.01           | 1.39           | 0.03     | 0.04   | 0.05          | 0.07          | 3.02        | 1536       |
|             | adaptive $\alpha\beta$ recursive filtering |        |                |               |             |                |                |                |          |        |               |               |             |            |
| HoD-S       | 0.16                                       | 2.20   | <i>0.18</i>    | 0.10          | <i>0.11</i> | 0.07           | 0.13           | 0.05           | 0.04     | 0.05   | 0.99          | 1.34          | 1.79        | <b>518</b> |
| FPFH        | 3.58                                       | 48.21  | 3.58           | 2.33          | 0.87        | 3.23           | 1.26           | 0.60           | 1.93     | 0.77   | 0.60          | 0.81          | 4.87        | 679        |
| SHOT        | 0.56                                       | 7.54   | 0.57           | 0.23          | 0.54        | 0.17           | 0.08           | 0.12           | 0.10     | 0.11   | 0.26          | 0.35          | 1.57        | 1784       |
| HoD         | <i>0.15</i>                                | 2.00   | 0.38           | 0.18          | 0.36        | 0.07           | 0.01           | 0.13           | 0.04     | 0.03   | 0.99          | 1.36          | 1.94        | 903        |
| RoPS        | 0.86                                       | 11.53  | 0.86           | 0.26          | 0.15        | 0.70           | 0.48           | 0.04           | 0.16     | 0.13   | 0.66          | 0.96          | 1.75        | 23620      |
| TriSI       | 0.26                                       | 3.53   | 3.13           | 1.69          | 3.13        | 0.01           | 0.01           | 1.40           | 0.03     | 0.04   | 0.06          | 0.08          | 3.03        | 1535       |
|             | -  |        |                | -             | ad          | aptive         |                | recurs         | ive filt | ering  |               |               |             |            |
| HoD-S       | 0.85                                       | 11.41  | 0.86           | 0.40          | 0.45        | 0.54           | 0.49           | 0.18           | 0.23     | 0.16   | 9.12          | 13.58         | 10.85       | 521        |
| FPFH        | 4.19                                       | 56.46  | 4.19           | 2.54          | 1.31        | 3.61           | 1.69           | 0.82           | 2.12     | 0.63   | 9.11          | 13.57         | 13.74       | 684        |
| SHOT        | 1.13                                       | 15.28  | 1.14           | 0.46          | 0.92        | 0.52           | 0.44           | <i>0.17</i>    | 0.28     | 0.13   | 8.61          | 12.77         | 10.24       | 1752       |
| HoD         | 0.85                                       | 11.43  | 0.85           | 0.38          | 0.48        | 0.53           | 0.47           | 0.14           | 0.20     | 0.18   | 9.12          | 13.57         | 10.71       | 907        |
| RoPS        | 1.23                                       | 16.63  | 1.24           | 0.53          | 0.50        | 1.04           | 0.42           | 0.22           | 0.35     | 0.17   | 9.13          | 13.57         | 11.07       | 2376       |
| TriSI       | <b>0.2</b> 7                               | 3.57   | 3.10           | 1.67          | 3.10        | 0.02           | 0.03           | 1.37           | 0.02     | 0.04   | 3.35          | 4.55          | <i>6.28</i> | 1536       |
|             |  |        |                |               |             |                | mpetit         |                | emes     |        |               | T             |             |            |
| ICP point   | 0.44                                       | 5.90   | 1.41           | 0.64          | 1.30        | 0.50           | 0.22           | 0.43           | 0.15     | 0.13   | 84.49         | 133.01        | 86.32       | 5          |
| ICP plane   | 1.90                                       | 25.61  | 1.91           | 0.97          | 1.79        | 0.07           | 0.67           | 0.61           | 0.40     | 0.35   |               | -111.87       |             | 9          |
| ICP x84     | 8.75                                       | 117.97 | 11.36          | 9.57          | 8.69        | 4.94           | 4.56           | 6.65           | 3.78     | 4.24   |               | -121.96       |             | 40         |
| S4PCS       | 1.26                                       | 16.98  | 1.91           | 1.09          | 0.10        | 1.89           | 0.19           | 0.16           | 0.73     | 0.45   | 77.01         | 141.53        | 79.53       | 1225       |
| S-ICP point | 0.13                                       | 1.70   | 3.52           | 1.97          | 3.51        | 0.20           | 0.11           | 1.64           | 0.08     | 0.07   | 0.01          | 0.01          | 3.42        | 145.76     |
| S-ICP plane | 0.13                                       | 1.70   | 3.52           | 1.97          | 3.51        | 0.20           | 0.11           | 1.64           | 0.08     | 0.07   | 0.01          | 0.01          | 3.42        | 150.16     |

In terms of processing efficiency, as expected HoD-S with HoD are the fastest to execute as both neglect a LRF/A estimation, and RoPS with TriSI are the least processing efficient due to involving a complex LRF estimation process. It is worth noting that despite HoD-S and HoD being implemented in MATLAB, these are still faster to execute than FPFH and SHOT that are in implemented in C++/PCL. From Table 3, we also observe that the adaptive  $\alpha\beta$  and Kalman filters afford similar accuracy, with  $\alpha\beta$  being slightly more accurate, demonstrating that due to the minor motion between  $P_k$  and  $P_{k+1}$ , a linear motion estimation model with two parameters, as is the  $\alpha\beta$ filter, is sufficient for space odometry. For better visualization of which filter is performing better, in Figure 8 we compare the best feature descriptor from each filter.

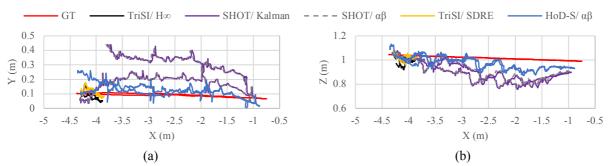


Figure 8: Forward – Backward *Real-FB* scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric along with the overall top performing in terms of accuracy and processing efficiency HoD-S/  $\alpha\beta$ . SHOT/ *Kalman* and SHOT/  $\alpha\beta$  present quite similar results highlighting the effectiveness of a linear 2-parameter motion estimation model. Despite TriSI presenting the lowest  $e^{RT}$  error for the SDRE filter, the error is biased by a low rotational error as the translational one is quite large.

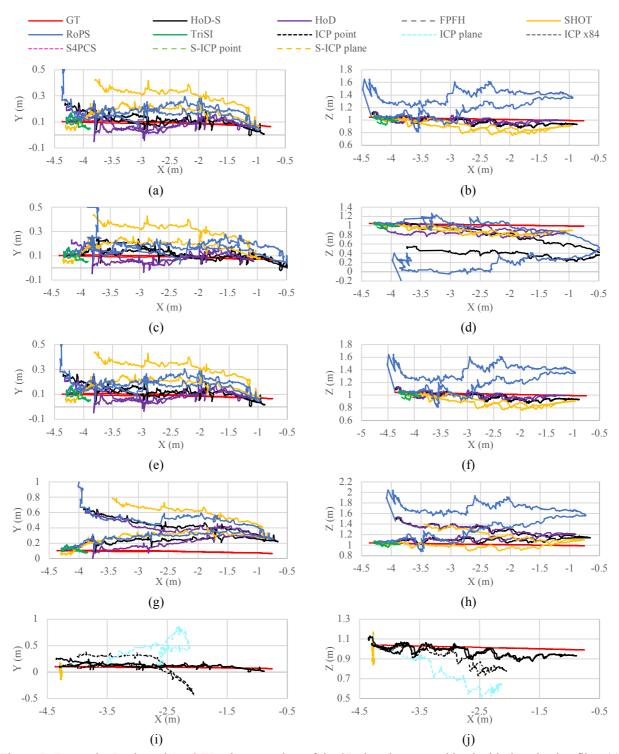


Figure 7: Forward – Backward *Real-FB* odometry plots of the 3D descriptors combined with the adaptive filter (a)-(b)  $H\infty$ , (c)-(d) *Kalman*, (e)-(f)  $\alpha\beta$ , (g)-(h) *SDRE*, and (i)-(j) the competitor methods along with the top performing method HoD-S/  $\alpha\beta$ , which is the black trajectory closest to the GT (due to large errors and for better readability we crop RoPS from (a),(b),(c),(e),(g), omit FPFH from (a) – (h) and ICP x84 and S4PCS from (i) –(j)). TriSI due to the sparse point clouds fails to provide an adequate number of geometrically consistent feature matches, forcing the recursive filtering process not to iterate properly and thus  $R^*$  mostly preserves its initialization value.

Regarding the competitor methods, the ICP point and plane variants are the fastest to execute and 1 are the most accurate methods among all competitor techniques evaluated. Despite that, in terms 2 of accuracy these are still inferior to most of the proposed combinations. From Table 3 and Figures 3 7 (i) and (j), we observe that ICP point is slightly more accurate than ICP plane, despite  $P_k$  mostly 4 comprising of flat surfaces. An explanation is that  $P_k$  has quite a few groups of vertices that are 5 horizontally aligned (Figure 2 (c)) with these groups having a substantial vertical distance between 6 them. Hence, depending on the frame-to-frame motion of the Target point cloud, the plane 7 estimation involved in the ICP plane process is affected by this structure, degrading the overall 8 9 performance of ICP plane. Similarly, ICP point fails to present an accurate odometry solution because the structure of  $P_k$  forces this ICP variant to converge to an appealing solution only if most 10 of these "horizontal groups of vertices" are aligned. Accordingly, ICP x84 and both S-ICP variants 11 fail to provide an accurate odometry. In addition to that, sparse point clouds force ICP to perform 12 suboptimal (Opromolla, Fasano, et al., 2017). For the S-ICP variants, due to the vertex geometry 13 these in most cases provide an  $R^*$  with zero rotation and translation, which is clearly presented in 14 Figure 7 (i) and (j). 15

### 16 3.3.2 *Real-Curved* trajectory

This scenario also considers real LIDAR data but is more challenging compared to the Real-FB 17 scenario because in addition to the poor structure and sparse Target point cloud, this trajectory is 18 also highly curved. Hence, most of the descriptors attains a larger  $e^{RT}$  error compared to the *Real*-19 FB scenario. From analyzing Table 4 and Figure 9, we conclude that HoD/ Kalman attains the 20 lowest error with HoD-S/  $\alpha\beta$  following next. However, given that the latter requires half the 21 processing time of the former, and that the  $e^{RT}$  based performance difference between these two 22 combinations is relatively small, we conclude that the overall optimum choice for this scenario is 23 the HoD-S/  $\alpha\beta$ . A commonality between the two real scenarios is that Trisi affords the lowest  $e^{RT}$ 24 error for a few filters, but again this metric is biased by the low rotational error of TriSI. In fact, 25

26 TriSI has the highest  $e_{avg}^{T}$  odometry error for the reasons already presented in Section 3.3.1.

For the adaptive *Kalman* and  $\alpha\beta$  filters, HoD-S is the optimum choice as it affords the lowest  $e^{RT}$ error and simultaneously requires the lowest processing time. Finally, similarly to the *Real-FB* 

29 scenario, in this scenario FPFH also attains the largest errors, which are more evident in the Z-

axis. In terms of processing efficiency, except for TriSI, the hierarchy is the same as for the *Real- FB* scenario.

Regarding the accuracy of the recursive filtering schemes, we notice from Table 4 and Figure 9 that the adaptive  $\alpha\beta$  filter gains the lowest  $e^{RT}$  error with the adaptive Kalman to follow. This is due to the minor motion between  $P_k$  and  $P_{k+1}$  that can be simulated with a 2-parameter linear model. To highlight which filter is performing better, in Figure 10 we compare the best feature descriptor from each filter. A further analysis at a higher level involving the overall performance of each

descriptor and filtering method over all scenarios is presented in Section 4.

38

39

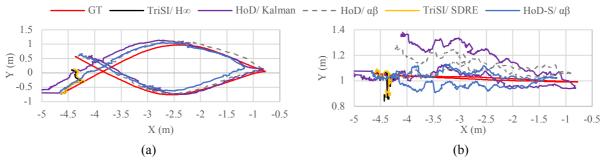


Figure 10: *Real-Curved* scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric along with the overall top performing in terms of accuracy and processing efficiency HoD-S/ $\alpha\beta$ . TriSI/SDRE presents the lowest  $e^{RT}$ , however it is biased by a low rotational error as the translational one is quite large forcing this combination to preserve the filter's initialization  $R^*$ .

|   | Table 4: Performance metrics for the <i>Real-Curved</i> scenario |        |              |               |             |                |        |                |          |        |               |              |          |            |
|---|--|--------|--------------|---------------|-------------|----------------|--------|----------------|----------|--------|---------------|--------------|----------|------------|
| Descriptor                              | drift  | Terror | $e_{\max}^T$ | $e_{avg}^{T}$ |             | k Error        | < /    |                | age erro | · · ·  | $e_{avg}^{T}$ | $e_{\max}^R$ | $e^{RT}$ | t (ms)     |
| Beschiptor                              | (m)  | (%)    | max          | Cavg          | Х           | Y              | Ζ      | Х              | Y        | Z      | avg           | max          | Ũ        | t (IIIS)   |
| adaptive <i>H</i> ∞ recursive filtering |  |        |              |               |             |                |        |                |          |        |               |              |          |            |
| HoD-S                                   | 0.27   | 2.15   | 0.28         | 0.16          | 0.20        | 0.04           | 0.20   | 0.08           | 0.07     | 0.08   | 12.22         | 17.95        | 13.51    | <i>481</i> |
| FPFH                                    | 1.19   | 9.60   | 1.60         | 1.01          | 0.29        | 0.62           | 1.43   | 0.22           | 0.53     | 0.71   | 11.99         | 17.90        | 14.60    | 690        |
| SHOT                                    | 0.72   | 5.86   | 0.93         | 0.71          | 0.80        | 0.45           | 0.11   | 0.57           | 0.34     | 0.04   | 11.05         | 16.72        | 13.55    | 1698       |
| HoD                                     | 0.06   | 0.51   | 0.47         | 0.23          | 0.42        | 0.22           | 0.03   | 0.16           | 0.10     | 0.05   | 12.00         | 17.96        | 13.42    | 817        |
| RoPS                                    | 0.91   | 7.35   | 0.91         | 0.37          | <i>0.17</i> | 0.05           | 0.89   | 0.16           | 0.06     | 0.26   | 12.27         | 18.18        | 14.08    | 2373       |
| TriSI                                   | 0.51   | 4.12   | 3.45         | 1.93          | 3.43        | 0.37           | 0.03   | 1.50           | 0.49     | 0.03   | 4.27          | 6.10         | 7.83     | 2452       |
|   |  |        |              |               | ada         | ptive <i>I</i> | Kalman | <i>i</i> recur | sive fil | tering |               |              |          |            |
| HoD-S                                   | 0.40   | 3.23   | 0.53         | 0.31          | 0.29        | 0.05           | 0.30   | 0.25           | 0.09     | 0.09   | 14.85         | 22.70        | 16.66    | <i>480</i> |
| FPFH                                    | 1.20   | 9.68   | 1.60         | 1.02          | 0.30        | 0.62           | 1.43   | 0.22           | 0.54     | 0.72   | 1.92          | 3.62         | 4.53     | 690        |
| SHOT                                    | 0.71   | 5.78   | 0.93         | 0.71          | 0.80        | 0.45           | 0.10   | 0.57           | 0.33     | 0.04   | 0.61          | 1.03         | 3.10     | 1697       |
| HoD                                     | 0.06   | 0.50   | <i>0.48</i>  | 0.24          | 0.42        | 0.22           | 0.03   | 0.16           | 0.11     | 0.05   | 0.98          | 1.90         | 2.41     | 816        |
| RoPS                                    | 0.36   | 2.90   | 1.01         | 0.65          | 0.42        | 0.39           | 0.56   | 0.18           | 0.05     | 0.51   | 13.57         | 20.16        | 15.35    | 2372       |
| TriSI                                   | 0.51   | 4.11   | 3.45         | 1.93          | 3.43        | 0.36           | 0.03   | 1.50           | 0.49     | 0.03   | 0.21          | 0.25         | 3.77     | 2452       |
| adaptive <i>αβ</i> recursive filtering  |  |        |              |               |             |                |        |                |          |        |               | -            |          |            |
| HoD-S                                   | 0.25   | 2.03   | 0.27         | 0.16          | 0.17        | 0.05           | 0.20   | 0.09           | 0.08     | 0.08   | 1.44          | 1.81         | 2.75     | <b>464</b> |
| FPFH                                    | 1.21   | 9.75   | 1.60         | 1.02          | 0.30        | 0.62           | 1.43   | 0.23           | 0.54     | 0.72   | 0.57          | 0.85         | 3.21     | 683        |
| SHOT                                    | 0.72   | 5.84   | 0.94         | 0.72          | 0.81        | 0.45           | 0.10   | 0.58           | 0.33     | 0.04   | 0.43          | 0.60         | 2.93     | 1691       |
| HoD                                     | 0.05   | 0.41   | 0.49         | 0.24          | 0.43        | 0.22           | 0.03   | 0.17           | 0.11     | 0.05   | 1.21          | 1.47         | 2.65     | 809        |
| RoPS                                    | 0.91   | 7.35   | 0.91         | 0.38          | 0.19        | 0.06           | 0.89   | 0.18           | 0.06     | 0.25   | 1.15          | 1.59         | 2.99     | 2357       |
| TriSI                                   | 0.51   | 4.11   | 3.45         | 1.93          | 3.43        | 0.36           | 0.03   | 1.50           | 0.49     | 0.03   | 0.14          | 0.16         | 3.70     | 2451       |
|   | -  |        |              | -             |             | aptive         |        |                | 1        | 0      |               |              |          |            |
| HoD-S                                   | 0.74   | 5.99   | 0.77         | 0.41          | 0.49        | 0.34           | 0.49   | 0.16           | 0.22     | 0.22   | 12.22         | 17.95        | 14.14    | <b>466</b> |
| FPFH                                    | 1.55   | 12.50  | 1.56         | 1.02          | 0.24        | 0.68           | 1.37   | 0.17           | 0.68     | 0.57   | 11.99         | 17.90        | 14.54    | 685        |
| SHOT                                    | 0.46   | 3.74   | 0.79         | 0.56          | 0.68        | 0.34           | 0.22   | 0.44           | 0.21     | 0.13   | 11.05         | 16.72        | 13.40    | 1675       |
| HoD                                     | 0.56   | 4.54   | 0.66         | 0.39          | 0.43        | 0.40           | 0.29   | 0.19           | 0.25     | 0.14   | 12.00         | 17.96        | 13.92    | 812        |
| RoPS                                    | 1.24   | 10.05  | 1.24         | 0.50          | 0.12        | 0.35           | 1.19   | 0.06           | 0.13     | 0.37   | 12.27         | 18.18        | 13.96    | 2360       |
| TriSI                                   | 0.46   | 3.72   | 3.43         | 1.91          | 3.41        | 0.35           | 0.05   | 1.48           | 0.48     | 0.04   | 4.27          | 6.10         | 7.84     | 2453       |
|   |  |        |              |               |             |                | mpetit |                |          |        |               |              |          |            |
| ICP point                               | 2.70   | 21.81  | 2.78         | 1.68          | 1.68        | 2.07           | 0.53   | 0.66           | 1.14     | 0.16   | 104           | -179.13      |          | 6          |
| ICP plane                               | 1.90   | 25.61  | 1.91         | 0.97          | 1.79        | 0.07           | 0.67   | 0.61           | 0.40     | 0.35   | -171          | -111.87      |          | 9          |
| ICP x84                                 | 7.08   | 57.23  | 7.46         | 4.24          | 6.30        | 3.66           | 1.59   | 2.48           | 2.07     | 1.17   | 135           | -142.43      |          | 53         |
| S4PCS                                   | 4.60   | 37.18  | 4.60         | 2.89          | 3.52        | 2.53           | 1.54   | 1.47           | 1.73     | 0.81   | 141           | -124.33      |          | 1219       |
| S-ICP point                             | 0.13   | 1.70   | 3.52         | 1.97          | 3.51        | 0.20           | 0.11   | 1.64           | 0.08     | 0.07   | 0.01          | 0.01         | 3.42     | 137        |
| S-ICP plane                             | 0.13   | 1.70   | 3.52         | 1.97          | 3.51        | 0.20           | 0.11   | 1.64           | 0.08     | 0.07   | 0.01          | 0.01         | 3.42     | 145        |

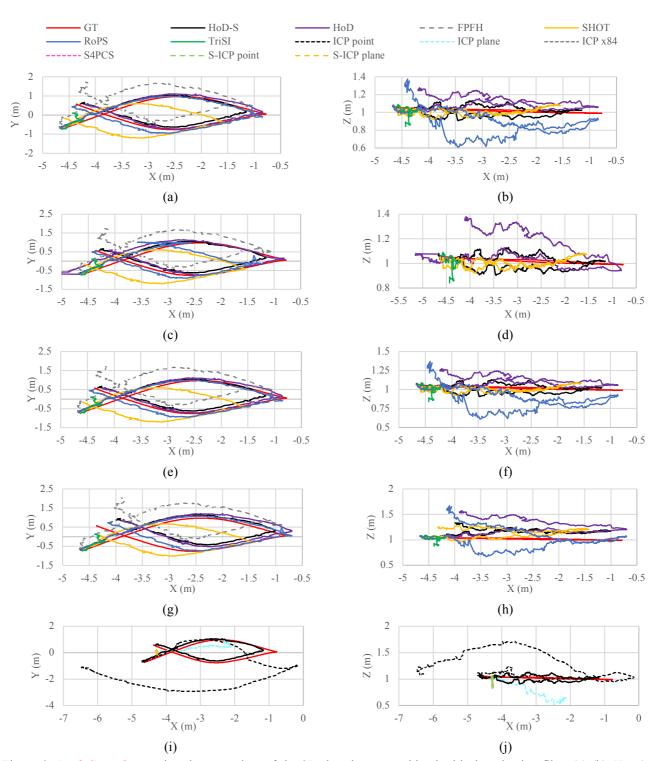


Figure 9: *Real-Curved* scenario odometry plots of the 3D descriptors combined with the adaptive filter (a)-(b)  $H\infty$ , (c)-(d) *Kalman*, (e)-(f)  $\alpha\beta$ , (g)-(h) *SDRE*, and (i)-(j) competitor methods along with the top performing proposed method HoD-S/ $\alpha\beta$ , which is the black trajectory closest to the GT (due to large errors and for better readability we omit FPFH from (b), (d), (f), (h), RoPS from (d), ICP x84 from (i)-(j)). TriSI due to the sparse point clouds fails to provide an adequate number of geometrically consistent feature matches, forcing the recursive filtering process not to iterate properly and thus  $R^*$  mostly preserves its initialization value.

1 As expected, the processing burden of every 3D local feature descriptor and recursive filtering

2 combination is higher than the time needed by any ICP variant, mainly due to the feature matching/

3 correspondence grouping process. Except from being processing efficient, all ICP methods are less

4 accurate posing a non-optimal odometry solution for the reason presented in Section 3.3.1.

5 Similarly to the *Real-FB* scenario, in this trajectory ICP x84 and both S-ICP variant also to fail to

6 provide an accurate odometry.

# 7 **3.4** Odometry trials on synthetic LIDAR data

# 8 3.4.1 Sim-EoI trajectory

9 This is a synthetic data scenario that involves a simulated Ellipsoidal trajectory of the *Source*10 platform around the *Target* platform. This is a realistic scenario with an average *Target* point cloud
11 size of 3099 vertices that are affected by several external parameters described in the introduction
12 of Section 3. Results on the Sim Fol trajectory are presented in Table 5 and Figure 11.

of Section 3. Results on the Sim-EoI trajectory are presented in Table 5 and Figure 11.

13 The combination of HoD-S with the adaptive  $\alpha\beta$  filter exhibits the highest accuracy. However due to the large vertex cardinality of  $P_k$  and the number of correspondences, the processing time 14 required by HoD-S is now one of the highest. Computationally, FPFH affords overall the smallest 15 burden due to the fewer number of correspondences it provides, but its accuracy is one of the 16 poorest. On the contrary, RoPS and TriSI require the highest processing time due to the processing 17 burden implied by their complex LRF estimation, in combination with the high cardinality of the 18 19 Target point cloud. In terms of translational error, HoD-S presents the lowest error, while similarly to the Real-FB and Real-Curved scenarios, TriSI affords the lowest rotational error. However, in 20 contrast to TriSI's translational performance presented in the scenarios earlier, here it achieves a 21 22 moderate accuracy. This is because as in this scenario TriSI has 1572 geometrically consistent correspondences  $\Omega$ , and thus the recursive filtering scheme performs 1572 iterations settling to a 23 more accurate rigid body transformation  $R^*$ . 24

Regarding the accuracy of the recursive filtering schemes, we notice from Table 5 that the adaptive 25  $\alpha\beta$  filter achieves the lowest average error, with the  $H\infty$  and SDRE filters following closely. 26 Surprisingly, the adaptive Kalman filter fails to provide an appealing accuracy with any of the 27 evaluated descriptors. In Figure 12 we compare the best feature descriptor from each filter. The 28 Kalman filter constantly attains the highest errors for all feature descriptors, while the latter ones 29 perform quite well with the rest of the filtering methods. This is because all modules within the 30 proposed architecture are tuned based on the sparse Real-FB scenario. Considering that the Sim-31 *EoI* scenario examined here is denser, we observe that the parameters of the Kalman filter are more 32 sensitive to the point cloud cardinality, while the rest of the filters are more robust. Thus, for this 33 scenario Kalman requires to have its parameters re-tuned, loosing though its generalization. For 34 the sake of the latter, we preserve the same parameter values as already tuned in the Real-FB 35 36 scenario

37

38

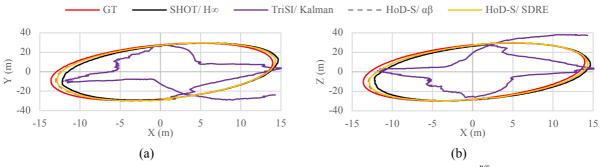


Figure 12: *Sim -Eol* scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric. Due to the  $P_k$  cardinality of this scenario, the parameters of Kalman fail to attain an appealing odometry accuracy.

Table 5: Performance metrics for the *Sim-EoI* scenario

| Descriptor  | drift        | Terror | $e_{\max}^T$  | $e_{avg}^{T}$ | max         | x Error        | : (m)           | Avera   | ige erro    | or (m)      | $e_{avg}^{T}$ | $e_{\max}^R$  | $e^{RT}$    | $t(m_0)$    |
|-------------|--------------|--------|---------------|---------------|-------------|----------------|-----------------|---------|-------------|-------------|---------------|---------------|-------------|-------------|
| Descriptor  | (m)          | (%)    | $e_{\rm max}$ | eavg          | Х           | Y              | Ζ               | Х       | Y           | Ζ           | eavg          | $e_{\rm max}$ | e           | t (ms)      |
|             |              |        |               |               | ac          | lantive        | e <i>H</i> ∞ re | cursiv  | e filter    | ring        |               |               |             |             |
| HoD-S       | 1.16         | 0.40   | 1.19          | 0.69          | 0.92        | 0.53           | 0.50            | 0.48    | 0.21        | 0.20        | 8.81          | 10.88         | 15.86       | 28157       |
| FPFH        | 2.56         | 0.88   | 2.59          | 1.49          | 2.40        | 0.94           | 0.18            | 1.24    | 0.36        | 0.22        | 7.56          | 10.71         | 17.18       | 6525        |
| SHOT        | 1.93         | 0.66   | 1.94          | 1.30          | 1.87        | 0.46           | 0.19            | 1.13    | 0.18        | 0.09        | 2.89          | 3.95          | 10.56       | 13701       |
| HoD         | 1.16         | 0.40   | 1.28          | 0.81          | 0.91        | 0.72           | 0.55            | 0.48    | 0.39        | 0.28        | 8.83          | 10.97         | 17.47       | 34832       |
| RoPS        | 2.37         | 0.81   | 3.16          | 1.87          | 2.82        | 0.77           | 1.18            | 1.56    | 0.27        | 0.39        | 7.91          | 10.33         |             | 40647       |
| TriSI       | 1.90         | 0.65   | 1.95          | 1.08          | 1.68        | <i>0.43</i>    | 0.27            | 0.84    | 0.29        | 0.09        | 8.98          | 11.16         | 16.80       | 38306       |
|             |              |        |               |               | ada         | ptive <i>k</i> | Kalman          |         | sive fil    | tering      |               |               |             |             |
| HoD-S       | 28.14        | 9.68   | 38.48         | 25.49         | 2.28        | 29.11          | 25.07           | 9.63    | 13.67       | 14.27       | 127.37        | 97.55         | 178.64      | 28144       |
| FPFH        | <i>14.83</i> | 5.10   | <i>14.98</i>  | 11.69         | 13.40       | <i>3.27</i>    | 4.59            | 9.64    | 2.16        | 3.42        | 109.41        | 154.76        | 136.54      | 6518        |
| SHOT        | 18.85        | 6.48   | 37.37         | 25.98         | 10.37       | 24.73          | 25.63           | 10.63   | 11.36       | 16.25       | 105.31        | 164.46        | 148.07      | 13870       |
| HoD         | 15.88        | 5.46   | 29.03         | 21.60         | 8.80        | 11.59          | 25.11           | 4.24    | 12.64       | 14.14       | 79.02         | 117.81        | 125.87      | 34817       |
| RoPS        | 20.36        | 7.00   | 39.97         | 28.72         | 8.13        | 29.34          | 23.98           | 10.17   | 13.88       | 18.76       | 156.53        | 200.72        | 202.61      | 40637       |
| TriSI       | 17.64        | 6.07   | 32.87         | 21.86         | <i>1.49</i> | 20.78          | 25.18           | 6.91    | 6.92        | 16.38       | <i>50.72</i>  | 66.26         | 90.25       | 38296       |
|             |              |        |               |               | a           | daptiv         | e αβ re         | cursiv  | e filter    | ing         |               |               |             |             |
| HoD-S       | 1.24         | 0.43   | 1.26          | 0.70          | 1.02        | 0.44           | 0.24            | 0.55    | <i>0.18</i> | 0.09        | 2.91          | 3.98          | <i>9.23</i> | 27954       |
| FPFH        | 2.61         | 0.90   | 2.63          | 1.49          | 2.47        | 0.89           | 0.11            | 1.26    | 0.34        | 0.10        | 2.77          | 3.88          | 11.59       | <i>6424</i> |
| SHOT        | 1.93         | 0.66   | 1.94          | 1.30          | 1.87        | 0.46           | <i>0.19</i>     | 1.13    | <i>0.18</i> | 0.09        | 2.89          | 3.95          | 10.56       | 13701       |
| HoD         | 1.22         | 0.42   | 1.27          | 0.81          | 1.00        | 0.63           | 0.30            | 0.55    | 0.38        | 0.15        | 2.89          | 3.92          | 10.80       | 34610       |
| RoPS        | 2.56         | 0.88   | 3.25          | 1.96          | 2.88        | 0.76           | 1.30            | 1.60    | 0.27        | 0.51        | 2.89          | 4.02          | 13.90       | 40502       |
| TriSI       | 2.04         | 0.70   | 2.08          | 1.16          | 2.04        | <i>0.35</i>    | <i>0.19</i>     | 0.90    | 0.30        | 0.13        | 2.73          | 3.66          | 11.10       | 38160       |
|             |              |        |               |               | ada         | ptive /        | SDRE 1          | recursi | ive filt    | ering       |               |               |             |             |
| HoD-S       | 1.44         | 0.50   | 1.46          | 0.86          | 1.17        | <i>0.27</i>    | 0.76            | 0.63    | <i>0.13</i> | 0.34        | 8.81          | 10.88         | 16.56       | 27990       |
| FPFH        | 2.79         | 0.96   | 2.81          | 1.65          | 2.70        | 0.64           | 0.48            | 1.39    | 0.24        | 0.35        | 7.56          | 10.71         | 17.45       | <i>6425</i> |
| SHOT        | 2.21         | 0.76   | 2.21          | 1.49          | 1.88        | 0.73           | 0.57            | 1.23    | 0.32        | 0.32        | 7.96          | 10.29         | 18.06       | 13702       |
| HoD         | 1.40         | 0.48   | 1.49          | 0.94          | 1.16        | 0.46           | 0.80            | 0.62    | 0.25        | 0.43        | 8.83          | 10.97         | 17.72       | 34725       |
| RoPS        | 2.63         | 0.91   | 3.21          | 2.02          | 2.98        | 0.62           | 1.02            | 1.70    | 0.35        | 0.30        | 7.91          | 10.33         | 18.65       | 40502       |
| TriSI       | 2.28         | 0.78   | 2.31          | 1.31          | 2.16        | 0.60           | 0.39            | 0.97    | 0.44        | <i>0.18</i> | 8.98          | 11.16         | 18.17       | 38161       |
|             |              |        |               |               |             | co             | mpetito         | or sche | emes        |             |               |               |             |             |
| ICP point   | 50.32        | 17.31  | 62.20         | 39.09         | 29.20       | 1.53           | 54.76           | 12.62   | 3.77        | 29.92       | -164.3        | -42.15        | 249.55      | 30.50       |
| ICP plane   | 42.71        | 14.69  | 57.96         | 36.50         | 28.71       | 0.08           | 49.43           | 10.99   | 0.45        | 29.10       | -167.5        | -30.44        | 235.93      | 31.38       |
| ICP x84     | 2.79         | 0.96   | 70.47         | 45.93         | 16.94       | 39.69          | 52.85           | 11.13   | 27.50       | 21.97       | -165.6        | -22.33        | 257.89      | 49.36       |
| S4PCS       | 151.14       | 51.99  | 151.14        | 103.35        | 46.02       | 79.36          | 114.71          | 43.40   | 45.31       | 60.85       | -155.6        | 32.60         | 342.80      | 1147        |
| S-ICP point | 0.04         | 0.01   | 20.08         | 11.44         | 0.37        | 0.05           | 20.06           | 0.24    | 0.04        | 9.05        | 0.01          | 0.01          | 17.49       | 276.68      |
| S-ICP plane | 0.04         | 0.01   | 20.08         | 11.44         | 0.37        | 0.05           | 20.06           | 0.24    | 0.04        | 9.05        | 0.01          | 0.01          | 17.49       | 327.62      |

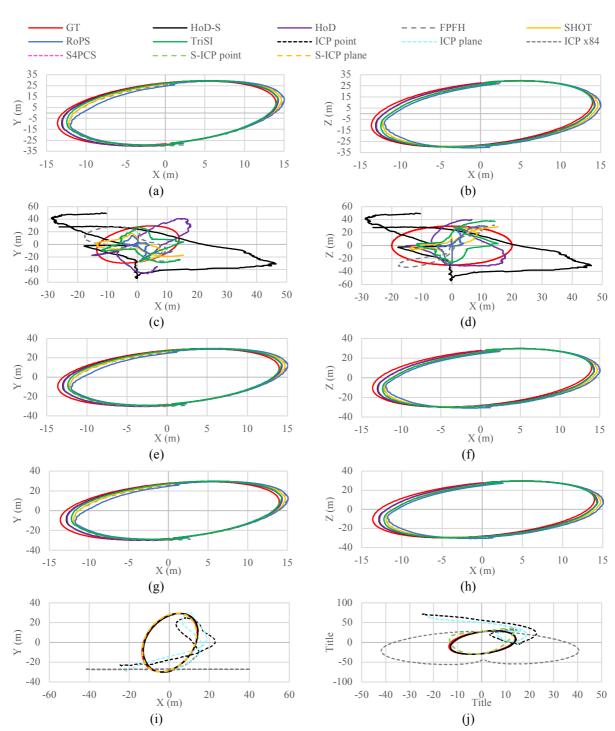


Figure 11: *Sim-Eol* scenario 3 odometry plots of the 3D descriptors combined with the adaptive filter (a)-(b)  $H\infty$ , (c)-(d) *Kalman*, (e)-(f)  $\alpha\beta$ , (g)-(h) *SDRE*, and (i)-(j) competitor methods along with the top performing proposed method HoD-S/  $\alpha\beta$  (due to large errors and for better readability we omit from (i)-(j) S4PCS). The *Kalman* filter clearly fails to provide a valid accuracy independently of the descriptor that it is combined. This is due to the Kalman parameters that are sensitive to the  $P_k$  cardinality. Competitor methods except from both S-ICP variant fail to attain accurate odometry as the  $P_k$  cardinality is below the operating threshold of ICP. Most of the proposed methods present a large error in the relatively sharp turning positions due to the combined *Source-Target* distance presenting less distinctive *Target* features.

1 Concerning the performance of the competitor methods, both S-ICP variants provide a highly

- 2 accurate odometry in an appealing execution time. The remaining competitor techniques attain an
- accuracy that is one order of magnitude larger compared to S-ICP. This is because despite this trial
- 4 having more vertices compared to the rest of the scenarios, the number of vertices is still small for
- 5 an ICP process to iterate properly (Opromolla, Fasano, et al., 2017).

In any case, it should be noted that the errors in this trial are larger compared to the real scenarios
mainly due to the length of each scenario as it is well known that odometry errors build-up as the
length of the trajectory increases. Therefore, at this point where we investigate the absolute
performance per scenario, cross comparing each method among all scenarios is not realistic.
However, in Section 4 we normalize the all the errors attained by each method and over all

11 scenarios, such as to make a cross-scenario comparison possible.

Despite a few descriptors and filtering combinations achieving an appealing accuracy, the processing time required by each combination does not pose an overall valid choice for space applications. Hence, for point clouds with a large cardinality as in this trial, adopting a subsampling scheme or utilizing a keypoint detection method shall afford a lower computational burden. However, for the sake of generalization and given that in the rest of the trials such an additional process within our architecture is not mandatory, we retain for this trail our architecture as it is and demonstrate it weakness.

# 19 3.4.2 Sim-Helical trajectory

This scenario involves synthetic data and is quite challenging due to the large curvature of the 20 trajectory in the X-Y plane, the large translational disposition in all three axes and the small Target 21 point cloud size that has an average size of only 438 vertices. This trajectory considers a 360° 22 rotation and simultaneous translation as presented in Figure 6 (d). We create self-occluded point 23 cloud views of the Target platform emulating realistic views of the virtual LIDAR placed on the 24 *Source* platform by exploiting the HPR algorithm. Even though in the context of space odometry 25 this trajectory might be extreme, we intentionally push the limits of odometry and investigate the 26 performance of the evaluated methods. Table 6 presents the detailed performance metrics, while 27 Figure 13 the error, i.e. difference of the GT trajectory and the estimated one per method, for each 28 of the three axes. For this scenario we prefer presenting the corresponding errors per method rather 29 than the estimated trajectory, due to the small errors attained by the majority of the feature 30 descriptors and recursive filtering methods. 31

From Table 6 it is evident that the HoD-S descriptor attains the lowest  $e^{RT}$  error among all 32 descriptors evaluated. Additionally, HoD-S achieves the lowest error per filter with any of the 33 filtering methods that it is combined with. Next to follow is SHOT, which poses the second-best 34 choice for each filter. From Table 6 and Figure 13 it is clear that TriSI is the least accurate 35 descriptor as it achieves the highest  $e^{RT}$  error for any of the filters evaluated. Given that RoPS and 36 TriSI share the same LRF estimation method and that RoPS gains a better odometry accuracy, the 37 encoding capability of TriSI on this scenario is limited. This is because the Spin Images descriptor 38 39 that is included in the TriSI descriptor is prone to highly sparse structures, in combination to the large frame-to-frame motion between  $P_k$  and  $P_{k+1}$ . Regarding processing efficiency, HoD-S is the 40 fastest to compute because it neglects a LRF/A estimation process. 41

|              | drift               | Terror       | Т                   | Т             | ma           | x Error             | (m)                 | Aver                | age erro  | or (m)       | т             | D            | DT             | t                 |
|--------------|---------------------|--------------|---------------------|---------------|--------------|---------------------|---------------------|---------------------|-----------|--------------|---------------|--------------|----------------|-------------------|
| Descriptor   | (m)                 | (%)          | $e_{\max}^{T}$      | $e_{avg}^{T}$ | X            | Y                   | Z                   | X                   | Y         | Z            | $e_{avg}^{T}$ | $e_{\max}^R$ | $e^{RT}$       | (ms)              |
|              |                     |              |                     |               |              |                     |                     |                     | C14 ·     |              | 1             |              |                |                   |
| LL-D C       | 1 05                | 0.00         | 2.00                | 1 (1          |              | 0.42                |                     |                     | filterin  |              | 0.09          | 0.16         | 12.55          | 127               |
| HoD-S        | <b>1.85</b><br>2.22 | <b>0.90</b>  | <b>2.09</b><br>2.90 | <b>1.61</b>   | 1.79<br>1.77 |                     | <b>1.00</b><br>2.30 | 1.28                | 0.17      | <b>0.74</b>  | 0.08          | 0.16         | <u>12.55</u>   | <b>137</b><br>620 |
| FPFH<br>SHOT | 5.89                | 1.08<br>2.86 | 2.90<br>5.92        | 2.07<br>2.17  | 3.63         | <b>0.07</b><br>4.33 | 1.64                | <b>1.04</b><br>1.67 | 0.22      | 1.65<br>0.74 | 0.08          | 0.16 0.15    | 15.81<br>13.69 | 1094              |
| HoD          | 6.27                | 3.04         | 6.27                | 3.29          | 5.05         | 4.55                | 3.08                | 2.03                | 1.27      | 1.04         | 0.08          | 0.13         | 17.55          | 997               |
| RoPS         | 2.16                | 1.05         | 2.45                | 1.83          | 1.37         | 0.33                | 1.74                | 1.20                | 0.14      | 1.04         | 0.08          | 0.14         | 14.88          | 1164              |
| TriSI        | 12.74               | 6.18         | 12.74               | 8.26          | 7.40         | 7.24                | 7.24                | 2.69                | 4.86      | 2.82         | 0.08          | 0.10<br>0.13 | 26.49          | 1042              |
| 11151        | 12.74               | 0.10         | 12.74               | 8.20          |              |                     |                     |                     | ve filter |              | 0.07          | 0.15         | 20.49          | 1042              |
| HoD-S        | 2.03                | 0.98         | 2.47                | 1.59          | 1.79         | <i>0.12</i>         | 1.70                | 1.22                | 0.23      | <b>0.</b> 77 | 0.01          | 0.01         | 13.13          | 134               |
| FPFH         | 32.38               | 15.71        | 33.74               | 14.92         | 10.05        | 5.48                | 31.74               | 2.63                | 1.12      | 8.52         | 32.61         | -179.99      |                | 619               |
| SHOT         | 5.87                | 2.85         | 5.90                | 2.16          | 3.58         | 4.38                | <b>1.57</b>         | 1.64                | 0.37      | 0.79         | <b>0.01</b>   | <b>0.01</b>  | 13.71          | 1092              |
| HoD          | 6.37                | 3.09         | 6.37                | 3.29          | 5.21         | 1.55                | 3.31                | 2.01                | 1.26      | 1.10         | 0.01          | 0.01         | 17.70          | 995               |
| RoPS         | 9.36                | 4.54         | 10.03               | 6.12          | 6.94         | 0.14                | 7.24                | 3.70                | 0.19      | 3.36         | 0.20          | 0.24         | 23.89          | 1161              |
| TriSI        | 12.84               | 6.23         | 12.84               | 8.28          | 7.42         | 7.20                | 7.37                | 2.70                | 4.85      | 2.86         | 0.01          | 0.01         | 26.52          | 1041              |
|              |                     | 0.120        |                     | 0.20          |              |                     |                     |                     | filterin  |              |               |              |                |                   |
| HoD-S        | 1.86                | 0.90         | 2.09                | 1.61          | 1.79         | 0.39                | 1.01                | 1.28                | 0.17      | 0.75         | 0.01          | 0.01         | 12.53          | 112               |
| FPFH         | 2.27                | 1.10         | 2.91                | 2.08          | 1.77         | 0.10                | 2.30                | 1.04                | 0.24      | 1.66         | 0.01          | 0.01         | 15.87          | 607               |
| SHOT         | 5.92                | 2.87         | 5.96                | 2.17          | 3.64         | 4.38                | 1.61                | 1.67                | 0.37      | 0.74         | 0.01          | 0.01         | 13.61          | 1074              |
| HoD          | 6.28                | 3.05         | 6.28                | 3.28          | 5.26         | 1.55                | 3.06                | 2.03                | 1.25      | 1.03         | 0.01          | 0.01         | 17.45          | 979               |
| RoPS         | 2.20                | 1.07         | 2.49                | 1.85          | 1.37         | 0.35                | 1.76                | 1.20                | 0.16      | 1.29         | 0.01          | 0.01         | 14.97          | 1140              |
| TriSI        | 12.73               | 6.18         | 12.73               | 8.25          | 7.41         | 7.20                | 7.23                | 2.70                | 4.85      | 2.81         | 0.01          | 0.01         | 26.43          | 1024              |
|              |                     |              |                     |               | a            | daptive             | SDRE 1              | recursiv            | e filteri | ng           |               |              |                |                   |
| HoD-S        | <i>1.81</i>         | 0.88         | 2.08                | 1.60          | 1.74         | 0.47                | 1.04                | 1.24                | 0.19      | 0.77         | 0.08          | 0.16         | 12.64          | <i>116</i>        |
| FPFH         | 2.29                | 1.11         | 2.91                | 2.08          | 1.73         | 0.03                | 2.34                | 1.01                | 0.19      | 1.68         | 0.08          | 0.16         | 15.75          | 609               |
| SHOT         | 5.78                | 2.81         | 5.82                | 2.14          | 3.57         | 4.27                | 1.58                | 1.64                | 0.38      | 0.75         | 0.08          | 0.15         | 13.69          | 1077              |
| HoD          | 6.18                | 3.00         | 6.18                | 3.27          | 5.19         | 1.44                | 3.02                | 2.00                | 1.29      | 1.03         | 0.08          | 0.14         | 17.46          | 981               |
| RoPS         | 2.20                | 1.07         | 2.48                | 1.83          | 1.15         | 0.09                | 2.18                | 1.16                | 0.13      | 1.32         | 0.08          | 0.16         | 14.82          | 1143              |
| TriSI        | 12.68               | 6.15         | 12.68               | 8.25          | 7.35         | 7.29                | 7.19                | 2.66                | 4.87      | 2.80         | 0.07          | 0.13         | 26.40          | 1027              |
|              |                     |              |                     |               | 0            |                     | mpetito             |                     |           | 0            | 1             | 1            | 0              |                   |
| ICP point    | 2.92                | 1.42         | 3.15                | 1.96          | 2.07         | 0.44                | 2.34                | 1.39                | 0.26      | 1.15         | 11.71         | 20.83        | 26.85          | 18                |
| ICP plane    | 22.70               | 11.02        | 27.08               | 11.36         | 22.61        | 10.36               | 4.70                | 5.99                | 3.35      | 2.06         | 58.66         | -96.87       | 84.62          | 89                |
| ICP x84      | 16615               | 8063         | 17277               | 9210          | 12253        | 8668                | 8333                | 1905.               | 2878      | 3333         | -132          | -15.79       | 8346           | 25                |
| S4PCS        | 147.65              | 71.65        | 155.65              | 84.13         | 46.40        | 146.59              | 24.19               | 15.94               | 64.69     | 10.21        | 109           | -169         | 207.98         | -                 |
| S-ICP point  |                     | 23.25        | 47.90               | 39.05         | 28.09        | 19.00               | 31.66               | 19.15               | 12.80     | 23.86        | 0.01          | 0.01         | 50.04          | 107               |
| S-ICP plane  | 49.32               | 23.93        | 49.32               | 40.37         | 29.40        | 19.40               | 32.86               | 20.21               | 12.96     | 24.82        | 0.01          | 0.01         | 51.00          | 105               |

Table 6: Performance metrics for the Sim-Helical scenario

We further analyze the interplay between HoD-S, which is the descriptor offering the smallest 

errors, and the filtering methods evaluated in this work, and present the results in Figure 14. From this figure we observe that  $H\infty$ ,  $\alpha\beta$  and *SDRE* have a very similar performance, with Kalman being 

less accurate especially in the Z-axis. 

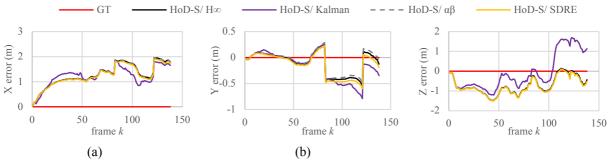


Figure 14: Sim -Helical scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric

Considering the competitor methods, the top performing ICP plane has half the accuracy of HoD-S/  $\alpha\beta$ . As already mentioned in Section 1, the proposed method can present an accurate odometry due to the feature matching and the geometric correspondence grouping schemes that provide to the recursive filter only well-established correspondences. These correspondences combined with the adaptive nature infused in the recursive filter afford an odometry trajectory with low errors. Despite that, ICP is highly processing efficient requiring only 18ms. Even though literature suggests that ICP attains a low accuracy on sparse point clouds (Opromolla, Fasano, et al., 2017) and we confirmed that in the previous trials, this trial despite being sparse, the frame-to-frame motion between  $P_k$  and  $P_{k+l}$  is such allowing ICP to settle to a more accurate solution. 

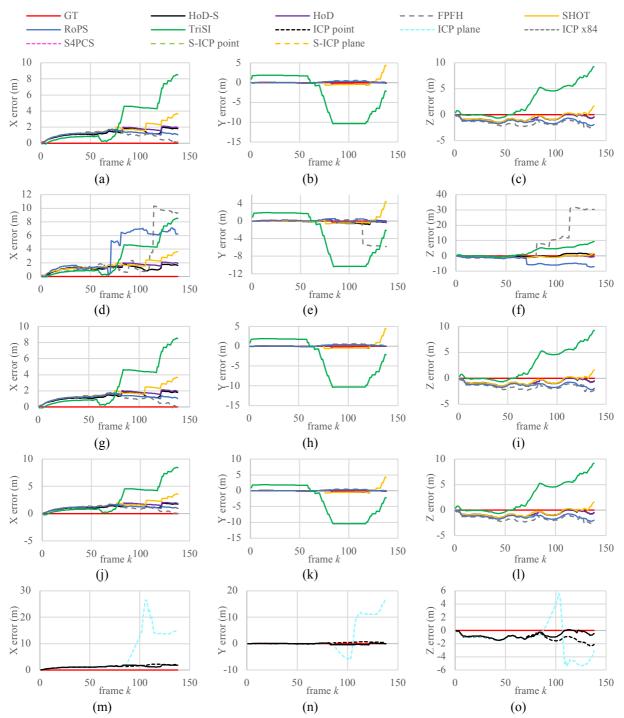


Figure 13: *Sim- Helical* odometry error plots of the 3D descriptors combined with the adaptive filter (a)-(c)  $H\infty$ , (d)-(f) *Kalman*, (g)-(i)  $\alpha\beta$ , (j)-(l) *SDRE*, and (m)-(o) competitor methods along with the top performing proposed method HoD-S/  $\alpha\beta$  (due to large errors and for better readability we omit ICP x84, S-ICP point, S-ICP plane and S4PCS from (m)-(o)). The large frame-to-frame motion combined with the highly sparse  $P_k$  prevent TriSI from providing an accurate odometry. Despite the sparse nature of  $P_k$  ICP point presents an odometry that is more accurate to the rest of the competitor methods.

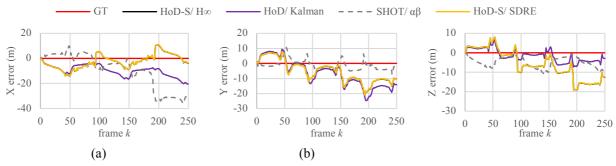
#### 1 3.4.3 Sim-Voyager trajectory

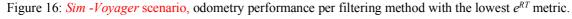
This scenario considers the *Source* platform orbiting in an ellipsoidal trajectory around the Voyager space platform. This is a synthetic scenario with an average  $P_k$  cardinality of 190 vertices, where the various *Target* platform poses are created using the HPR algorithm. In order to assess the performance our architecture on repetitive trajectories, this scenario considers the *Source* platform moving along the ellipsoidal trajectory 2.5 times. Thus, in contrast to the trajectories evaluated so far, this is the longest one with a GT length of 788 meters.

The results on this scenario are presented in Table 7 and Figure 15. As expected, due to the long 8 trajectory length evaluated here, the performance of al methods is substantially higher. However, 9 as already stated, a direct cross-scenario performance comparison is biased towards the shortest 10 trajectories. Hence, in Section 4, we normalize the performance of each method such as to make it 11 independent of the distance travelled and thus make a cross-scenario performance comparison 12 feasible. The performance achieved by each method is quite similar among the filters evaluated. 13 This demonstrates that establishing correct feature matches is very important as miss-matches will 14 negatively influence the odometry output of the filter. However, as demonstrated in Section 34.1, 15 for the Kalman filter the training and testing scenarios should involve a *Target* with a similar level 16 of sparsity. Optimum scheme is the SHOT/  $\alpha\beta$ , while the overall tope performing descriptor is 17 SHOT with HoD following closely. However, due to the large computational burden of SHOT and 18 given that the next best performing combination is HoD-S/ SDRE that is also 10 times faster to 19 execute, we select the latter as the optimum method. Considering the performance of the filtering 20 methods, the overall top performing is  $H\infty$  with  $\alpha\beta$  being the next optimum choice. In terms of 21 processing efficiency, once again HoD-S and HoD are the fastest to compute. The least accurate 22 23 method is HoD-S/ Kalman posing large translational and rotational errors.

Figure 16 presents the performance of the most appealing schemes per filtering method, where we observe that SHOT/  $\alpha\beta$  shows a substantial accuracy drop in the X-axis after frame 200, i.e. after two complete ellipsoidal translations. Additionally, Figure 16 highlights that all methods present

a repetitive error that coincides with the corresponding relative *Source – Target* position.





28

29 Considering the competitor methods, ICP point attains an  $e^{RT}$  error that is close but inferior to the

30 well performing proposed combinations, with ICP plane following. However, as expected, both

31 these ICP variants are much faster to execute. Despite the average  $P_k$  cardinality is only 190, both

32 S-ICP variants are less accurate than their standard ICP counterparts because  $P_k$  is not sparse.

33 Interestingly, all errors are sinusoidal-based that coincides with the relative Source-Target

# position. This is more evident for the S4PCS, where the error amplitude is the highest presented in Figure 15 (m)-(o).

Table 7: Performance metrics for the Sim-Voyager scenario

| Descriptor  | drift<br>(m)                               | Terror<br>(%) | $e_{\max}^{T}$ | $e_{avg}^{T}$ |             | x Error | < <i>/</i>      | Aver          | age erro | or (m)      | $e_{\max}^R$ | $e_{avg}^{T}$ | $e^{RT}$     | t<br>(ms) |
|-------------|--|---------------|----------------|---------------|-------------|---------|-----------------|---------------|----------|-------------|--------------|---------------|--------------|-----------|
|             | (III)                                      | (70)          |                | urs           | Х           | Y       | Z               | Х             | Y        | Z           |              |               |              |           |
|             |  |               |                |               |             | a       | daptive         | <i>H</i> ∞ re | cursive  | filterin    | g            |               |              |           |
| HoD-S       | 16.59                                      | 2.10          | 28.76          | 14.27         | 10.68       | 18.79   | 18.97           | 5.12          | 7.50     | 7.54        | 0.14         | 0.27          | 40.91        | 66        |
| FPFH        | 104  | 13.24         | 105            | 62.86         | 28.27       | 50.14   | 88.19           | 11.47         | 29.59    | 47.60       | 0.13         | 0.26          | 97.43        | 438       |
| SHOT        | 33.35                                      | 4.23          | 38.02          | 18.05         | 9.55        | 36.17   | 6.80            | 4.84          | 12.11    | 2.63        | 0.13         | 0.25          | 42.38        | 599       |
| HoD         | 24.31                                      | 3.08          | 27.71          | 15.36         | 19.58       | 18.44   | 6.63            | 9.25          | 9.04     | 3.18        | 0.13         | 0.26          | 41.68        | 103       |
| RoPS        | 21.66                                      | 2.75          | 31.10          | 16.00         | 12.20       | 19.09   | 14.14           | 5.68          | 10.79    | 5.79        | 0.14         | 0.27          | 43.15        | 398       |
| TriSI       | 22.87                                      | 2.90          | 39.56          | 22.20         | 12.54       | 29.45   | 23.24           | 7.13          | 13.09    | 12.63       | 0.08         | 0.16          | 46.39        | 336       |
|             |  |               |                |               |             | ada     | aptive <i>K</i> | alman         | recursiv | ve filter   | ing          |               |              |           |
| HoD-S       | 10.34                                      | 1.31          | 55.07          |               | 52.30       | 12.06   | 2.33            | 13.55         | 6.65     | 4.64        | 95.19        | -162.41       | 140.12       | 66        |
| FPFH        | 93.16                                      | 11.82         | 93.21          |               | 32.86       | 35.56   | 79.65           | 13.70         | 24.50    | 46.74       | 0.10         | 0.20          | 94.85        | 438       |
| SHOT        | 34.55                                      | 4.38          | 39.12          | 18.30         |             | 37.61   | 6.37            | 4.43          | 12.13    | 2.46        | 0.18         | 0.40          | 45.20        | 598       |
| HoD         | 25.04                                      | 3.18          | 28.35          | 15.74         |             | 18.81   | 6.20            | 9.67          | 9.18     | 3.03        | 0.01         | 0.02          | <i>41.79</i> | 102       |
| RoPS        | 21.99                                      | 2.79          | 28.41          | 17.71         | 19.10       | 12.94   | 15.49           | 8.05          | 5.87     | 11.90       | 24.21        | 92.37         | 71.60        | 397       |
| TriSI       | 22.50                                      | 2.85          | 38.94          | 22.09         | 12.59       | 29.27   | 22.39           | 7.14          | 13.07    | 12.61       | 1.19         | 2.98          | 47.58        | 335       |
|             | adaptive $\alpha\beta$ recursive filtering |               |                |               |             |         |                 |               |          |             |              |               |              |           |
| HoD-S       | 15.77                                      | 2.00          | 28.03          | <i>13.83</i>  |             | 18.03   | 18.63           | 5.11          | 7.05     | 7.35        | 1.88         | 3.58          | 41.68        | 57        |
| FPFH        | 104  | 13.24         | 105            | 62.86         | 28.27       | 50.14   | 88.19           | 11.47         | 29.59    | 47.60       | <i>0.13</i>  | 0.26          | 97.43        | 438       |
| SHOT        | 33.36                                      | 4.23          | 38.03          | 17.89         | <i>9.82</i> | 36.00   | 7.32            | 5.00          | 11.89    | <i>2.81</i> | 1.53         | 3.09          | 38.19        | 595       |
| HoD         | 24.29                                      | 3.08          | 27.49          | 15.18         | 20.09       | 17.70   | <i>6.21</i>     | 9.44          | 8.67     | 3.04        | 2.23         | 4.51          | 43.13        | 91        |
| RoPS        | 22.08                                      | 2.80          | 30.72          | 16.08         | 12.71       | 18.64   | 14.88           | 5.98          | 10.57    | 6.18        | 1.03         | 1.97          | 44.68        | 390       |
| TriSI       | 22.93                                      | 2.91          | 39.64          | 22.22         | 12.55       | 29.36   | 23.50           | 7.11          | 13.07    | 12.67       | 0.80         | 1.50          | 47.06        | 331       |
|             |  |               | -              | _             | _           |         |                 |               | ecursiv  |             |              |               |              |           |
| HoD-S       | <i>16.41</i>                               | 2.08          | 28.67          | 14.20         |             | 18.70   | 18.88           | 5.12          | 7.45     | 7.49        | 0.14         | 0.27          | <i>40.78</i> | 57        |
| FPFH        | 104  | 13.23         | 105            | 62.83         | 28.16       | 50.26   | 88.08           | 11.42         | 29.65    | 47.54       | 0.13         | 0.26          | 97.38        | 435       |
| SHOT        | 33.21                                      | 4.21          | 37.87          | 17.98         | 9.44        | 36.06   | 6.69            | <b>4.79</b>   | 12.06    | 2.61        | 0.13         | 0.25          | 41.23        | 595       |
| HoD         | 24.14                                      | 3.06          | 27.52          | 15.26         |             | 18.33   | 6.52            | 9.19          | 8.99     | 3.13        | 0.13         | 0.26          | 41.52        | 91        |
| RoPS        | 21.46                                      | 2.72          | 30.98          | 15.91         | 12.09       | 18.98   | 14.03           | 5.63          | 10.74    | 5.74        | 0.14         | 0.27          | 42.99        | 391       |
| TriSI       | 22.85                                      | 2.90          | 39.50          | 22.18         | 12.60       | 29.39   | 23.18           | 7.16          | 13.08    | 12.62       | 0.08         | 0.16          | 46.42        | 332       |
|             |  |               |                |               |             |         |                 |               | or schen |             |              |               |              |           |
| ICP point   | 9.52                                       | 1.21          | 21.03          | 11.22         | 4.93        | 19.40   | 6.43            | 4.48          | 6.37     | 2.91        | 19.22        | 34.10         | 55.27        | 15        |
| ICP plane   | 11.15                                      | 1.41          | 26.18          | 13.30         |             | 23.66   | 10.27           | 3.92          | 8.38     | 4.26        | 41.48        | 75.56         | 80.69        | 16        |
| ICP x84     | 80.60                                      | 10.22         | 80.60          | 61.73         |             | 58.43   | 15.68           | 43.74         | 24.99    | 9.27        | 147.65       | -160          | 234.32       | 17        |
| S4PCS       | 39.98                                      | 5.07          | 50.32          | 38.59         |             | 30.43   | 30.39           | 20.14         | 18.90    | 18.91       | 1.65         | 1.65          | 52.48        | 136       |
| S-ICP point | 28.94                                      | 3.67          | 38.45          | 29.50         |             | 14.80   | 28.40           | 14.82         | 12.27    | 16.18       | 0.01         | 0.01          | 46.33        | 171       |
| S-ICP plane | 28.94                                      | 3.67          | 38.45          | 29.50         | 21.24       | 14.80   | 28.40           | 14.82         | 12.27    | 16.18       | 0.01         | 0.01          | 46.33        | 177       |

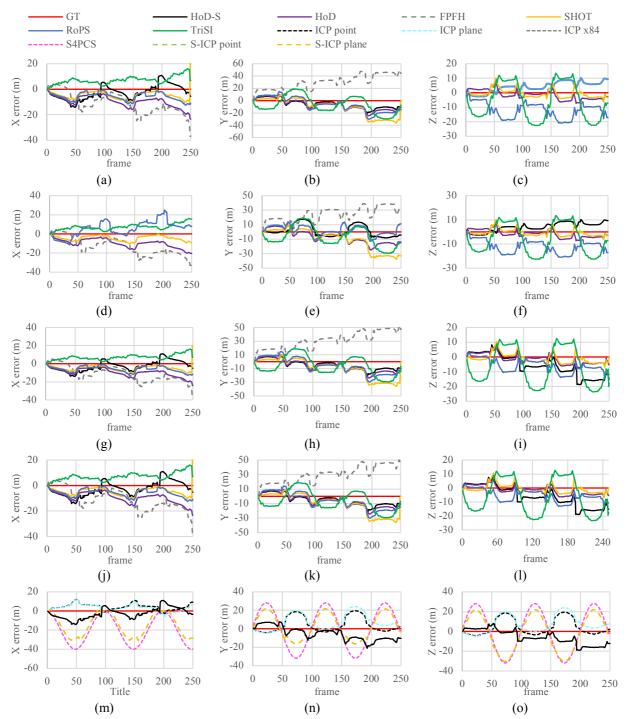


Figure 15: *Sim-Voyager* scenario 5 odometry error plots of the 3D descriptors combined with the adaptive filter (a)-(c)  $H\infty$ , (d)-(f) *Kalman*, (g)-(i)  $\alpha\beta$ , (j)-(l) *SDRE*, and (m)-(o) competitor methods and top performing proposed method HoD-S/ SDRE (due to large errors and for better readability we omit FPFH from Z error plots, HoD-S from (d) and ICP x84 from (m)-(o))

#### 1 3.4.4 Sim-Orion trajectory

This scenario is identical to the Sim-Voyager, but the Voyager satellite is substituted with the Orion 2 space capsule. Main characteristics of this trial are the flat surfaces of Orion that include less 3 distinctive features. The average  $P_k$  cardinality is 288. In terms of performance, Table 8 and Figure 4 17 demonstrate that SHOT and RoPS provide the smallest  $e^{RT}$  errors with the former combined 5 with the Kalman filter being the optimum choice for this scenario. In contrast to the previous 6 scenarios, HoD and HoD-S perform poor highlighting that for point clouds that are mainly flat 7 with poor distinctive features neglecting a LRF/A has a negative impact on the feature matching 8 9 process. Similarly to the *Sim-Voyager* scenario, guite a few descriptor and filtering combination present the sinusoidal error. Due to the challenging nature of this scenario, HoD, HoD-S and TriSI 10 present quite large errors and thus for the sake of readability these descriptors are neglected from 11 12 several plots in Figure 17. In Figure 18 we present the top performing descriptor per filtering method. Interestingly, this figure indicates that all RoPS descriptors attain almost the same 13 performance independently of the filter. Additionally, all RoPS based solutions and the SHOT/ 14 Kalman achieve a similar performance in the Y-axis. 15

Considering the competitor methods, these are of inferior accuracy to the majority of the feature
descriptor / recursive filtering combinations of the proposed method. Specifically, both ICP
variants present a low translational error but due to their low rotational accuracy, these cannot be
considered as overall optimum choices. On the contrary, S4PCS and both S-ICP variants attain

20 low rotational errors and large translational errors.

21

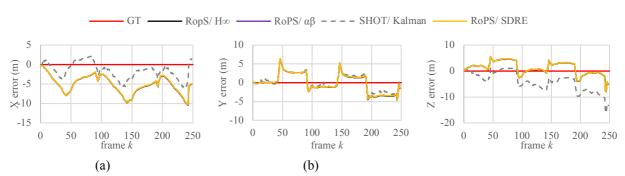


Figure 18: *Sim -Orion* scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric along with the overall top performing in terms of accuracy and processing efficiency HoD-S/ *SDRE* 

22

- 23
- 24
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- 27

|  |       |             |                |               |       |                 |               |             |             | n seend |               | -             |          |            |
|--|-------|-------------|----------------|---------------|-------|-----------------|---------------|-------------|-------------|---------|---------------|---------------|----------|------------|
| Descriptor                                 | drift | Terror      | $e_{\max}^{T}$ | $e_{avg}^{T}$ |       | x Error         | (m)           |             | rage err    |         | $e_{\max}^R$  | $e_{avg}^{T}$ | $e^{RT}$ | t(ms)      |
| Descriptor                                 | (m)   | (%)         | $e_{\rm max}$  | eavg          | Х     | Y               | Z             | Х           | Y           | Ζ       | $e_{\rm max}$ | eavg          | е        | t (ms)     |
|  |       |             |                |               | 9     | dantive         | <i>H</i> ∞ re | cursive     | filteri     | nσ      |               |               |          |            |
| HoD-S                                      | 109   | 13.84       | 111            | 64.28         | 7.72  | 4.21            | 109           | <b>3.61</b> | 3.89        | 54.45   | 0.14          | 0.27          | 70.76    | 156        |
| FPFH                                       | 12.22 | 1.55        | 14.74          | 8.72          | 8.50  | 3.27            | 9.86          | 5.06        | <b>1.97</b> | 5.12    | 0.14          | 0.27          | 30.19    | 720        |
| SHOT                                       | 9.43  | 1.20        | 11.94          | 5.91          | 7.39  | 7.08            | 6.16          | 3.08        | 2.59        | 2.74    | 0.14          | 0.27          | 26.93    | 859        |
| HoD  | 118   | 14.97       | 138            | 78.47         | 79.15 | 81.10           | 78.99         |             | 33.68       | 32.72   | 0.03          | 0.06          | 101      | 169        |
| RoPS                                       | 7.30  | 0.93        | 11.33          | 6.70          | 7.21  | 6.38            | 5.56          | 5.13        | 2.03        | 2.27    | 0.14          | 0.27          | 26.46    | 1514       |
| TriSI                                      | 77.47 | 9.83        | 85.93          | 50.77         | 65.86 | 39.21           | 38.37         | 38.10       | 16.16       | 16.04   | 0.06          | 0.12          | 67.97    | 1159       |
| 11101                                      | ,,,   | 2.00        | 00.70          | 00.77         |       |                 | alman         |             |             |         | 0.00          | 0.12          | 07.27    | 1109       |
| HoD-S                                      | 29.37 | 3.73        | 37.06          | 25.17         | 19.83 | 6.74            | 28.52         | 11.48       | 5.03        | 18.05   | 50.37         | -159          | 94.00    | 156        |
| FPFH                                       | 11.88 | 1.51        | 14.59          | 8.70          | 7.58  | 3.41            | 10.38         | 4.63        | 2.02        | 5.34    | 0.01          | 0.01          | 29.85    | 719        |
| SHOT                                       | 8.46  | 1.07        | 10.76          | 5.32          | 5.72  | 6.80            | 6.07          | 2.44        | 2.29        | 2.65    | 0.01          | 0.01          | 24.25    | 858        |
| HoD  | 118   | 14.98       | 138            | 78.50         | 79.24 | 81.09           | 78.99         |             |             | 32.72   | 0.01          | 0.01          | 101      | 169        |
| RoPS                                       | 13.40 | 1.70        | 16.59          | 6.44          | 0.89  | 3.53            | 16.19         | 2.14        | 1.90        | 4.33    | 0.10          | 0.22          | 24.69    | 1513       |
| TriSI                                      | 77.59 | 9.84        | 86.05          | 50.82         |       | 39.19           | 38.42         | 38.15       |             | 16.05   | 0.01          | 0.01          | 67.95    | 1158       |
| adaptive $\alpha\beta$ recursive filtering |       |             |                |               |       |                 |               |             |             |         |               |               |          |            |
| HoD-S                                      | 109   | 13.91       | 111            | 64.50         | 7.66  | 4.07            | 110           | 3.59        | 3.90        | 54.62   | 0.05          | 0.10          | 70.84    | <i>146</i> |
| FPFH                                       | 12.29 | 1.56        | 14.77          | 8.75          | 8.55  | 3.35            | 9.85          | 5.09        | 2.00        | 5.12    | 0.07          | 0.13          | 30.28    | 711        |
| SHOT                                       | 9.55  | 1.21        | 11.98          | 5.96          | 7.39  | 7.09            | 6.21          | 3.10        | 2.63        | 2.79    | 0.11          | 0.22          | 26.99    | 845        |
| HoD  | 118   | 14.97       | 138            | 78.50         | 79.19 | 81.09           | 79.04         | 48.39       | 33.68       | 32.74   | 0.01          | 0.03          | 101      | 166        |
| RoPS                                       | 7.24  | <i>0.92</i> | 11.40          | 6.72          | 7.23  | 6.39            | 5.61          | 5.15        | 2.01        | 2.28    | 0.09          | 0.19          | 26.46    | 1503       |
| TriSI                                      | 77.54 | 9.84        | 86.01          | 50.80         | 65.92 | 39.23           | 38.41         | 38.12       | 16.17       | 16.05   | 0.03          | 0.05          | 67.95    | 1154       |
|  |       |             |                |               | ada   | aptive <b>J</b> | SDRE 1        | ecursiv     | ve filter   | ring    |               |               |          |            |
| HoD-S                                      | 109   | 13.83       | 111            | 64.22         | 7.83  | 4.09            | 109           | 3.65        | 3.90        | 54.39   | 0.14          | 0.27          | 70.74    | 147        |
| FPFH                                       | 12.12 | 1.54        | 14.59          | 8.66          | 8.39  | 3.38            | 9.74          | 5.00        | 2.02        | 5.08    | 0.14          | 0.27          | 30.24    | 712        |
| SHOT                                       | 9.53  | 1.21        | 11.95          | 5.94          | 7.36  | 7.10            | 6.18          | 3.05        | 2.64        | 2.79    | 0.14          | 0.27          | 26.60    | 846        |
| HoD  | 118   | 14.97       | 138            | 78.46         | 79.18 | 81.07           | 78.97         | 48.39       | 33.67       | 32.71   | 0.03          | 0.06          | 101      | 168        |
| RoPS                                       | 7.11  | 0.90        | 11.33          | 6.65          | 7.19  | 6.40            | 5.58          | 5.07        | 2.01        | 2.27    | 0.14          | 0.27          | 26.40    | 1504       |
| TriSI                                      | 77.50 | 9.83        | 85.93          | 50.78         | 65.91 | 39.16           | 38.32         | 38.12       | 16.15       | 16.03   | 0.06          | 0.12          | 68.01    | 1155       |
|  | _     |             |                |               | -     |                 | mpetito       |             |             |         |               |               | _        |            |
| ICP point                                  | 13.90 | 1.76        | 16.75          | 9.38          | 6.71  | 11.50           | 8.08          | 4.63        | 5.09        | 3.41    |               |               | 262.48   |            |
| ICP plane                                  | 11.54 | 1.46        | 12.59          | 8.64          | 8.10  | 3.02            | 8.79          | 4.62        | 1.80        | 4.91    |               |               | 267.53   | 50         |
| ICP x84                                    | 88.92 | 11.28       | 127.39         | 66.46         | 89.92 | 1.62            | 90.21         | 26.43       |             | 37.32   |               |               | 277.57   | 24         |
| S4PCS                                      | 54.65 | 6.93        | 65.76          | 43.33         | 39.43 | 37.30           | 37.11         | 27.31       | 19.49       | 19.47   | 0.54          | 1.07          | 60.24    | 1641       |
| S-ICP point                                |       | 3.80        | 46.69          | 32.92         | 20.57 | 28.57           | 30.31         | 15.04       |             | 16.66   | 0.01          | 0.01          | 48.12    | 125        |
| S-ICP plane                                | 29.98 | 3.80        | 46.69          | 32.92         | 20.57 | 28.57           | 30.31         | 15.04       | 17.15       | 16.66   | 0.01          | 0.01          | 48.12    | 133        |

Table 8: Performance metrics for the Sim-Orion scenario

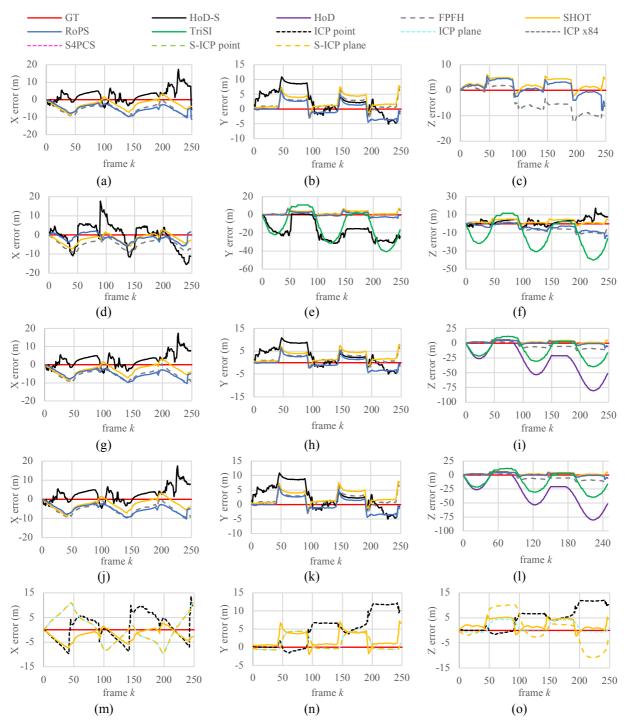


Figure 17: *Sim-Orion* scenario 6 odometry plots of the 3D descriptors combined with the adaptive filter (a)-(b)  $H\infty$ , (c)-(d) *Kalman*, (e)-(f)  $\alpha\beta$ , (g)-(h) *SDRE*, and (i)-(j) competitor methods and top performing proposed method SHOT/ *Kalman* (due to large errors and for better readability we omit HoD from (a), (b), (c), (d), (e), (f), (g), (h), (j), (k), HoD-S from (c), (i), (l), TriSI from (a), (b), (c), (d), (g), (h), (j), (k), and S4PCS, Sparse ICP point2point and ICP x84 from (m)-(o))

#### 1 3.4.5 Sim-Bennu trajectory

2 This also the same trajectory to the Sim-Voyager and Sim-Orion but considers the Bennu asteroid as the *Target* object. The main challenge of this trial is the very small average point cloud 3 cardinality which is only 151. The results obtained are presented in Figure 19 and Table 9, where 4 it is evident that for all filters but Kalman, HoD-S is the optimum choice. This is because, in 5 contrast to the *Sim-Orion* scenario where the *Target* involves perfectly flat surfaces, the surfaces 6 of Bennu despite being smooth, these still allow for HoD-S to efficiently encode the local region 7 where it is applied. Considering the Kalman filter, FPFH attains the lowest  $e^{RT}$  error. However, it 8 9 is obvious from Figure 20 that FPFH/ Kalman presents a relatively large periodic translational error, and thus this combination cannot be considered as an optimum choice. This error is because 10 the FPFH descriptor lacks providing geometrically consistent point pair correspondences and thus 11 12 the FPFH feature matches are rejected by the GCC module, forcing the proposed architecture to 13 proceed with the initialization  $R^*$ , i.e. a unity rotation matrix and a zero-translation matrix.

Similarly to the previous trials, the competitor method do not pose an optimum choice as these do not offer a balanced rotational and translational error, forcing the  $e^{RT}$  error to be quite large.



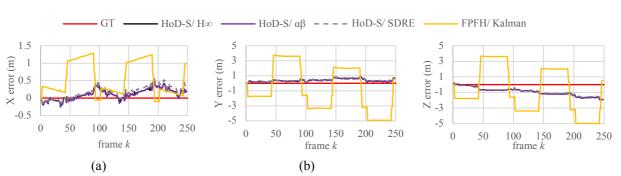
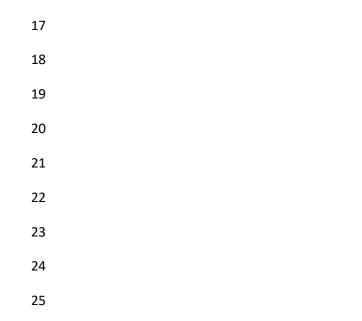


Figure 20: *Sim -Bennu* scenario, odometry performance per filtering method with the lowest  $e^{RT}$  metric along with the overall top performing in terms of accuracy and processing efficiency HoD-S/ *SDRE* 



| Decorintor  | drift                                      | Terror      | $e_{\max}^{T}$ | $a^T$         | max         | x Error | (m)         | Aver        | age erro    | r (m)  | $e_{\max}^{R}$ | $e_{avg}^{T}$ | $e^{RT}$     | t (ms) |
|-------------|--|-------------|----------------|---------------|-------------|---------|-------------|-------------|-------------|--------|----------------|---------------|--------------|--------|
| Descriptor  | (m)  | (%)         | $e_{\rm max}$  | $e_{avg}^{T}$ | Х           | Y       | Ζ           | Х           | Y           | Ζ      |                |               |              |        |
|             |  |             |                |               |             | adanti  | ve Hm       | recurs      | ive filter  | inσ    |                |               |              |        |
| HoD-S       | 2.02                                       | 0.26        | 2.04           | 1.15          | 0.21        | 0.64    | 1.93        | 0.15        | 0.38        | 0.92   | 0.14           | 0.28          | 10.76        | 47     |
| FPFH        | 3.41                                       | 0.43        | 5.59           | 3.67          | 0.21        | 4.31    | 3.43        | 0.52        | 1.97        | 2.22   | 0.14           | 0.27          | 18.12        | 440    |
| SHOT        | 1.22                                       | 0.15        | 7.05           | 4.54          | 0.25        | 4.98    | 4.99        | 0.58        | 2.89        | 2.92   | 0.13           | 0.26          | 22.72        | 516    |
| HoD         | 77.69                                      | 9.85        | 104            | 56.85         | 40.82       | 67.82   | 67.71       | 27.89       | 27.51       | 27.46  | 0.03           | 0.06          | 69.37        | 53     |
| RoPS        | 11.07                                      | 1.40        | 11.08          | 6.19          | 1.73        | 7.16    | 8.26        | 0.76        | 2.95        | 3.56   | 0.14           | 0.28          | 20.72        | 591    |
| TriSI       | 50.19                                      | 6.37        | 55.81          | 39.46         | 36.34       | 29.85   | 29.83       | 25.40       | 17.93       | 17.93  | 0.03           | 0.06          | 59.38        | 457    |
|             | adaptive Kalman recursive filtering        |             |                |               |             |         |             |             |             |        |                |               |              |        |
| HoD-S       | 8.67                                       | 1.10        | 29.09          | 16.80         | 9.38        | 24.27   | 12.99       | 3.68        | 11.23       | 6.43   | 0.02           | 0.08          | 40.24        | 46     |
| FPFH        | 3.40                                       | 0.43        | 5.57           | 3.67          | <i>0.21</i> | 4.32    | 3.42        | 0.52        | <i>1.96</i> | 2.22   | 0.01           | 0.01          | <i>17.96</i> | 439    |
| SHOT        | 1.20                                       | 0.15        | 7.06           | 4.54          | 0.25        | 4.98    | 4.99        | 0.57        | 2.89        | 2.92   | 0.01           | 0.01          | 22.57        | 516    |
| HoD         | 77.69                                      | 9.85        | 104            | 56.85         | 40.83       | 67.82   | 67.70       | 27.89       | 27.51       | 27.46  | 0.01           | 0.01          | 69.34        | 53     |
| RoPS        | 11.07                                      | 1.40        | 11.08          | 6.19          | 1.74        | 7.15    | 8.27        | 0.76        | 2.95        | 3.56   | 0.01           | 0.01          | 20.59        | 590    |
| TriSI       | 50.19                                      | 6.37        | 55.82          | 39.46         | 36.34       | 29.86   | 29.83       | 25.40       | 17.93       | 17.93  | 0.01           | 0.01          | 59.35        | 456    |
|             | adaptive $\alpha\beta$ recursive filtering |             |                |               |             |         |             |             |             |        |                |               |              |        |
| HoD-S       | 2.04                                       | 0.26        | 2.05           | 1.16          | 0.20        | 0.64    | <i>1.94</i> | <i>0.15</i> | 0.38        | 0.93   | 0.01           | 0.01          | 10.65        | 41     |
| FPFH        | 3.42                                       | 0.43        | 5.59           | 3.67          | 0.21        | 4.32    | 3.42        | 0.52        | 1.97        | 2.23   | 0.01           | 0.01          | 17.96        | 437    |
| SHOT        | 1.21                                       | 0.15        | 7.06           | 4.54          | 0.25        | 4.98    | 4.99        | 0.57        | 2.90        | 2.92   | 0.01           | 0.01          | 22.58        | 509    |
| HoD         | 77.71                                      | 9.86        | 104            | 56.85         | 40.84       | 67.83   | 67.71       | 27.90       | 27.52       | 27.46  | 0.01           | 0.01          | 69.35        | 51     |
| RoPS        | 11.07                                      | 1.40        | 11.09          | 6.19          | 1.74        | 7.15    | 8.27        | 0.76        | 2.95        | 3.56   | 0.01           | 0.01          | 20.58        | 583    |
| TriSI       | 50.20                                      | 6.37        | 55.83          | 39.47         | 36.36       | 29.86   | 29.83       | 25.40       | 17.93       | 17.93  | 0.01           | 0.01          | 59.35        | 453    |
|             |  |             |                |               | a           | daptiv  | e SDRI      | E recur     | sive filte  | ering  |                |               |              |        |
| HoD-S       | 1.97                                       | 0.25        | <i>1.98</i>    | 1.12          | 0.33        | 0.76    | 1.80        | 0.21        | <i>0.44</i> | 0.86   | 0.14           | 0.28          | 11.14        | 42     |
| FPFH        | 3.54                                       | 0.45        | 5.69           | 3.68          | 0.30        | 4.41    | 3.52        | 0.50        | 1.96        | 2.22   | 0.14           | 0.27          | 18.09        | 437    |
| SHOT        | 1.40                                       | <i>0.18</i> | 6.92           | 4.51          | 0.34        | 4.89    | 4.89        | 0.62        | 2.88        | 2.91   | 0.13           | 0.26          | 22.83        | 509    |
| HoD         | 77.68                                      | 9.85        | 104            | 56.84         | 40.84       | 67.79   | 67.69       | 27.90       | 27.50       | 27.45  | 0.03           | 0.06          | 69.37        | 52     |
| RoPS        | 10.88                                      | 1.38        | 10.90          | 6.09          | 1.61        | 7.03    | 8.15        | 0.71        | 2.91        | 3.50   | 0.14           | 0.28          | 20.46        | 584    |
| TriSI       | 50.21                                      | 6.37        | 55.80          | 39.47         | 36.37       | 29.83   | 29.81       | 25.41       | 17.93       | 17.93  | 0.03           | 0.06          | 59.39        | 453    |
|             |  | -           |                | -             |             |         |             | itor sch    | nemes       |        |                |               |              |        |
| ICP point   | 150  |             |                |               |             | 194.21  |             |             | 90.65       | 79.85  | -143           | 38.05         | 458.55       | 13     |
| ICP plane   | 39.90                                      | 5.06        | 52.43          | 38.27         | 25.85       | 32.17   | 32.21       | 19.93       | 18.58       | 18.62  | 0.01           | 0.01          | 50.07        | 82     |
| ICP x84     | 219  |             |                |               |             | 349.77  |             | 160         |             | 152.07 | -146           |               | 653.59       | 35     |
| S4PCS       | 22.72                                      | 2.88        |                | 20.89         |             |         | 23.09       | 9.07        | 10.72       | 10.35  | 81.95          | 172.80        | 125.48       | 1137   |
| S-ICP point |  | 5.06        | 52.43          |               | 25.85       | 32.17   | 32.21       | 19.93       | 18.58       | 18.62  | 0.01           | 0.01          | 50.07        | 99     |
| S-ICP plane | 39.90                                      | 5.06        | 52.43          | 38.27         | 25.85       | 32.17   | 32.21       | 19.93       | 18.58       | 18.62  | 0.01           | 0.01          | 50.07        | 112    |

Table 9: Performance metrics for the Sim-Bennu scenario

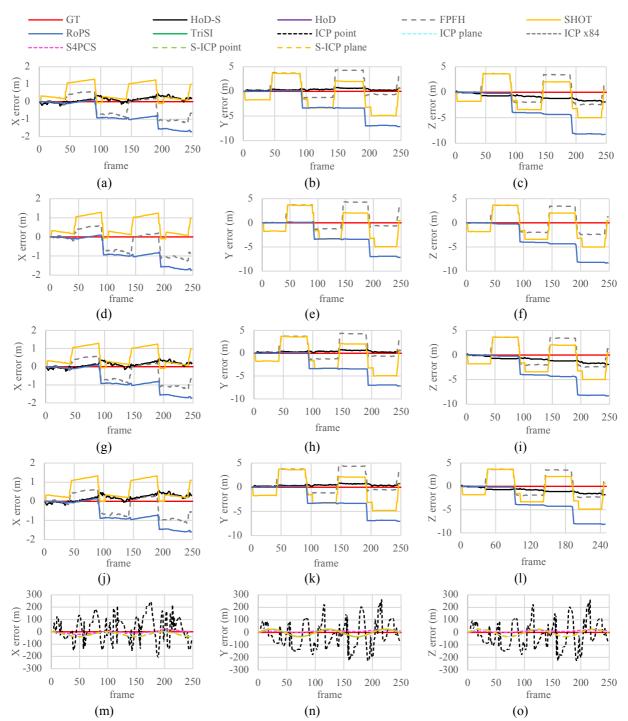


Figure 19: *Sim-Bennu* scenario 7 odometry plots of the 3D descriptors combined with the adaptive filter (a)-(b)  $H\infty$ , (c)-(d) *Kalman*, (e)-(f)  $\alpha\beta$ , (g)-(h) *SDRE*, and (i)-(j) competitor methods (due to large errors and for better readability we omit HoD and TriSI from all plots, HoD-S from (d)-(f) and ICP-x84 from (m)-(o). We also omit the top performing HoD-S/  $\alpha\beta$  from (m)-(o) as errors compared to competitor methods are at least one order of magnitude lesser)

### 1 4. Discussion

In Section 3 we presented the odometry performance of several feature descriptors and recursive 2 filtering combinations against several competitor methods. Trials involved seven scenarios that 3 included real and simulated point cloud data. In this section we further analyze the contribution of 4 each descriptor and filtering method to the odometry performance based on the normalized  $e^{RT}$ . 5 6 Normalization is performed by dividing all  $e^{RT}$  metrics by the worst  $e^{RT}$  per filter or descriptor depending on the evaluation. This normalization is done for each scenario. In order to cross-7 compare the normalized  $e^{RT}$  between the different scenarios we also divide it with the ground truth 8 distance of each scenario. This is important as it is well known that odometry errors build up with 9 distance and therefore cross-comparing  $e^{RT}$  across all scenarios is only possible if it is normalized 10 for the distance travelled. For better readability of the plots we use a logarithmic scale and in order 11 to compensate for values that are less than one, we scale the normalized  $e^{RT}$  errors by multiplying 12 them with a fixed constant. Additionally, in order to highlight the performance improvement only 13 when the descriptor can provide true matches, we discard the descriptor with the lowest odometry 14 accuracy. 15

#### 16 4.1 Feature description performance analysis

Figure 21 presents the average normalized  $e^{RT}$  metric of all recursive filters evaluated in this work 17 per feature and per scenario vs. the total processing time required by the entire odometry 18 architecture. This is important because for odometry applications the trajectory accuracy and the 19 computational burden are equally important. In Figure 21 the color of the marker is related to the 20 scenario, while the shape to the descriptor. Identifying the overall most appealing descriptor is not 21 an easy task because the performance of each descriptor varies for each scenario depending on the 22 characteristics of the trajectory, i.e. Source - Target range, frame-to-frame Target motion, and on 23 24 the complexity of the *Target* structure. Figure 21 demonstrates that the average normalized  $e^{RT}$  for each descriptor is of the same order, with only minor differences. However, in terms of processing 25 efficiency, the descriptors impose a different processing time that is governed by several 26 27 parameters including the individual features of each scenario, i.e. level of sparsity, the robustness 28 of each descriptor, the number of geometrically consistent feature matches and finally, the number of iterations for each filter. Overall, we conclude that HoD-S is the most appealing descriptor for 29 30 the majority of the scenarios, i.e. Real-FB, Sim-Orion, Sim-Helical and Sim-Bennu, with FPFH being the most appealing for the Real-Curved and the Sim-EoI scenarios. These findings confirm 31 that HoD and HoD-S are very robust to low density point clouds (Odysseas Kechagias-Stamatis & 32 33 Aouf, 2016), while in parallel these also afford a low processing time.

34 Interestingly, for each scenario all descriptors attain errors of the same order, with the only major differentiation being the processing burden. This claim should not be confused with the individual 35 findings for each scenario, as in Section 3 we presented the performance of each feature descriptor 36 and filtering method per scenario, while here we evaluate the average performance of each 37 descriptor aver all filtering methods. From Figure 21 it is evident that scenarios exploiting real 38 LIDAR data pose larger errors compared to the synthetic ones. This is important as it highlights 39 that despite creating realistic synthetic scenarios as done in this work, simulating various noise 40 sources, range dependent  $P_k$  resolution variation and viewing dependent  $P_k$  creation from a 41 complete 3D Target model, cannot be as realistic as real data acquisition. However, the feature 42 43 description hierarchy for the top performing descriptors is relatively stable confirming that validity 1 of the results and that despite the disadvantages of synthetic vs. real data, exploiting synthetic data

2 is still valuable.

Regarding computational efficiency, in most cases HoD-S is at least one order of magnitude faster 3 to compute than the rest of the descriptors. On the contrary, RoPS imposes the highest processing 4 burden. This is because the former descriptor neglects estimating a LRF/A, while the latter 5 involves a computationally expensive LRF. This is also evident from the TriSI descriptor that 6 exploits the same LRF estimation method as RoPS, and thus is also processing inefficient. 7 Interestingly, despite FPFH and SHOT being implemented in C++/PCL and executed via a MEX 8 9 wrapper, in most of the scenarios these are less processing efficient than HoD-S and HoD that are entirely implemented in MATLAB. It is worth noting that the Sim-EoI scenario imposes the 10 highest processing burden among all scenarios. This is due to the large  $P_k$  cardinality, 11 12 demonstrating that in such cases, down sampling  $P_k$  or exploiting a keypoint detection strategy 13 rather encoding all  $P_k$  should be considered.

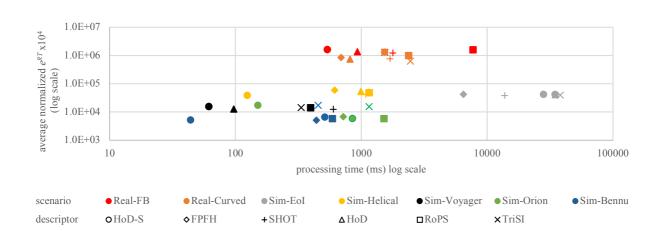
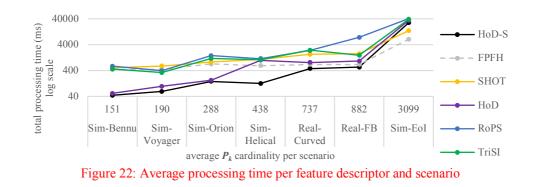


Figure 21: Normalized  $e^{RT}$  vs. processing time per feature descriptor and scenario. Marker shape indicates the descriptor type, while color the scenario. Descriptors attain similar average performance, over all filtering methods, with HoD-S in the majority of cases being the fastest descriptor.

19

14

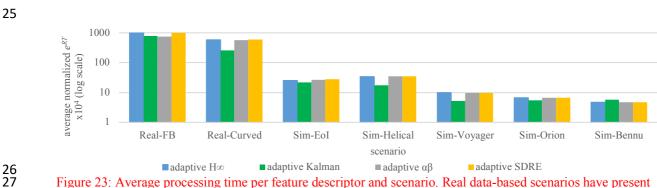
Figure 22 presents the interplay between the  $P_k$  cardinality and the processing burden per 20 descriptor. This figure highlights that FPFH is the least affected by the  $P_k$  cardinality, while HoD 21 and HoD-S are the most affected ones. This is because the processing efficiency of HoD and HoD-22 S, due to neglecting an LRF/A estimation, is not balanced in high cardinality point cloud scenarios, 23 24 i.e. Sim-EoI scenario, due to their large description radius. Our findings in Figure 22, confirm (Guo et al., 2016) in respect to the relative processing efficiency between SHOT, RoPS, TriSI and FPFH. 25 The minor processing time fluctuations between various  $P_k$  cardinality values are because the total 26 processing time considered in this plot is not only affected by the cardinality of  $P_k$  but also by the 27 number of correspondences between  $P_k$  and  $P_{k+1}$ . 28

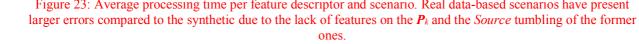




#### 4 4.2 Recursive filtering performance analysis

Next, we evaluate the performance of each filter per scenario, as an average over all feature 5 descriptors evaluated. From Tables 3-9 we observe that the average processing time of each filter 6 per scenario is almost independent from the recursive filtering method used, i.e. the fastest filter 7 has only a 2% speed-up against the slowest one. Therefore, in Figure 23 we decouple the average 8 normalized  $e^{RT}$  error from the total processing time per scenario and presents only the error. The 9 results clearly demonstrate the superiority of the adaptive Kalman filtering as in five out of seven 10 trials it affords a greater odometry accuracy over its competitor filters. Even for the Real-FB and 11 Sim-Bennu scenarios where the adaptive Kalman filter is not the top performing one, it's  $e^{RT}$  error 12 is only 2.5% and 8.3% greater compared to the top performing filter respectively. This is because 13 14 opposing to the  $\alpha\beta$  filter that is restricted by two states and uses static manually defined filter gains, the Kalman filter is not restricted and relies on a time-dependent automatically updated estimate 15 of the state covariance, which is based on user defined covariance noise models. SDRE is a non-16 17 linear filter and since the Target point cloud between  $P_k$  and  $P_{k+1}$  is small, it can be better approximated with linear models. However, as already mentioned, these observations consider the 18 average performance per filter and scenario, and do not prohibit the case where a filter attains a 19 low average performance but a very appealing odometry accuracy if combined with a specific 20 descriptor. Similarly to Figure 21, Figure 23 also highlights the difference between using real and 21 synthetic data. In fact, scenarios involving real data impose errors that are at least one order of 22 magnitude greater compared to synthetic data. This is mainly due to the poor structure of the  $P_k$ 23 acquired by the LIDAR sensor and due to the minor Source platform tumbling. 24

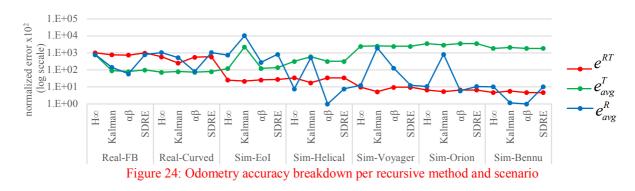




29 30

In Figure 24 we further analyze the performance of each filter by presenting the  $e^{RT}$ ,  $e^{T}_{avg}$  and  $e^{R}_{avg}$ errors per filter and scenario. From this figure it is also obvious that the data modality, i.e. real vs. synthetic, has a great impact on the odometry accuracy. As already presented in Figure 23, the  $e^{RT}$ error in the real scenarios is higher compared to the error in the simulated ones. Interestingly, in the real LIDAR data and in the Sim-EoI scenario, which has a high  $P_k$  cardinality, the  $e_{avg}^T$  is smaller than the  $e_{avg}^{R}$ , while in the remaining synthetic scenarios with a low  $P_{k}$  cardinality this is reversed. This effect is because of the frame-to-frame motion of the real-data scenarios that is less smooth compared to the synthetic ones and also due to the high  $P_k$  cardinality of the Sim-EoI scenario. Furthermore, given that the Sim-EoI and the Sim-Voyager, Sim-Orion and Sim-Bennu scenarios adopt the same trajectory, the difference between the  $e_{avg}^{R}$  and  $e_{avg}^{T}$  errors can be related to the  $P_k$  sparsity in combination to the amount of details/ distinctive features in each  $P_k$ . It should be noted that the calculation of the error metrics presented in Figure 24 is based on eq. (27), (29) and (31) respectively, with the former two equations being conceptually different compared to the third one. Therefore, the  $e_{avg}^{R}$  and  $e_{avg}^{T}$  errors can significantly differ from the  $e^{RT}$  error, e.g. the errors of the Kalman filter for the Sim-EoI scenario presented in Figure 24. 





For completeness, we also investigate the importance of the recursive filtering module by substituting it in our odometry pipeline with the ICP point-to-point registration process, which is a commonly used registration method in the space navigation literature. Hence, in this trial we apply the ICP point-to-point on the correspondences produced by the GCC process, rather than on the entire  $P_k$  as done in the trials of Section 3. The performance attained with and without the recursive filtering module per scenario is presented in Table 10, where it is clear that the recursive filtering process has a great impact on the odometry accuracy. However, exploiting a recursive filtering scheme increases the total computational time. 

| Scenario    |                 | $e_{avg}^{T}$  |                      | $e_a^{l}$      | R<br>Ivg          | e              | RT                   | t (ms)         |                   |
|-------------|-----------------|----------------|----------------------|----------------|-------------------|----------------|----------------------|----------------|-------------------|
|             | top combination | with filtering | without<br>filtering | with filtering | without filtering | with filtering | without<br>filtering | with filtering | without filtering |
|             |                 |                | 0                    | 0              |                   | 0              | 0                    | 0              | 0                 |
| Real-FB     | HOD-S/ αβ       | 0.10           | 11.58                | 0.99           | -77.59            | 1.79           | 298.93               | 1753           | 1481              |
| Real-Curved | HOD-S/ αβ       | 0.16           | 2.05                 | 1.44           | 137.10            | 2.75           | 140.36               | 816            | 801               |
| Sim-EoI     | HOD-S/ αβ       | 0.70           | 37.88                | 2.91           | -163.74           | 9.23           | 246.67               | 27954          | 26362             |
| Sim-Helical | HOD-S/ αβ       | 1.61           | 10.36                | 0.01           | 18.56             | 12.53          | 45.06                | 112            | 66                |
| Sim-Voyager | HoD-S/ SDRE     | 14.20          | 28.52                | 0.14           | 119.44            | 40.78          | 177.50               | 57             | 27                |
| Sim-Orion   | SHOT/ Kalman    | 5.32           | 49.83                | 0.01           | 91.69             | 24.25          | 176.40               | 858            | 714               |
| Sim-Bennu   | HOD-S/ αβ       | 1.16           | 147.22               | 0.01           | 164.89            | 10.65          | 365.75               | 41             | 27                |

#### Table 10: Odometry performance with and without the recursive filtering module

3

#### 4 4.3 Performance analysis of the top performing description – filtering combination

In Table 11 we summarize the most appealing module per scenario, i.e. descriptor, filtering method 5 and the combination of the former two modules, along with the special features per scenario. From 6 7 the results presented in Figure 21 and summarized in Table 11, it can be concluded that overall in terms of odometry accuracy and computational burden, HoD-S is the most appealing feature 8 descriptor, with FPFH to follow. Considering the best performing filtering scheme, from Figure 9 23 we observe that the adaptive Kalman is the optimum choice, with the adaptive  $\alpha\beta$  filter to 10 follow. A summary of the top performing filtering method per scenario is presented in Table 11. 11 Interestingly, the most appealing descriptors and recursive filtering methods per scenario, as 12 concluded from the scenarios in Section 3, do not necessarily coincide with the most appealing 13 combination of these two modules individually. This is because in the former analysis on the 14 optimum descriptor per scenario, we considered the overall performance of all recursive filtering 15 methods evaluated in this work. 16

17

#### Table 11: Top performing module per scenario

| Scenario    | Top<br>descriptor | Top recursive<br>filtering | Top combination       | Scenario features   |
|-------------|-------------------|----------------------------|-----------------------|---|
| Real-FB     | HoD-S             | αβ                         | HoD-S / $\alpha\beta$ | Low density – poor structure                                |
| Real-Curved | FPFH              | Kalman                     | HoD-S / αβ            | Low density – high curvature – poor<br>structure            |
| Sim-EoI     | FPFH              | Kalman                     | HoD-S / $\alpha\beta$ | High density – high curvature                               |
| Sim-Helical | HoD-S             | Kalman                     | HoD-S / αβ            | Very low density – high curvature –<br>large 3D translation |
| Sim-Voyager | HoD-S             | Kalman                     | HoD-S / SDRE          | Very low density – high curvature                           |
| Sim-Orion   | HoD-S             | Kalman                     | SHOT / Kalman         | Very low density – High curvature –<br>poor structure       |
| Sim-Bennu   | HoD-S             | αβ                         | HoD-S / $\alpha\beta$ | Very low density – High curvature                           |

18 19

their processing efficiency confirming the findings of (Odysseas Kechagias-Stamatis & Aouf,
 2016). Despite that, in the *Sim-Orion* scenario SHOT combined with the adaptive *Kalman* filter

present the most appealing combination. This is because the *Target* involved in this scenario has

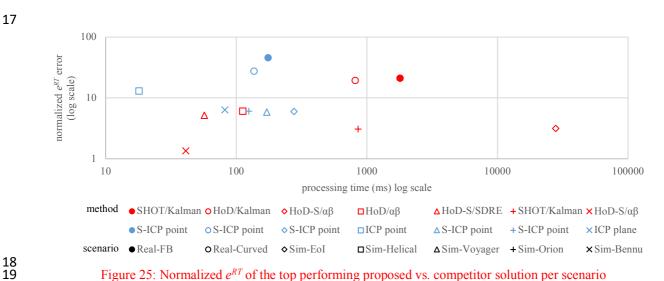
present the most appearing combination. This is because the *rarget* involved in this set

<sup>20</sup> HoD-S is appealing because of its robustness to low and very low density point clouds along with

a poor structure comprising mostly of flat surfaces, indicating that for that type of scenarios 1 involving a LRF in the description process is crucial. 2

We further analyze the performance of the top performing combinations per scenario, by 3 comparing them against the corresponding top performing competitor solutions. Evaluation 4 considers the odometry accuracy expressed via the normalized  $e^{RT}$  error metric and the 5 computational burden imposed by each solution. From Figure 25 it is obvious that the proposed 6 method is more accurate, while ICP based methods are generally faster to execute. It should be 7 noted that the results of Figure 25 are normalized but not scaled, i.e. multiplied with a fixed 8 9 constant. By combining the information presented in Figure 25 and the average  $P_k$  cardinality per scenario shown in Figure 12, the following conclusions can be made: First, for highly sparse point 10 clouds, e.g. Sim-Voyager and Sim-Bennu scenarios, the proposed method is more accurate than the 11 12 top performing competitor method evaluated in this work and is faster to execute. For sparse  $P_k$ , e.g. Real-FB, Real-Curved, Sim-Helical and Sim-Orion, identifying the most appealing solutions 13 depends on the nature of  $P_k$ , i.e. real vs. simulated data. Specifically, for the real LIDAR data case, 14 the top performing ICP variant is one order of magnitude faster than the proposed method, with 15

the  $e^{RT}$  error being of the same order. 16



# 18 19

20 From the trials presented in this paper, it is clear that the proposed odometry is more accurate 21 compared to current space-oriented navigation techniques. One limitation of our method is that for 22 point clouds exceeding 200 vertices, its computational burden is higher than the burden imposed 23 by the ICP variants. However, in this paper we focus on cases simulating a low-resolution point 24 cloud that is acquired by a space graded LIDAR sensor at greater distances or by a low-cost low-25 resolution space-graded LIDAR device. Thus, this limitation considers a broader usage of our 26 architecture and not for the cases examined here. Regarding the computational burden, partially 27 this is because our architecture is a blend of MATLAB and C++ and thus it is not optimized in 28 terms processing efficiency. However, given that our odometry architecture comprises of several 29 processes, i.e. feature description, matching, geometric consistency checks and recursive filtering, 30 31 implementing it in C++ shall still be more processing costly compared to ICP, but with a smaller time difference. However, as already stated, this paper is focusing on the conceptual validity of 32 the proposed method rather than to a readily available solution. An additional limitation of our 33

1 method is its sensitivity to *Targets* with smooth surfaces because 3D local feature descriptors are

2 prone to mismatches affecting the odometry accuracy. Despite that, in scenarios that involve

3 *Targets* with flat surfaces, the proposed odometry solution still manages to attain lower odometry

4 errors compared to typical ICP techniques.

# 5 4.4 GCC module performance analysis

We also investigate the influence of the GCC module by substituting it in our odometry pipeline 6 with RANSAC, which is a commonly used in computer vision applications to define the inliers of 7 two data sets. Table 12 compares the odometry performance of our original architecture against 8 the one using RANSAC. We implement the latter with a false alarm rate of 0.1, an inlier ratio of 9 10 99% and performing at least 50,000 iterations. From Table 12, it is evident that GCC is up to one order of magnitude more accurate than RANSAC, while the normalized rotational accuracy is up 11 to two orders of magnitude more accurate. This performance difference is more evident in the real 12 scenarios highlighting that RANSAC is more prone to real LIDAR point clouds that suffer from 13 minor noise and sensor tumbling during acquisition. 14

In terms of processing burden, we partially confirm (Yang et al., 2018), which states that RANSAC 15 imposes up to two orders of magnitude additional computational time. In fact, our trials confirm 16 17 the former statement but only for Target point clouds with a cardinality that is less than approximately 700 vertices. In fact, for larger point clouds we observe that GCC and RANSAC 18 require the same order of execution time, with RANSAC though being faster to execute. This is 19 20 because for each iteration RANSAC exploits only a random sample out of the corresponding vertices and then applies the estimated model on the entire input data, while GCC involves in each 21 iteration all the corresponding vertices as produced by the coarse matching process of eq. (5). 22 Therefore, given that the inter-motion between  $P_k$  and  $P_{k+l}$  is small, the number of corresponding 23 vertices produced by eq. (5) is directly related to the point cloud cardinality. In simple words, GCC 24 is faster to execute because if  $P_k$  and  $P_{k+1}$  have a small cardinality, then eq. (5) produces less 25 correspondences that need to be evaluated by the GCC module. 26

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- 28 29

Table 12: Odometry performance with and without the GCC module

| Scenario    | top combination       | normalized $e_{avg}^T$ |        | normali | zed $e_{avg}^R$ | normali | $zed e^{RT}$ | t (ms) |        |
|-------------|-----------------------|------------------------|--------|---------|-----------------|---------|--------------|--------|--------|
|             | 1                     | GCC                    | RANSAC | GCC     | RANSAC          | GCC     | RANSAC       | GCC    | RANSAC |
| Real-FB     | HoD-S / $\alpha\beta$ | 0.013                  | 0.543  | 0.133   | 11.690          | 0.241   | 12.421       | 1753   | 1442   |
| Real-Curved | HoD-S / $\alpha\beta$ | 0.013                  | 0.351  | 0.116   | 11.215          | 0.222   | 11.800       | 816    | 677    |
| Sim-EoI     | HoD-S / $\alpha\beta$ | 0.002                  | 0.190  | 0.010   | 0.550           | 0.032   | 0.761        | 27954  | 9896   |
| Sim-Helical | HoD-S / $\alpha\beta$ | 0.008                  | 0.518  | 0.001   | -0.553          | 0.061   | 1.776        | 112    | 3102   |
| Sim-Voyager | HoD-S/ SDRE           | 0.018                  | 0.067  | 0.001   | 0.226           | 0.052   | 0.300        | 57     | 3128   |
| Sim-Orion   | SHOT/ Kalman          | 0.007                  | 0.058  | 0.001   | -0.175          | 0.031   | 0.347        | 858    | 3857   |
| Sim-Bennu   | HOD-S/ αβ             | 0.001                  | 0.071  | 0.001   | -0.190          | 0.014   | 0.348        | 41     | 3409   |

30

## 31 4.5 Comparison against the Correspondence by Local and Global Voting method

32 We further challenge the performance of the proposed pipeline against the Correspondence by

33 Local and Global Voting (CLGV) (Buch et al., 2014). This technique involves four steps, namely

34 feature description, correspondence refinement via GCC and RANSAC, and finally Singular Value

Decomposition (SVD) to estimate the rigid transformation between  $P_k$  and  $P_{k+l}$ . Table 13 1 highlights that the proposed solution is more appealing compared to CLGV, attaining odometry 2

accuracy that is one order of magnitude more accurate and more processing efficient. This is 3

because the SVD suffers from ambiguity in the orientation of the singular vectors (Tomasi, 2016) 4

affecting the estimation of  $R^*$  (eq. (1)). Regarding computational effort, CLGV imposes a large 5

processing burden mainly due to the two iterative processes involved, i.e. GCC and RANSAC. 6

7

8

| Scenario    | top combination       | normalized $e_{avg}^T$ |       | normaliz | ed $e^{R}_{avg}$ | normaliz | $ed e^{RT}$ | t (ms)   |       |
|-------------|-----------------------|------------------------|-------|----------|------------------|----------|-------------|----------|-------|
|             | •                     | proposed               | CLGV  | proposed | CLGV             | proposed | CLGV        | proposed | CLGV  |
| Real-FB     | HoD-S / $\alpha\beta$ | 0.013                  | 0.554 | 0.133    | 14.447           | 0.241    | 15.260      | 1753     | 1382  |
| Real-Curved | HoD-S / $\alpha\beta$ | 0.013                  | 0.328 | 0.116    | 7.183            | 0.222    | 7.653       | 816      | 645   |
| Sim-EoI     | HoD-S / $\alpha\beta$ | 0.002                  | 0.185 | 0.010    | 0.510            | 0.032    | 0.705       | 27954    | 39249 |
| Sim-Helical | HoD-S / $\alpha\beta$ | 0.008                  | 0.319 | 0.001    | 0.613            | 0.061    | 0.958       | 112      | 3016  |
| Sim-Voyager | HoD-S/ SDRE           | 0.018                  | 0.061 | 0.001    | -0.140           | 0.052    | 0.378       | 57       | 3245  |
| Sim-Orion   | SHOT/ Kalman          | 0.007                  | 0.103 | 0.001    | -0.204           | 0.031    | 0.379       | 858      | 4221  |
| Sim-Bennu   | HOD-S/ αβ             | 0.001                  | 0.087 | 0.001    | -0.213           | 0.014    | 0.345       | 41       | 3482  |

Table 13: Proposed vs. Global / Local voting odometry

9

#### Interplay between performance and number of iterations for the ICP variants 4.6 10

In Section 3, we set the number of maximum iterations per ICP method, i.e. ICP point 20, ICP 11 plane 1000, ICP x84 20, while the iterations for both S-ICP variants are set to 20. To support this 12 choice per ICP method, we evaluate each ICP variant by setting the maximum number of iterations 13 14 to 20 and 1000. Evaluation considers the scenarios presented in Section 3 and the corresponding 15 results are presented in Table 14. For better readability, the best performance per normalized error is highlighted in red, if it is attained by setting to 20 iterations, and in blue if setting to 1000 16

iterations. 17

18 From the results obtained it is clear that the chosen number of iterations used in Section 3 is the optimum one for each ICP variant. However, from further analyzing the results of Table 14, we 19 observe that the ICP plane variant settles in up to 20 iterations, for both the real and the simulated 20 data scenarios. Accordingly, the ICP plane variant requires more iterations to settle and thus setting 21 to the threshold up to 1000 is mandatory. It is worth noting that for both variants, the normalized 22 translational, rotational and  $e^{RT}$  errors equally benefit from the number of iterations set. However, 23 interestingly this is not the case for the ICP x84 variant, as the translational and  $e^{RT}$  errors benefit 24 from a low number of iterations, while the rotational error from a large number. This behavior is 25 present in both the real and the synthetic data scenarios. The S-ICP point variant, presents overall 26 a higher odometry accuracy when the iterations are up to 20. However, this is only valid for the 27 synthetic data scenarios, as real data scenarios require more iterations. Given that during the 28 parameter setup we set the parameters of each method to be universal, i.e. selected for an overall 29 30 optimum odometry accuracy on both real and synthetic data scenarios, we set iterations to 20. Finally, the S-ICP plane variant is quite stable requiring up to 20 iterations. The results obtained 31 confirm our previous findings that real and simulated data require a different parameter setup. 32 33

Table 14: ICP performance vs. number of iterations

| C           | LOD         | normaliz           | $e^{T}_{avg}$ | normaliz      | $e^{R}_{avg}$  | normaliz           | $e^{RT}$     | t (n       | ns)        |
|-------------|-------------|--------------------|---------------|---------------|----------------|--------------------|--------------|------------|------------|
| Scenario    | ICP variant | 20                 | 1000          | 20            | 1000           | 20                 | 1000         | 20         | 1000       |
|             |             | iterations         | iterations    | iterations    | iterations     | iterations         | iterations   | iterations | iterations |
|             | ICP point   | 0.086              | 0.086         | 11.402        | 11.402         | 11.649             | 11.649       | 5          | 6          |
|             | ICP plane   | 0.131              | 0.131         | -23.090       | -23.090        | 25.872             | 25.872       | 9          | 9          |
| Real-FB     | ICP x84     | 1.291              | 6.126         | -22.321       | -16.821        | 27.893             | 38.699       | 41         | 983        |
|             | S-ICP point | 0.266              | 0.131         | 0.001         | -23.090        | 0.462              | 25.872       | 145        | 191        |
|             | S-ICP plane | 0.266              | 0.105         | 0.001         | 0.313          | 0.462              | 0.602        | 150        | 305        |
|             | ICP point   | 0.136              | 0.227         | <b>8.44</b> 7 | 12.427         | <b>8.</b> 723      | 12.745       | 6          | 6          |
|             | ICP plane   | 0.146              | 0.177         | -13.567       | 12.922         | 15.792             | 13.225       | 10         | 28         |
| Real-Curved | ICP x84     | 0.343              | 11.547        | 10.971        | -9.621         | 11.341             | 31.967       | 53         | 1058       |
|             | S-ICP point | 0.159              | 0.176         | 0.001         | 12.933         | 0.276              | 13.234       | 137        | 28         |
|             | S-ICP plane | 0.159              | 0.025         | 0.001         | 1.196          | 0.276              | 1.343        | 145        | 250        |
|             | ICP point   | 0.134              | 0.135         | -0.565        | -0.565         | 0.858              | 0.859        | 30         | 30         |
|             | ICP plane   | 0.126              | 0.126         | -0.576        | -0.576         | 0.811              | 0.811        | 31         | 51         |
| Sim-EoI     | ICP x84     | 0.158              | 1.004         | -0.570        | -0.445         | 0.887              | 2.223        | <b>49</b>  | 1059       |
|             | S-ICP point | 0.039              | 0.126         | 0.001         | -0.576         | 0.060              | 0.811        | 276        | 51         |
|             | S-ICP plane | 0.039              | 0.088         | 0.001         | 0.434          | 0.060              | 0.610        | 327        | 14702      |
|             | ICP point   | 0.041              | 0.019         | 0.057         | 0.339          | 0.192              | 0.422        | 8          | 10         |
|             | ICP plane   | 1012               | 0.048         | 0.578         | 0.297          | 3x10 <sup>11</sup> | <i>0.461</i> | 17         | 127        |
| Sim-Helical | ICP x84     | 11.933             | 3.500         | -0.788        | <b>-0.65</b> 7 | 18.400             | 5.940        | 36         | 417        |
|             | S-ICP point | 0.190              | 0.055         | 0.001         | 0.285          | 0.243              | 0.411        | 107        | <u>84</u>  |
|             | S-ICP plane | 0.196              | 0.008         | 0.001         | 0.001          | 0.248              | 0.064        | 105        | 123        |
|             | ICP point   | 0.038              | 0.083         | 0.209         | 0.220          | 0.296              | 0.344        | 7          | 10         |
|             | ICP plane   | 7x10 <sup>5</sup>  | 0.025         | 0.174         | 0.126          | 6x10 <sup>5</sup>  | 0.189        | 8          | 19         |
| Sim-Voyager | ICP x84     | 0.358              | 0.362         | 0.215         | -0.164         | 0.710              | 0.749        | 16         | 284        |
|             | S-ICP point | 0.037              | 0.017         | 0.001         | 0.053          | 0.059              | 0.102        | 171        | 14         |
|             | S-ICP plane | 0.037              | 0.028         | 0.001         | 0.120          | 0.059              | 0.176        | 177        | 307        |
|             | ICP point   | 0.012              | 0.065         | -0.165        | 0.064          | 0.333              | 0.185        | 13         | 14         |
|             | ICP plane   | 761.035            | 0.045         | 0.192         | 0.062          | 1014.713           | 0.158        | 12         | 14         |
| Sim-Orion   | ICP x84     | 0.084              | 0.963         | -0.207        | -0.176         | 0.352              | 1.701        | 24         | 407        |
|             | S-ICP point | 0.042              | 0.069         | 0.001         | -0.223         | 0.061              | 0.354        | 125        | 15         |
|             | S-ICP plane | 0.042              | 0.069         | 0.001         | 0.004          | 0.061              | 0.122        | 133        | 52         |
|             | ICP point   | 0.371              | 0.055         | -0.199        | 0.212          | 0.731              | 0.300        | 11         | 16         |
|             | ICP plane   | 3x10 <sup>14</sup> | 0.143         | -0.189        | 0.184          | 5x10 <sup>14</sup> | 0.373        | 36         | 84         |
| Sim-Bennu   | ICP x84     | 0.265              | 0.652         | -0.014        | -0.223         | 0.604              | 1.127        | 35         | 419        |
|             | S-ICP point | 0.049              | 0.011         | 0.001         | -0.157         | 0.064              | 0.339        | 99         | 55         |
|             | S-ICP plane | 0.049              | 0.034         | 0.001         | 0.107          | 0.064              | 0.172        | 112        | 300        |

# 4 **5.** Conclusion

5 LIDAR based odometry for space relative navigation is challenging due to the absence of 6 background, the limited structure and the sparsity of the *Target* point cloud. As demonstrated, 7 several ICP variants, the S4PCS, and the Correspondence Local/ Global voting method, which are 8 currently widely used for point cloud registration and odometry applications, do not guarantee an 9 accurate space odometry trajectory. Spurred by this, we suggest a robust architecture appropriate 10 for space odometry that combines the concepts of 3D local feature description, geometric 11 correspondence grouping for feature matching refinement and adaptive recursive filtering.

The accuracy of the proposed pipeline is tested on seven scenarios that include both real and 1 synthetic point cloud data, on four space objects comprising of quite a few different satellites, a 2 space capsule and an asteroid. In our trials we evaluate several current 3D local descriptor and 3 recursive filtering combinations and demonstrate that the proposed architecture is 50% more 4 accurate compared to current solutions. Our trials highlighted that HoD-S combined with the 5 adaptive  $\alpha\beta$  filtering poses the most appealing combination for the majority of the scenarios 6 evaluated, affording a high quality odometry performance with a low processing burden. 7 Additional advantages of the proposed architecture over current LIDAR space odometry 8 architectures are; being independent of an off-line training process and not requiring a priori 9 knowledge of the *Target* platform. 10

#### 11 Acknowledgements

- 12 This research was supported by the European Union as part of the H2020 project "Integrated 3D
- 13 Sensors (I3DS)" under grant Nº 730118. Authors would like to thank Thales Alenia Space for
- 14 providing the simulated data for the *Sim-EoI* scenario 3. The authors would also like to thank
- 15 the anonymous reviewers for their constructive comments.

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