

Adaptive Iterative Learning Control of Non-uniform Trajectory Tracking for Strict Feedback Nonlinear Time-varying Systems

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Abstract: In this paper, an iterative learning control strategy is presented for a class of nonlinear time-varying systems, the time-varying parameters are expanded into Fourier series with bounded remainder term. The backstepping design technique is used to deal with system dynamics with non-global Lipschitz nonlinearities and the approach proposed in this paper solves the non-uniform trajectory tracking problem. Based on the Lyapunov-like synthesis, the proposed method shows that all signals in the closed-loop system remain bounded over a pre-specified time interval $[0, T]$. And perfect non-uniform trajectory tracking of the system output is completed. A typical series is introduced in order to deal with the unknown bound of remainder term. Finally, a simulation example shows the feasibility and effectiveness of the approach.

Keywords: Iterative learning control, time-varying systems, Lyapunov-like, non-uniform trajectory tracking, Fourier series expansion, backstepping.

1 Introduction

Iterative learning control (ILC) or adaptive iterative learning control (AILC) has become one of the most effective control strategies in dealing with repeated tracking control of nonlinear systems. And the additional requirement of the repetitive mode is that a specified output trajectory on a finite interval is followed with a high precision (or so called exactly tracking). Examples of such systems include robotic manipulators required to repeat a given task with high precision, chemical batch processes, vehicles and man-machine systems. The ILC system improves the control performances by self-tuning the leaning gains in the traditional D-type, P-type, PD-type or PID-type ILC for linear or affine nonlinear dynamic systems with nonlinearities satisfying the global Lipschitz continuous condition^[1,2].

In the existing literature, the tracking trajectory must be uniform, for a complex tracking trajectory problem (such as varying trajectory along iterative direction), there is no well-posed method to consider it. Actually, the non-uniform trajectory can be considered as an uncertain time-varying parameter along both iterative direction and time domain, therefore, it becomes a challenging problem to study an ILC strategy for uncertain time-varying parametric systems. In [3], D-type, PD-type and PID-type learning algorithms were presented to solve the problem of slow varying trajectory along iterative direction. In [4], an adaptive iterative learning control method via Lyapunov technique was proposed for the system with unknown constant parameter uncertainty, which can be used to track the similar variant trajectory or unseen trajectories. In [5], a new adaptive iterative learning control strategy was presented on the basis

of neural networks, which has the capability of generalization both for tracking trajectory and for system structure. However, there still have some restricts on the trajectory. In [6], for the first-order hybrid parametric system, a new iterative learning control law consisting of a feedback term and a learning term was proposed, which can perform different tracking control tasks. Recently, a novel adaptive iterative learning control approach was proposed for a class of hybrid parametric nonlinear systems by means of backstepping method in [7]. Similarly, a novel adaptive iterative learning control approach was proposed for a class of hybrid parametric nonlinear time-delay systems^[8]. The approach consists of a differential-deference type updating law and a learning control law for handling the non-uniform trajectory tracking problem. It avoids the restrictions on the tracking trajectory in the traditional ILC.

In many industrial applications, the system parameters are completely unknown or partially unknown. When these parameters are unknown time-varying ones, the controller design problem of the uncertain nonlinear system becomes a challenging topic^[9-11]. When the period of uncertain parameters of the system is known in advance, by the pointwise integral mechanism, a new adaptive control approach characterized by periodic parameter adaptation was proposed, which complements periodic parameter adaptation control of the first-order uncertain system with mixed linear parameters, such that the tracking error converges to zero asymptotically in the L_T^2 -norm sense^[12]. In [13], a new approach of designing a repetitive learning controller for a class of unmatched nonlinear systems with both completely unknown virtual control coefficients and unknown time-varying parameters was proposed, which by incorporating a Nussbaum-type function and backstepping technique, can guarantee uniform ultimate boundedness of the states. In [14], combining the backstepping approach with the pointwise integral mechanism, a novel adaptive repeti-

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tive learning control for high-order nonlinear systems with time-varying and time-invariant parameters was proposed. An iterative learning controller was presented for a class of strict-feedback nonlinear systems with time-varying uncertainties in [15]. The learning controller is designed based on the Lyapunov-like synthesis, which can handle system dynamics with non-global Lipschitz nonlinearities. The theoretical analysis shows that all signals in the closed-loop system remain bounded over a pre-specified time interval $[0, T]$. And complete tracking of the system output is achieved. But the control objective of the article was uniform and the bound of remain term was known.

Motivated by the above discussion, we propose an iterative learning controller for a class of nonlinear time-varying systems to solve the non-uniform trajectory tracking problem. The learning controller is designed based on the Lyapunov-like synthesis, which can handle system dynamics with non-global Lipschitz nonlinearities. For the controller design, the time-varying parameters are expanded into Fourier series with bounded remainder term, whose bound is unknown. The theoretical analysis shows that all signals in the closed-loop system remain bounded, and perfect non-uniform trajectory tracking of the system output is completed. Finally, we give a simulation example to show the feasibility and effectiveness of the approach.

2 System description

Consider a class of high-order nonlinear time-varying systems

$$\begin{aligned} \dot{x}_i &= x_{i+1} + \theta^T(t)\varphi_i(\bar{x}_i) \\ \dot{x}_n &= u(t) + \theta^T(t)\varphi_n(\bar{x}_n) \\ y &= x_1 \end{aligned} \quad (1)$$

where $\bar{x}_n = [x_1, \dots, x_n]^T \in \mathbf{R}^n$ is the state vectors of the system, which is assumed to be available for measurement, $\bar{x}_i = [x_1, \dots, x_i]^T$, $u \in \mathbf{R}$ and $y \in \mathbf{R}$ correspond to system input and output, respectively. Denote $x = \bar{x}_n$. $x(t_0) = x_0$ represents initial conditions of the system, $\theta(t) \in \mathbf{R}^p$ is an unknown continuous time varying function vector, $\varphi_i(\bar{x}_i)$, $i = 1, \dots, n$ are all known smooth function, and $\varphi_i(0) = 0$, $i = 1, \dots, n$.

Now, we suppose that the system time-varying parameter vector $\theta(t)$ is a fully unknown continuous periodic function vector with a known period T . Each component $\theta_i(t)$, $i = 1, \dots, p$ of the continuous and periodic function vector $\theta(t)$ can be expressed by a linearly parameterized Fourier series expansion as

$$\theta_i(t) = \phi_i^T(t)\eta_i + \delta_i(t), |\delta_i(t)| \leq \bar{\delta}_i \quad (2)$$

where $\eta_i = [\eta_{i1}, \eta_{i2}, \dots, \eta_{iq}]^T \in \mathbf{R}^q$ is a constant vector consisting of the first q coefficients of the Fourier series expansion of $\theta_i(t)$ (q is an odd integer). $\delta_i(t)$ is the truncation error with the minimum upper bound $\bar{\delta}_i > 0$, which can be arbitrarily decreased by increasing q . And $\phi_i(t) = [\phi_{i1}(t), \dots, \phi_{iq}(t)]^T$ with $\phi_{i1}(t) = 1$, $\phi_{i2j}(t) = \sin(\frac{2\pi jt}{T})$ and $\phi_{i2j+1}(t) = \cos(\frac{2\pi jt}{T})$, $j = 1, \dots, \frac{(q-1)}{2}$, whose derivatives up to n -order are smooth and bounded.

Let $\phi(t) = \text{diag}\{\phi_1(t), \phi_2(t), \dots, \phi_n(t)\}$, $\eta = [\eta_1^T, \eta_2^T, \dots, \eta_n^T]^T$, $\delta(t) = [\delta_1(t), \delta_2(t), \dots, \delta_n(t)]^T$. Then the parameter

vector $\theta(t)$ can be rewritten as

$$\theta(t) = \phi^T(t)\eta + \delta(t). \quad (3)$$

From (2), we have $\|\delta(t)\| \leq s$. We assume that the upper bound s is an unknown parameter. Then after substituting (3) into system (1), system (1) becomes

$$\begin{aligned} \dot{x}_i &= x_{i+1} + \eta^T \phi(t)\varphi_i(\bar{x}_i) + \delta^T(t)\varphi_i(\bar{x}_i) \\ \dot{x}_n &= u(t) + \eta^T \phi(t)\varphi_n(\bar{x}_n) + \delta^T(t)\varphi_n(\bar{x}_n) \\ y &= x_1. \end{aligned} \quad (4)$$

Our objective is to design an adaptive iterative learning control law $u_k(t)$ on $[0, T]$, such that the tracking error $e_k(t) = y_k(t) - y_{r,k}(t)$ converges to zero completely when $k \rightarrow \infty$, and all signals of the closed-loop system are kept bounded, where k denotes the iteration index, $y_{r,k}(t)$ represents the k -th sufficiently smooth iterative target trajectory.

In order to design the controller, a definition of convergent series sequence and its lemma are given as follows.

Definition 1^[15]. A convergent series sequence $\{\Delta_k\}$ is defined as

$$\Delta_k = \frac{a}{k^l} \quad (5)$$

where $k = 1, 2, \dots$; a and l are designed constant parameters, and $a > 0 \in \mathbf{R}$, $l \geq 2 \in \mathbf{N}$.

Lemma 1^[15]. For given sequence $\{\frac{1}{k^l}\}$, where $k = 1, 2, \dots$, and the positive integer $l \geq 2$, the following inequality holds:

$$\lim_{k \rightarrow \infty} \sum_{i=1}^k \frac{1}{i^l} \leq 2. \quad (6)$$

3 Adaptive iterative learning controller design

In the design process of the controller, we introduce the convergent series sequence of Definition 1 to eliminate the effect on system performance of the redundant item after expanding the time-varying parameter by using Fourier series. We give the design process of the controller for high-order strict feedback nonlinear time-varying systems as follows.

3.1 Design of the controller

Step 1. Let $\omega_{1,k} = \varphi_{1,k}$. There exists a smooth function $\bar{\varphi}_{1,k}(x_{1,k}) > 0$ such that $|\delta^T(t)\varphi_{1,k}(x_{1,k})| \leq \|\delta^T(t)\|\bar{\varphi}_{1,k}(x_{1,k}) \leq s\bar{\varphi}_{1,k}(x_{1,k})$. Denote $S = s^2$, $z_{1,k} = x_{1,k} - y_{r,k}$, $z_{2,k} = x_{2,k} - \alpha_{1,k} - \dot{y}_{r,k}$, where $\alpha_{1,k}$ is the virtual controller. The time derivative of $z_{1,k}$ along systems (4) is given as

$$\dot{z}_{1,k} = z_{2,k} + \alpha_{1,k} + \eta^T \phi(t)\omega_{1,k} + \delta^T(t)\omega_{1,k}. \quad (7)$$

For any real number $a > 0$ and positive integer $l \geq 2$, let $\Delta_k = \frac{a}{k^l}$, and denote $\tau_{1,k} = \Gamma_1 \phi(t)\omega_{1,k} z_{1,k}$, $\nu_{1,k} = \Gamma_2 \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}^2$.

Take virtual control as $\alpha_{1,k} = -c_1 z_{1,k} - \hat{\eta}_k^T \phi(t)\omega_{1,k} - \hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}$, where c_1 is a positive constant. It is substi-

tuted into (7), and we have

$$\begin{aligned} \dot{z}_{1,k} &= z_{2,k} - c_1 z_{1,k} + \tilde{\eta}_k^T \phi(t) \omega_{1,k} - \\ &\hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k} + \delta^T(t) \omega_{1,k} \end{aligned} \quad (8)$$

where $\hat{\eta}_k$ is the estimation of parameter η , and $\tilde{\eta}_k = \eta - \hat{\eta}_k$ is parameter estimation error. Take the following nonnegative function:

$$V_{1,k}(z_k, \hat{\eta}_k, \hat{S}_k) = \frac{1}{2} z_{1,k}^2 + \frac{1}{2} \tilde{\eta}_k^T \Gamma_1^{-1} \tilde{\eta}_k + \frac{1}{2} \Gamma_2^{-1} \tilde{S}_k^2 \quad (9)$$

where Γ_1 and Γ_2 are symmetric positive definite matrices. \hat{S}_k is the estimation of parameter S , $\tilde{S}_k = S - \hat{S}_k$ is the parameter estimation error. The time derivative of $V_{1,k}$ along systems (8) is given as

$$\begin{aligned} \dot{V}_{1,k} &= z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) - \\ &\hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}^2 + \delta^T(t) \omega_{1,k} z_{1,k} - \Gamma_2^{-1} \tilde{S}_k \dot{\hat{S}}_k \leq \\ &z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) - \\ &\hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}^2 + s \bar{\varphi}_{1,k} |z_{1,k}| - \Gamma_2^{-1} \tilde{S}_k \dot{\hat{S}}_k \leq \\ &z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) - \\ &\hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}^2 + \frac{1}{\Delta_k} s^2 \bar{\varphi}_{1,k}^2 z_{1,k}^2 + \\ &\frac{1}{4} \Delta_k - \Gamma_2^{-1} \tilde{S}_k \dot{\hat{S}}_k = \\ &z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) - \\ &\hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{1,k}^2 z_{1,k}^2 + \frac{1}{\Delta_k} S \bar{\varphi}_{1,k}^2 z_{1,k}^2 + \\ &\frac{1}{4} \Delta_k - \Gamma_2^{-1} \tilde{S}_k \dot{\hat{S}}_k = \\ &z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) + \\ &\frac{1}{4} \Delta_k + \frac{1}{\Delta_k} \tilde{S}_k \bar{\varphi}_{1,k}^2 z_{1,k}^2 - \Gamma_2^{-1} \tilde{S}_k \dot{\hat{S}}_k = \\ &z_{1,k} z_{2,k} - c_1 z_{1,k}^2 + \tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{1,k} - \dot{\hat{\eta}}_k) + \\ &\tilde{S}_k \Gamma_2^{-1} (\nu_{1,k} - \dot{\hat{S}}_k) + \frac{1}{4} \Delta_k. \end{aligned} \quad (10)$$

The following inequality is used in the previous equation. For any $r > 0$, $mn \leq \frac{1}{r} m^2 + \frac{1}{4} n^2 r$, where $r = \Delta_k$.

Step 1 (2 ≤ i ≤ n-1). Let $\omega_{i,k} = \varphi_{i,k} - \sum_{j=1}^{i-1} \frac{\partial \alpha_{i-1,k}}{\partial x_{j,k}} \varphi_{j,k}$. Because $\varphi_{1,k}, \dots, \varphi_{i,k}$ are known smooth functions, there exist smooth function $\bar{\varphi}_{i,k}(x_{1,k}, \dots, x_{i,k}, \hat{\eta}_k, \hat{S}_k) > 0$ such that $|\delta^T(t)(\varphi_{i,k} - \sum_{j=1}^{i-1} \frac{\partial \alpha_{i-1,k}}{\partial x_{j,k}} \varphi_{j,k})| \leq \|\delta^T(t)\| \bar{\varphi}_{i,k} \leq s \bar{\varphi}_{i,k}$. Denote $z_{i+1,k} = x_{i+1,k} - \alpha_{i,k} - y_{r,k}^{(i)}$, $\tau_{i,k} = \tau_{i-1,k} + \Gamma_1 \phi(t) \omega_{i,k} z_{i,k}$, $\nu_{i,k} = \nu_{i-1,k} + \Gamma_2 \frac{1}{\Delta_k} \bar{\varphi}_{i,k}^2 z_{i,k}^2$. Then the time derivative of $z_{i,k}$ is given as

$$\begin{aligned} \dot{z}_{i,k} &= z_{i+1,k} + \alpha_{i,k} + \eta^T \phi(t) \omega_{i,k} + \delta^T(t) \omega_{i,k} - \\ &\frac{\partial \alpha_{i-1,k}}{\partial t} - \sum_{j=1}^{i-1} \frac{\partial \alpha_{i-1,k}}{\partial x_{j,k}} x_{j+1,k} - \\ &\frac{\partial \alpha_{i-1,k}}{\partial \hat{\eta}_k} \dot{\hat{\eta}}_k - \frac{\partial \alpha_{i-1,k}}{\partial \hat{S}_k} \dot{\hat{S}}_k. \end{aligned} \quad (11)$$

Take virtual controller as

$$\begin{aligned} \alpha_{i,k} &= -z_{i-1,k} - c_i z_{i,k} - \hat{\eta}_k^T \phi(t) \omega_{i,k} + \frac{\partial \alpha_{i-1,k}}{\partial t} + \\ &\sum_{j=1}^{i-1} \frac{\partial \alpha_{i-1,k}}{\partial x_{j,k}} x_{j+1,k} + \frac{\partial \alpha_{i-1,k}}{\partial \hat{\eta}_k} \tau_{i,k} + \vartheta_{i,k} + \\ &\frac{\partial \alpha_{i-1,k}}{\partial \hat{S}_k} \nu_{i,k} + \psi_{i,k} - \hat{S}_k \frac{1}{\Delta_k} \bar{\varphi}_{i,k}^2 z_{i,k} \end{aligned} \quad (12)$$

where $\vartheta_{i,k} = \sum_{j=1}^{i-2} \frac{\partial \alpha_{j,k}}{\partial \hat{\eta}_k} \Gamma_1 \phi(t) \omega_{i,k} z_{j+1,k}$, $\psi_{i,k} = \sum_{j=1}^{i-2} \frac{\partial \alpha_{j,k}}{\partial \hat{S}_k} \Gamma_2 \frac{1}{\Delta_k} \bar{\varphi}_{i,k}^2 z_{i,k} z_{j+1,k}$.

Choose the following nonnegative function:

$$V_{i,k}(z_k, \hat{\eta}_k, \hat{S}_k) = \sum_{j=1}^i \frac{1}{2} z_{j,k}^2 + \frac{1}{2} \tilde{\eta}_k^T \Gamma_1^{-1} \tilde{\eta}_k + \frac{1}{2} \Gamma_2^{-1} \tilde{S}_k^2. \quad (13)$$

The time derivative of $V_{i,k}$ along systems (11) is given, and (12) is substituted into it. We have

$$\begin{aligned} \dot{V}_{i,k} &\leq z_{i,k} z_{i+1,k} - \sum_{j=1}^i c_j z_{j,k}^2 + \\ &\left(\sum_{j=1}^{i-1} \frac{\partial \alpha_{j,k}}{\partial \hat{\eta}_k} \right) z_{i,k} (\tau_{i,k} - \dot{\hat{\eta}}_k) + \\ &\left(\sum_{j=1}^{i-1} \frac{\partial \alpha_{j,k}}{\partial \hat{S}_k} \right) z_{i,k} (\nu_{i,k} - \dot{\hat{S}}_k) + \\ &\tilde{\eta}_k^T \Gamma_1^{-1} (\tau_{i,k} - \dot{\hat{\eta}}_k) + \\ &\tilde{S}_k \Gamma_2^{-1} (\nu_{i,k} - \dot{\hat{S}}_k) + i \frac{1}{4} \Delta_k. \end{aligned} \quad (14)$$

Step n. Let $\omega_{n,k} = \varphi_{n,k} - \sum_{j=1}^{n-1} \frac{\partial \alpha_{n-1,k}}{\partial x_{j,k}} \varphi_{j,k}$. Because $\varphi_{1,k}, \dots, \varphi_{n,k}$ are known smooth functions, there exist smooth function $\bar{\varphi}_{n,k}(x_{1,k}, \dots, x_{n,k}, \hat{\eta}_k, \hat{S}_k) > 0$ such that $|\delta^T(t)(\varphi_{n,k} - \sum_{j=1}^{n-1} \frac{\partial \alpha_{n-1,k}}{\partial x_{j,k}} \varphi_{j,k})| \leq \|\delta^T(t)\| \bar{\varphi}_{n,k} \leq s \bar{\varphi}_{n,k}$. Denote $\tau_{n,k} = \tau_{n-1,k} + \Gamma_1 \phi(t) \omega_{n,k} z_{n,k}$ and $\nu_{n,k} = \nu_{n-1,k} + \Gamma_2 \frac{1}{\Delta_k} \bar{\varphi}_{n,k}^2 z_{n,k}^2$. Then the time derivative of $z_{n,k}$ is given as

$$\begin{aligned} \dot{z}_{n,k} &= u_k - y_{r,k}^{(n)} + \eta^T \phi(t) \omega_{n,k} (\bar{x}_{n,k}) + \delta^T(t) \omega_{n,k} (\bar{x}_{n,k}) - \\ &\frac{\partial \alpha_{n-1,k}}{\partial t} - \sum_{j=1}^{n-1} \frac{\partial \alpha_{n-1,k}}{\partial x_{j,k}} x_{j+1,k} - \\ &\frac{\partial \alpha_{n-1,k}}{\partial \hat{\eta}_k} \dot{\hat{\eta}}_k - \frac{\partial \alpha_{n-1,k}}{\partial \hat{S}_k} \dot{\hat{S}}_k. \end{aligned} \quad (15)$$

Take the following controller and adaptive iterative learning laws:

$$u_k = \alpha_{n,k} + y_{r,k}^{(n)} \quad (16)$$

$$\dot{\hat{\eta}}_k = \tau_{n,k} \quad (17)$$

$$\dot{\hat{S}}_k = \nu_{n,k}. \quad (18)$$

Choose the following nonnegative function:

$$V_{n,k}(z_k, \hat{\eta}_k, \hat{S}_k) = \sum_{j=1}^n \frac{1}{2} z_{j,k}^2 + \frac{1}{2} \tilde{\eta}_k^T \Gamma_1^{-1} \tilde{\eta}_k + \frac{1}{2} \Gamma_2^{-1} \tilde{S}_k^2. \quad (19)$$

The time derivative of $V_{n,k}$ along systems (15) is given, and after (16)–(18) are substituted into it, we have

$$\dot{V}_{n,k} \leq - \sum_{j=1}^n c_j z_{j,k}^2 + n \frac{1}{4} \Delta_k. \quad (20)$$

For the setting of the initial state, we give the following assumptions condition.

Assumption 1. For any k , when $t = 0$, $x_{1,k}(0) = y_{r,k}(0)$; $x_{i+1,k}(0) = \alpha_{i,k}(0) - y_{r,k}^{(i)}(0)$, $i = 1, \dots, n-1$; $\hat{\eta}_k(0) = \hat{\eta}_{k-1}(T)$; $\hat{S}_k(0) = \hat{S}_{k-1}(T)$; $y_{r,k}^{(i)}(0) = y_{r,k-1}^{(i)}(T)$, $i = 1, \dots, n$.

3.2 Stability and convergence analysis

Theorem 1. For nonlinear system (1) with assumption 1, we design controller (16) and parameter adaptive laws (17) and (18). Then all signals of closed loop system are bounded on $[0, T]$, and we have

$$\lim_{k \rightarrow \infty} z_{j,k}(t) = 0, \quad j = 1, 2, \dots, n. \quad (21)$$

Proof. According to Assumption 1, we have $\|z_k(0)\|^2 = 0 \leq \|z_k(T)\|^2$. By (19), we obtain

$$V_{n,k}(z_k(0), \hat{\eta}_k(T), \hat{S}_k(T)) \leq V_{n,k}(z_k(0), \hat{\eta}_k(0), \hat{S}_k(0)) + \int_0^T \dot{V}_{n,k} dt. \quad (22)$$

Substitute (20) into (22), then

$$V_{n,k}(z_k(0), \hat{\eta}_k(T), \hat{S}_k(T)) \leq V_{n,1}(z_1(0), \hat{\eta}_1(0), \hat{S}_1(0)) - \sum_{i=1}^k \sum_{j=1}^n \int_0^T c_j z_{j,i}^2 dt + n \left(\frac{1}{4}\right) T \left(\sum_{i=1}^k \Delta_i\right). \quad (23)$$

Denote $V_0(k) = V_{n,1}(z_1(0), \hat{\eta}_1(0), \hat{S}_1(0)) + n \left(\frac{1}{4}\right) T \left(\sum_{i=1}^k \Delta_i\right)$, then (23) can be rewritten as

$$\sum_{i=1}^k \sum_{j=1}^n \int_0^T c_j z_{j,i}^2 dt \leq V_0(k) - V_{n,k}(z_k(0), \hat{\eta}_k(T), \hat{S}_k(T)). \quad (24)$$

By (6), we have $\lim_{k \rightarrow \infty} V_0(k) \leq V_{n,1} + 2an \left(\frac{1}{4}\right) T$, then $V_0(k)$ is bounded, and $V_{n,k}(z_k(0), \hat{\eta}_k(T), \hat{S}_k(T)) \geq 0$, so

$$\lim_{k \rightarrow \infty} \sum_{j=1}^n \int_0^T c_j z_{j,k}^2 dt = 0. \quad (25)$$

By (19), for any k , $V_{n,k}(t) = V_{n,k}(0) + \int_0^t \dot{V}_{n,k}(\tau) d\tau$. Substitute (20) into the previous equations, then

$$V_{n,k}(t) \leq V_{n,k}(0) - \sum_{j=1}^n \int_0^t c_j z_{j,k}^2(\tau) d\tau + tn \left(\frac{1}{4}\right) \Delta_k. \quad (26)$$

By (25), $\sum_{j=1}^n \int_0^t c_j z_{j,k}^2(\tau) d\tau$ is bounded. According to Definition 1, Δ_k is bounded, and $t \in [0, T]$, so $tn \left(\frac{1}{4}\right) \Delta_k$ is also bounded. And also $\hat{\eta}_k(0) = \hat{\eta}_{k-1}(T)$, $\hat{S}_k(0) = \hat{S}_{k-1}(T)$.

By (23), for any k , $V_{n,k}(0, \hat{\eta}_k(T), \hat{S}_k(T))$ is bounded, so $V_{n,k}(0, \hat{\eta}_k(0), \hat{S}_k(0)) = V_{n,k-1}(0, \hat{\eta}_{k-1}(T), \hat{S}_{k-1}(T))$ is also bounded. From all above, for any k , $V_{n,k}(t)$ is bounded, then we have $x_{i,k}$, $\hat{\eta}_k(t)$ and $\hat{S}_k(t)$ are bounded. By (16), u_k is bounded. By (11), $\dot{z}_{i,k}$ is bounded. So $z_{i,k}$ is continuously uniform, thus we get the conclusion of (21). \square

4 An illustrative example

In this section, an example is presented to show the effectiveness of the proposed adaptive iterative learning controller.

Consider the following second-order strict feedback nonlinear system:

$$\begin{aligned} \dot{x}_{1,k} &= x_{2,k} + \theta(t)x_{1,k}^2, \\ \dot{x}_{2,k} &= u_k(t) \\ y_k &= x_{1,k} \end{aligned} \quad (27)$$

where $t \in [0, 1]$, $\theta(t)$ is systems uncertain periodical time-varying parameter. After it is expanded by Fourier series, system (27) can be described as

$$\begin{aligned} \dot{x}_{1,k} &= x_{2,k} + \eta^T \phi(t)x_{1,k}^2 + \delta^T(t)x_{1,k}^2, \\ \dot{x}_{2,k} &= u_k(t) \\ y_k &= x_{1,k} \end{aligned} \quad (28)$$

where $x_{1,k}$ and $x_{2,k}$ are state variables, $u_k(t)$ is the input variable. $\eta = [\eta_1, \eta_2, \eta_3, \eta_4, \eta_5]^T$, $\phi(t) = [1, \sin(t), \cos(t), \sin(2t), \cos(2t)]^T$, $\|\delta(t)\| \leq s$, where s is an unknown constant. In order to simulate, we suppose $\theta(t) = \sin(2\pi t)$ in the actual system. Choose the reference trajectory $y_{r,k} = g_k \sin(2\pi t)$ with difference amplitudes. For the non-uniform trajectory case, we choose $g_k = -0.2$ when k is even, and $g_k = 0.1$ when k is odd.

Step 1. Let $z_{1,k} = x_{1,k} - y_{r,k}$, $z_{2,k} = x_{2,k} - \alpha_{1,k} - \dot{y}_{r,k}$, where the virtual control is taken as $\alpha_{1,k} = -c_1 z_{1,k} - \hat{\eta}_k \phi(t)x_{1,k}^2 - \frac{1}{\Delta_k} \hat{S}_k x_{1,k}^4 z_{1,k}^2$, $\Delta_k = \frac{a}{k^2}$, $\tau_{1,k} = \Gamma_1 \phi(t)x_{1,k}^2 z_{1,k}$, $\nu_{1,k} = \Gamma_2 \frac{1}{\Delta_k} x_{1,k}^4 z_{1,k}^2$.

Step 2. Design the controller $u_k(t) = -z_{1,k} - c_2 z_{2,k} + y_{r,k}^{(2)} - \hat{\eta}_k^T \phi(t) - \frac{\partial \alpha_{1,k}}{\partial x_{1,k}} x_{1,k}^2 + \frac{\partial \alpha_{1,k}}{\partial x_{1,k}} x_{2,k} + \frac{\partial \alpha_{1,k}}{\partial \hat{\eta}_k} \tau_{2,k} + \frac{\partial \alpha_{1,k}}{\partial \hat{S}_k} \nu_{2,k} - \hat{\eta}_k^T \dot{\phi}(t)x_{1,k}^2 - \hat{S}_k \frac{1}{\Delta_k} - \left| \frac{\partial \alpha_{1,k}}{\partial x_{1,k}} x_{1,k}^2 \right|^2 z_{2,k}$, where $\Delta_k = \frac{a}{k^2}$, $\tau_{2,k} = \tau_{1,k} + \Gamma_1 \phi(t) - \frac{\partial \alpha_{1,k}}{\partial x_{1,k}} x_{1,k}^2 |z_{2,k}$, $\nu_{2,k} = \nu_{1,k} + \Gamma_2 \frac{1}{\Delta_k} \left(\left| -\frac{\partial \alpha_{1,k}}{\partial x_{1,k}} x_{1,k}^2 \right| \right)^2 z_{2,k}^2$. Design the parameter adaptive laws: $\dot{\hat{\eta}}_k = \tau_{2,k}$, $\dot{\hat{S}}_k = \nu_{2,k}$.

Choose the following parameters and the initial values of states and the estimated parameters: $a = \frac{100}{3}$, $c_1 = c_2 = 0.1$, $\Gamma_1 = \text{diag}\{0.1\}$, $\Gamma_2 = 0.1$, $x_{1,k}(0) = 0$, $x_{2,k}(0) = -0.4$, $\hat{\eta}_k(0) = [0, 0, 0, 0, 0]^T$, $\hat{S}_k(0) = 0$. For the iteration index $k = 80$, the simulation results are shown in Figs. 1–5.

Simulation results in Figs. 1–5 show the effectiveness of the developed control scheme for system (27). From Figs. 1 and 2, it can be seen that good tracking performance is obtained, that is to say, the tracking error can converge to zero. Moreover, The boundedness of the control signal $\|u_k\|$ is illustrated on the interval $[0, 1]$ in Fig. 3. Parameter estimations $\|\hat{\eta}_k\|$, $\|\hat{S}_k\|$ are also bounded as given in Figs. 4 and 5.

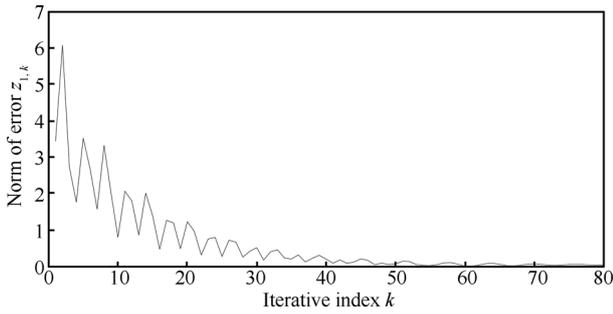


Fig. 1 Change of $\|z_{1,k}\|$ with iteration index

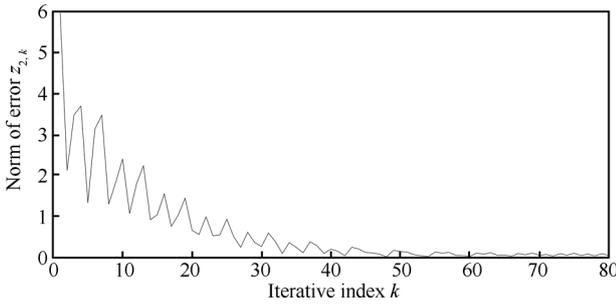


Fig. 2 Change of $\|z_{2,k}\|$ with iteration index

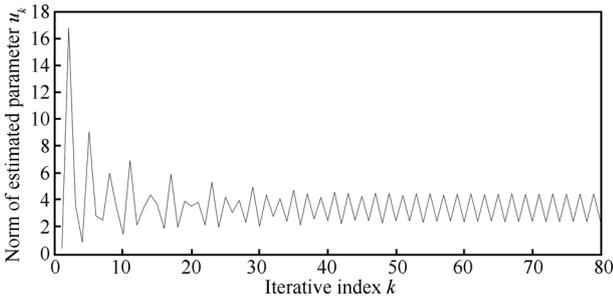


Fig. 3 Change of $\|u_k\|$ with iteration index

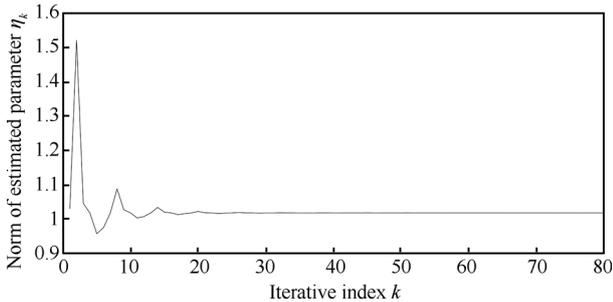


Fig. 4 Change of $\|\hat{\eta}_k\|$ with iteration index

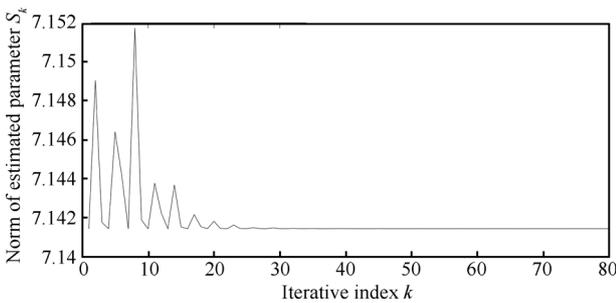


Fig. 5 Change of $\|\hat{S}_k\|$ with iteration index

5 Conclusions

This paper deals with the non-uniform trajectory tracking problem of a class of high-order nonlinear systems with unknown time-varying parameters. An adaptive iterative learning controller is designed for nonlinear systems with unknown time-varying parameters to realize the non-uniform trajectory tracking perfectly. Then, based on the Lyapunov stability theory, the asymptotic tracking of the controlled nonlinear system is proved. Simulation results demonstrate the effectiveness of the proposed control method. The future work is how to design the iterative learning controller for nonlinear systems with unknown time-varying parameters and uncertain control direction.

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