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# **Gait Modification and Optimization using Neural Network-Genetic Algorithm Approach: Application to Knee Rehabilitation**

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**Abstract**

Gait modification strategies play an important role in the overall success of total knee arthroplasty. There are a number of studies based on multi-body dynamic (MBD) analysis that have minimized knee adduction moment to offload knee joint. Reducing the knee adduction moment, without consideration of the actual contact pressure, has its own limitations. Moreover, MBD-based framework that mainly relies on iterative trial-and-error analysis, is fairly time consuming. This study embedded a time-delay neural network (TDNN) in a genetic algorithm (GA) as a cost effective computational framework to minimize contact pressure. Multi-body dynamic and finite element analyses were performed to calculate gait kinematics/kinetics and the resultant contact pressure for a number of experimental gait trials. A TDNN was trained to learn the nonlinear relation between gait parameters (inputs) and contact pressures (output). The trained network was then served as a real-time cost function in a GA-based global optimization to calculate contact pressure associated with each potential gait pattern. Two optimization problems were solved: first, knee flexion angle was bounded within the normal patterns and second, knee flexion angle was allowed to be increased beyond the normal walking. Designed gait patterns were evaluated through multi-body dynamic and finite element analyses.

The TDNN-GA resulted in realistic gait patterns, compared to literature, which could effectively reduce contact pressure at the medial tibiofemoral knee joint. The first optimized gait pattern reduced the knee contact pressure by up to 21% through modifying the adjacent joint kinematics whilst knee flexion was preserved within normal walking. The second optimized gait pattern achieved a more effective pressure reduction (25%) through a slight increase in the knee flexion at the cost of considerable increase in the ankle joint forces. The proposed approach is a cost-effective computational technique that can be used to design a variety of rehabilitation strategies for different joint replacement with multiple objectives.

**Keywords:** Gait modification, Tibiofemoral knee joint, Time delay neural network, Genetic algorithm, Contact pressure

## 1 **1. Introduction:**

2 Following total knee arthroplasty (TKA), rehabilitation strategies are of significant importance to accelerate  
3 patient recovery (Isaac et al., 2005, Klein et al., 2008), reinforce joint functionality (Moffet et al., 2004, Rahmann et  
4 al., 2009), decrease gait asymmetry (Zeni Jr et al., 2011), and augment the durability and life time of knee  
5 prostheses (Fransen, 2011, Mont et al., 2006). Gait rehabilitations mainly aim to decrease knee joint loading through  
6 minor changes in human gait patterns. However, recognizing the synergistic kinematic changes, required for joint  
7 offloading, is a challenging task, hence; computational approaches have been used to facilitate the design procedure.  
8 To best of our knowledge, most of the current literature on gait modification strategies have been designed through  
9 multi-body dynamic (MBD) analysis (Barrios et al., 2010, Barrios and Davis, 2007, Fregly et al., 2009, Hunt et al.,  
10 2008, Mündermann et al., 2008, Willson et al., 2001, Ackermann and van den Bogert, 2010, Anderson and Pandey,  
11 2001, Fregly et al., 2007) . However, iterative “trial-and-error” MBD analysis, that has been performed in such  
12 studies, is fairly time demanding which limits the applicability and generality of the method. Hence, a cost-effective  
13 computational framework that minimizes the computational cost is of particular interest.

14 Besides the computational cost, there are a number of aspects that have not been well addressed by the  
15 conventional MBD-based framework. First , MBD-based approach attempts to reduce the peak values of knee  
16 adduction moment (KAM) which is not always a reliable measure since decreasing KAM may not necessarily  
17 decrease knee joint loading (Walter et al., 2010); and the results of such approach are sensitive to the chosen  
18 reference frame (e.g. laboratory, floating reference frames) (Lin et al., 2001, Shull et al., 2012). Second , joint-  
19 offloading gait patterns are likely to decrease the contact area of articulating surfaces that unfavorably may increase  
20 the contact pressure at the knee joint (D'Lima et al., 2008). Therefore, reducing the contact pressure should be  
21 concerned as the principal goal of rehabilitation design. Conventional computational frameworks however are  
22 inherently unable to consider the contact pressure in the design procedure since the conventional methods require an  
23 explicit cost function whilst the relation between gait kinematics and the resultant contact pressure has not been  
24 stated explicitly before. Also, predicting the contact pressure requires implementing finite element analysis (FEA)  
25 which in turn increases the computational cost (Halloran et al., 2010). A cost-effective surrogate which releases the  
26 necessity of iterative FEA is therefore of significant advantage. Third, previous studies could not reach a general  
27 consensus about the contribution of knee flexion to the knee joint offloading. Knee flexion is a key synergetic  
28 parameter that is often increased within the clinical execution of the rehabilitation patterns (Barrios et al., 2010,  
29 Fregly et al., 2007, van den Noort et al., 2013). Several studies concluded that increasing the knee flexion would  
30 reduce KAM (Fregly et al., 2009, Fregly, 2008, Fregly et al., 2007), whilst others showed that it has no association  
31 with KAM (Creaby et al., 2013) or may even increase contact pressure at the knee bearing surfaces (D'Lima et al.,

32 2008). A systematic investigation is required to enhance our understanding of the contribution of knee flexion to  
33 the knee joint offloading.

34 Artificial neural networks (ANN) and genetic algorithm (GA) are two relatively new techniques in the field  
35 of biomechanics. Artificial neural network (ANN) can be used as a real-time surrogate model with the ability to  
36 learn a nonlinear relationship. Once a set of inputs and corresponding outputs are presented to the network, it will  
37 then “learn” the causal interactions between inputs and outputs. Given a new set of inputs, the trained neural network  
38 (surrogate model) can generalize the relationship to produce the associated outputs. The ANN surrogate therefore  
39 can be of significant advantage especially when the original model necessitates repeating a time-consuming  
40 computation. For example, ANN has been widely used as a surrogate of FEA (Campoli et al., 2012, Hambli, 2010,  
41 Hambli, 2011, Naito and Torii, 2005, Lu et al., 2013, Simic et al., 2011, Zadpoor et al., 2012). Genetic algorithm is a  
42 time-efficient global optimization technique which searches the entire data space to find the best solution (Goldberg,  
43 1989). In each iteration, only potential candidates that better optimize the cost function will survive to the next  
44 iteration. Thus, regardless of the initial point, the search data space is iteratively modified and GA will rapidly  
45 converge to the global optimum solution. This in turn assures the robustness of the method and minimizes the  
46 computational effort required to find the best solution. Moreover, GA is capable of dealing with multivariable data  
47 space, nonlinear input-output interactions and non-explicit, non-differential cost function.

48 Therefore, the overall aim of this study was to develop a hybrid framework of time delay neural network  
49 (TDNN) and genetic algorithm (GA) to address the aforementioned limitations of the literature. In particular this  
50 study aimed to (1) optimize the gait pattern in order to minimize the contact pressure at the knee articulating surfaces  
51 and (2) investigate the role of knee flexion in knee joint offloading. The advantage of the proposed approach was  
52 also compared over the existing knee rehabilitations in the literature.

## 53 **2. Materials and methods**

54 The proposed computational approach was implemented in the following steps:

55 Step 1) Experimental gait analysis data were obtained from the literature (Section 2.1), and imported into MBD  
56 analysis to calculate gait kinematics and kinetics (Section 2.2). Knee flexion angle and three dimensional knee joint  
57 loadings were predicted by MBD, and then served as boundary condition and loading profiles for the finite element  
58 simulation to calculate contact pressure (Section 2.3). Gait trials were then outlined via a number of kinematic  
59 features and the corresponding maximum contact pressure values (CPRESS-max) (Section 2.4).

60 Step 2) A time-delay neural network (TDNN) was trained to learn the nonlinear relationship between kinematic  
61 features as inputs and the corresponding CPRESS-max values as output (Section 2.5).

62 Step 3) A genetic algorithm (GA) was implemented to search for the optimum kinematic features (optimization  
63 variables) which minimized the CPRESS-max at the knee joint bearing surfaces. In this GA, the trained TDNN was  
64 served as a real-time cost function to calculate the objective value (CPRESS-max) (Section 2.6).

## 65 **2.1. Experimental gait data**

66 Experimental gait analysis data of a single subject with unilateral TKA (female, height 167 cm, mass 78.4  
67 kg) was obtained from the literature (<https://simtk.org/home/kneeloads>; accessed on June 2013). The subject walked  
68 with a variety of different gait patterns including normal, medial thrust, trunk sway, walking pole, bouncy, crouch,  
69 smooth and fore foot strike. Medial thrust, trunk sway and walking pole were knee rehabilitation strategies, designed  
70 to decrease KAM, whilst the remaining gait trials were different walking patterns to cover the span of executable gait  
71 for the subject. Compared to normal walking, the subject walked with a slightly decreased pelvis obliquity, slightly  
72 increased pelvis axial rotation and leg flexion to implement medial thrust pattern. For trunk sway pattern, the subject  
73 walked with an increased lateral leaning of the trunk in the frontal plane over the standing leg. In walking pole, the  
74 subject used bilateral poles as walking aids. For each gait pattern, five gait trials were repeated under the same  
75 walking condition at a self-selected pace. A total of two complete gait cycles were picked up from each trial, leading  
76 to a total of 84 data sets. For further details, see (Fregly et al., 2012). Gait trials were recorded in terms of marker  
77 trajectory data (Motion Analysis Corp., Santa Rosa, CA) and ground reaction forces (AMTI Corp., Watertown, MA).

## 78 **2.2. Multi-body dynamic**

79 Experimental ground reaction forces and marker trajectories were imported into the three-dimensional multi-  
80 body dynamic simulation software, AnyBody Modelling System (version 5.2, AnyBody Technology, Aalborg,  
81 Denmark). A lower extremity musculoskeletal model was used in AnyBody software based on the University of  
82 Twente Lower Extremity Model (TLEM) (Klein Horsman, 2007). This model, available in the AnyBody published  
83 repository, had 160 muscle units as well as foot, thigh, patella, shank, trunk and thorax segments. Hip joint was  
84 modelled as a spherical joint with three degrees of freedom (DOF): flexion-extension, abduction-adduction and  
85 internal-external rotation. Knee joint was modelled as a hinge joint with only one DOF for flexion-extension and  
86 universal joint was considered for ankle-subtalar complex. Since the assumptions of the simplified knee joint and  
87 rigid multi-bodies were made, the detailed knee implant was not considered in the MBD analysis. Knee flexion angle  
88 and three dimensional knee joint loads, aligned in medial-lateral, proximal-distal and anterior-posterior directions,  
89 were calculated for each complete gait cycle. A complete gait cycle was defined as the time period from heel strike of

one leg to the following heel strike of the same leg (Vaughan et al., 1992). Computations were then normalized to 100 samples to represent one complete gait cycle. Knee flexion and three dimensional knee joint loads then served as the boundary condition and load profiles for FEA.

### 2.3. Finite element method

A typical tibiofemoral knee implant was modelled in the commercial finite element package; ABAQUS/Explicit (version 6.12 Simulia Inc., Providence, RI) using the computer aided design (CAD) of a clinically available fixed bearing knee implant. The knee implant consisted of two main parts; femoral component and tibia insert. Rigid body assumptions were applied to both parts, with a simple linear elastic foundation model defined between the two contacting bodies (Halloran et al., 2005). Tetrahedral (C3D10M) elements were used to mesh the model in ABAQUS. Convergence was tested by decreasing the element size from 8 mm to 0.5 mm in five steps (8, 4, 2, 1, and 0.5 mm). The solution converged on contact pressure ( $\leq 5\%$ ) with over 86000 and 44000 elements representing the femoral component and the tibia insert respectively. This was also consistent with the previous mesh convergence studies for similar finite element models (Abdelgaied et al., 2011, Halloran et al., 2005). The physical interaction between femoral component and tibia insert was taken into account as a surface-to-surface contact (femur as the master surface and tibia as the slave surface) through a penalty-based approach with an isotropic friction coefficient of 0.04 (Abdelgaied et al., 2011, Halloran et al., 2005). The tibia insert was constrained in all available DOFs and the femoral component was only allowed for flexion-extension under the three dimensional load which were obtained from MBD analysis. The model calculated the contact pressure at each node for each time increment. An output field was created over all simulation frames to compute the maximum value of the contact pressures (CPRESS\_max) over the entire gait cycle. Since the medial compartment experiences the CPRESS-max value (Schipplein and Andriacchi, 1991), this part was considered for the rest of the study (Figure 1a).

### 2.4. Feature extraction

During a complete gait cycle, the extent to which a joint can be moved (range of motion) and the corresponding absolute values of motions directly affect the quality of human gait and joint loading. For example, increasing the “maximum” value of hip adduction angle or hip internal rotation would decrease the “peak” values of KAM (Barrios et al., 2010). On the other hand, to design a realistic gait modification strategy, the overall trend of kinematic patterns cannot differ significantly from natural human walking habitudes; otherwise the pattern would not be acceptable and executable by the patient. Thus, only the key features of kinematic waveforms are needed to be modified whilst the overall trends should be preserved consistent. Gait kinematics were therefore outlined through a

119 total of 39 descriptive kinematic features (Table 1 and Figure 1b). These features have been suggested in the literature  
 120 for a number of studies such as gait analysis (Collins et al., 2009, Gates et al., 2012a, Gates et al., 2012b), gait  
 121 classification (Armand et al., 2006) , evaluation of joint loading (Simonsen et al., 2010), and joint inter-  
 122 coordination (Wang et al., 2009). Kinematic features (optimization variables) were then allowed to vary within the  
 123 corresponding ranges of experimental values plus  $\pm 20\%$  variations to cover a thorough span of executable movement  
 124 patterns for the subject. Contact pressure was also characterized by the maximum pressure value occurred over the  
 125 entire gait cycle (CPRESS-max).

## 126 2.5. Time-delay neural network

127 Time delay neural network (TDNN) was implemented to model the highly nonlinear relationship between  
 128 kinematic features (39 inputs) and CPRESS-max values (one output). The trained network was then embedded in an  
 129 optimization process (GA) as a real-time cost function to calculate the objective values (CPRESS-max). The TDNN  
 130 architecture consisted of a feed forward neural network in which a tapped delay line was added to the input layer  
 131 (Figure 2). Similar to other types of neural networks, a number of processor units (neurons) were arranged in a  
 132 certain configuration (layers). A weighted sum of all inputs was fed into each hidden neuron where an activation  
 133 function acted on this weighted sum to produce the output of the hidden neuron. All of the hidden neurons were  
 134 activated using “hyperbolic tangent sigmoid” function which linearly scaled its input signal to  $[-1, 1]$  interval:

$$135 \quad y_j^m = \frac{2}{1 + \exp(-2 * V_j^m)} - 1 \quad j = 1, 2, \dots, M_m \quad (1)$$

136 Where  $y_j^m$  is the output of  $j^{\text{th}}$  hidden neuron located at the  $m^{\text{th}}$  hidden layer,  $M_m$  is the number of hidden neurons  
 137 at the  $m^{\text{th}}$  hidden layer, and  $V_j^m(n)$  is the weighted sum of the signals from the previous layer which was fed to the  $j^{\text{th}}$   
 138 hidden neuron of  $m^{\text{th}}$  hidden layer:

$$139 \quad V_j^m = \sum_{k=1}^{M_{m-1}} (y_k^{m-1} * W_{jk}) + b_j \quad j = 1, 2, \dots, M_m, \quad k = 1, 2, \dots, M_{m-1} \quad (2)$$

140 Where  $W_{jk}$  is the weight relating the output of  $k^{\text{th}}$  neuron located at the  $(m-1)^{\text{th}}$  layer ( $y_k^{m-1}$ ) to the  $j^{\text{th}}$  hidden neuron at  
 141 the  $m^{\text{th}}$  hidden layer with the bias value of  $b_j$ , and  $M_m$  and  $M_{m-1}$  are the number of neurons at the  $m^{\text{th}}$  and  $(m-1)^{\text{th}}$  layers  
 142 respectively. A weighted sum of all hidden neurons' outputs was also fed into the single output node which was  
 143 activated by a “pure line” function:

$$144 \quad y_{\text{out}} = \sum_{k=1}^{M_m} w_k y_k^m + \bar{y} \quad (3)$$

145 in which  $\bar{y}$  is the output bias .

146 TDNN was trained using the scaled conjugate gradient algorithm (SCG) (Møller, 1993). The available data  
 147 space, obtained from MBD and FEA, was randomly divided into three main parts: train (70%), validation (15%) and  
 148 test (15%) subsets. The train and validation subsets were used to train the network whilst the test subset was not  
 149 included in training. The network prediction error on the validation subset implied how accurate the network has  
 150 learned the input-output causal relationship (accuracy). On the other hand, the network prediction error on the test  
 151 subset indicated the extent to which the trained network could generalize this causal relationship for new inputs  
 152 (generality). Generally speaking, the structure of the FFANN would build a trade-off between “prediction accuracy”  
 153 and “generality”. Whilst increasing the number of hidden neurons/layers would increase the prediction accuracy,  
 154 using too many neurons would decrease the generality and increase the test error. The number of hidden layers and  
 155 hidden neurons were therefore determined according to the network prediction error for the test and validation  
 156 subsets. The input delay was also determined by trial and error.

## 157 2.6. Genetic algorithm

158 In the present study, gait optimization was stated as follows:

$$159 \text{ Minimize } Y : Y=U(X) \quad AX \leq b \quad , \quad X_L \leq X \leq X_U \quad (4)$$

160 Where Y is the CPRESS-max, X is the optimization variables (kinematic features), and U is the trained TDNN. Upper  
 161 and lower bounds of the optimization variables ( $X_L$  and  $X_U$ ) were obtained from the experimental gait trials plus  $\pm$   
 162 20% variations. Matrix A and vector b described the linear inequality constraints in order to control the natural trends  
 163 of the gait kinematics (Appendix). Genetic algorithm (GA) was used to search for those kinematic features that could  
 164 minimize CPRESS-max. Kinematic features (optimization variables) were configured as 1\*N arrays called  
 165 individuals (N=39). In each iteration, the GA created a population of individuals and then employed the trained  
 166 TDNN to calculate the resultant CPRESS-max values associated with potential individuals. Those individuals that  
 167 led to lower CPRESS-max values were assigned a higher survivorship probability to be selected and make the next  
 168 population. Each individual is indeed a potential solution and each population is a search space of solutions.  
 169 Accordingly, after passing several iterations, the population (solution search space) evolved toward the optimized  
 170 individuals.

171 The first population was initialized with random individuals in which features of gait kinematics were  
 172 randomly chosen due to  $X_L$  and  $X_U$ . The next populations were created through selected individuals by elitism,

173 crossover and mutation operators of GA (Goldberg, 1989). Table 2 summarizes the setting of the proposed GA in  
174 MATLAB (v.2009, Genetic Algorithm toolbox). In the present study, two systematic optimizations were performed:  
175 first, knee flexion was bounded to vary within the normal walking. Second, the knee flexion was allowed to vary  
176 beyond the normal walking up to the medial thrust pattern. Once the GA converged to the optimum kinematic  
177 features, a typical normal gait cycle was adjusted to these optimum features using the curve fitting technique and the  
178 optimized gait pattern was reconstructed. Figure 3 shows schematic of the proposed combined TDNN-GA  
179 methodology in this study.

### 180 3. Results

#### 181 3.1. Network training

182 A four-layer TDNN with four delay units at its input layer , 20 hidden neurons at the first hidden layer and 15  
183 hidden neurons at the second one, was trained using 70% of the generated data base. Then, it was validated and tested  
184 with the remaining 30%. Figure 4 shows the average performance of the proposed network over 100 training and  
185 testing repetitions, each time with a random selection of subsets(Iyer and Rhinehart, 1999). According to the results,  
186 the TDNN could accurately predict CPRESS-max values for the training, validation and test subsets. Pearson  
187 correlation coefficients, between network predictions (Y axis) and real outputs (X axis), were all above  $p=0.98$ .  
188 Figures 4a, b show that the network learned the nonlinear interaction of kinematics and contact pressure variables  
189 ( $p=0.99$ ). Figure 4c shows that the network could predict the CPRESS-max values corresponding to new sets of  
190 kinematics which were not included in the training data space ( $p=0.98$ ).

#### 191 3.2. Optimization problem

192 The crossover fraction substantially affects the convergence of GA. Optimization was therefore run for a  
193 variety of different values of crossover fraction ranged from 0 to 1 in the step size of 0.05. The crossover fraction of  
194 0.85 led to the lowest CPRESS-max value (see Figure 5). Thus, this value was adopted for the rest of this study. In  
195 the first optimization problem, knee flexion angle was bounded within normal walking. The algorithm was  
196 terminated after 75 populations due to stall generation criterion, in which the average change of the objective value  
197 (CPRESS-max) was less than  $10^{-6}$  (function tolerance) over 50 populations (stall generations). Figure 6a shows the  
198 mean and the best CPRESS-max values associated with each population. After successful convergence of the  
199 algorithm, TDNN-GA achieved the lowest CPRESS-max value of 25.58 MPa for the best individual of the last  
200 population.

201 Using curve fitting technique, a typical normal gait cycle was adjusted to the obtained optimum kinematic  
202 features and the optimized gait pattern was reconstructed (Figure 7). The optimized kinematics laid within the  
203 experimental gait patterns suggesting that it would be feasible for the subject to execute the optimized pattern. Using  
204 multi-body dynamic analysis, the corresponding joint loadings were computed and compared with the span of  
205 experimental values (Figure 8). Results show that lower extremity joints (ankle, knee and hip) underwent realistic  
206 loading conditions i.e. within and with similar pattern to the experimental gait trials. Particularly, hip joint loading  
207 was generally low in the anterior-posterior direction. A general reduction at the anterior-posterior component of knee  
208 joint loading and significant reduction at its medial-lateral component around 40%-60% of the gait cycle occurred.  
209 Moreover, the medial-lateral component of ankle joint loading was significantly decreased accompanied with a  
210 reduction at its anterior-posterior component around 40%-60% of the gait cycle. Figure 9 shows the resultant  
211 distribution of the maximum contact pressure at the medial tibiofemoral joint over the entire gait cycle. The  
212 maximum contact pressure was reduced by 21.8% compared to the normal walking, while previously published gait  
213 modifications were fairly ineffective to decrease the contact pressure magnitudes.

214 In the second optimization problem,  $X_L$  and  $X_U$  were modified and the knee joint flexion was bounded  
215 between normal and medial thrust patterns. The GA achieved the convergence value of 24.61 MPa after 77  
216 populations (Figure 6b). Reconstructed gait kinematics and the resultant joint loading patterns are presented in  
217 Figures 7 and 8 respectively. Results demonstrate that the second optimized gait pattern also laid within the span of  
218 executable gait patterns. The second optimized gait modification led to a significant reduction at the three  
219 dimensional hip joint loading (anterior-posterior, proximal-distal and medial-lateral) around 0-25% of the gait cycle.  
220 This pattern also led to an overall reduction at anterior-posterior component of the knee joint loading. Anterior-  
221 posterior and medial-lateral components of the ankle joint loading were substantially low at 0-25% of the gait cycle,  
222 however ankle joint loading was slightly increased around 40%-60% of the gait cycle. By comparison, the second  
223 optimization problem yielded to a more effective gait modification pattern that better reduced the magnitude of the  
224 contact pressure by up to 25% (Figure 9).

## 225 4. Discussion

### 226 4.1. Hybrid neural network-genetic algorithm

227 Neural network was employed: first, to model the highly nonlinear relationship between gait kinematics and  
228 contact pressure; second, to serve as a real-time cost function that allowed the optimization algorithm to be  
229 performed in a reasonable computation time. A recent study by Lu et al. (2013) demonstrated that the dynamic

230 structure of a time delay neural network was preferred for modelling the relation between tibiofemoral cartilage load  
231 (input) and von Mises stress (output), compared to the traditional static feed forward neural network. Therefore, this  
232 structure was used in this study. Moreover, neural network has been used to calculate joint loading from ground  
233 reaction forces and gait kinematics (Ardestani et al., 2013, Ardestani et al., 2014) and ground reaction force from gait  
234 kinematics (Oh et al., 2013, Ren et al., 2008). In this study, neural network was employed to calculate the contact  
235 pressure from gait kinematics. The high correlation that was found between the target values and the network  
236 predictions for validation and test subsets reassures the reliability of the proposed structure. The TDNN in turn  
237 necessitated involving the GA as the optimization technique. In fact, other classical optimization approaches mainly  
238 rely on iterative derivation of an explicit cost function however TDNN modelled the problem non-explicitly.

#### 239 **4. 2. Current research contribution**

240 There are a number of implications on the gait modification and optimization both in terms of methodology and  
241 findings. Major limitations of the previous studies were addressed in the present research. First, compared to  
242 previous studies in which iterative “trial-and-error” MBD analysis has been used, this study presented a cost-  
243 effective computational alternative. TDNN provided a real-time cost function for the GA that could rapidly evaluate  
244 the contact pressure associated with each potential gait pattern. Moreover, GA is a stochastic direct search method in  
245 which the search data space is modified iteratively. This in turn reduced the computational effort required to find the  
246 optimized solution. It should be pointed out that although various gait modifications have been developed in  
247 association with knee joint offloading, none of them have yet been accepted as a general modification strategy. In  
248 fact, due to the large inter-patient variability, reported in gait kinematics and joint loading patterns (Kutzner et al.,  
249 2010, Taylor et al., 2004), gait rehabilitation strategies should be determined patient specifically. Hence, to design a  
250 gait modification strategy, it is crucial that the proposed computational method is cost-effective and easy to recreate.

251 Second, unlike the previous studies in which KAM reduction has been the principal goal of gait modification,  
252 here, contact pressure was adopted as a more accurate criterion for knee joint offloading. This in turn built more  
253 confidence in the efficiency of the proposed gait modification. Previous gait modifications were mainly designed to  
254 reduce knee joint moment. Although these modification patterns could decrease knee joint loading, none of them  
255 could decrease contact pressure at the knee joint bearing surfaces whilst the proposed gait pattern in this study could  
256 effectively decrease the contact pressure by up to 25% (see Figure 9).

257 Third, whilst previous studies have debated on the influence of increasing knee flexion, this study could  
258 address the contribution of knee flexion angle to the knee joint offloading in a systematic manner. Two optimizations  
259 were performed: first, knee flexion angle was kept within normal patterns to investigate whether it was possible to

260 decrease knee joint loading through adjacent joints effects. Second, knee flexion was allowed for a non-significant  
261 increase. Results showed that in the first optimized gait, contact pressure was reduced by up to 21% whilst knee  
262 flexion was preserved within normal walking. In the second optimized pattern, a more effective pressure reduction  
263 (25%) was achieved with a slight increase in the knee flexion at the cost of considerable increase in the ankle joint  
264 forces at 40-60% of the gait cycle. This observation is consistent with previous studies (Fregly et al., 2007) and  
265 suggests that perhaps the first optimization pattern in which joint reaction forces were within the experimental range  
266 might be more physiologically feasible. Allowing the knee flexion angle to be more increased led to higher ankle  
267 joint loading and a gradual reduction in the contact area which in turn increased contact pressure.

268 Overall, hip adduction, ankle flexion, subtalar eversion, pelvis posterior rotation and pelvis medial-lateral  
269 rotation were increased during the stance phase for both optimized gait patterns (see Figure 7). However it should be  
270 noted that the exact amount of kinematic changes, compared to normal gait, was not reported in this study since  
271 specific gait rehabilitation, designed for a particular subject, may not be equally applicable for other patients.  
272 Therefore, the quantitative amount of kinematic variations, compared to normal gait, was not focused in this study.

### 273 **4. 3. Limitations**

274 There were several limitations in this study: (1) there was a lack of clinical investigation on the estimated  
275 kinematics. Nevertheless, from a technical point of view, the predicted kinematic waveforms are expected to be  
276 feasible since the TDNN was trained based on executable walking patterns. Once the network learns this dynamic, it  
277 uses this dynamic as the acting function to respond to new sets of inputs. Therefore, it is unlikely that it would  
278 generate highly aberrant kinematics. Regardless, further investigations are required to test whether the predicted  
279 kinematics is feasible to implement for compensatory or unexpected effects on the other joints or the contra-lateral  
280 limb; (2) rigid body constraints were applied to both the femoral and tibia components. Halloran et al.(2005) showed  
281 that rigid body analysis of the tibiofemoral knee implant can calculate contact pressure in an acceptable consistence  
282 with a full deformable model whilst rigid body analysis would be much more time-efficient. Therefore, in order to  
283 produce the training data base, required to train the neural network, rigid body constraints were applied. This was  
284 consistent with the present multi-body dynamic analysis in which no detailed modelling on the knee implant was  
285 included; (3) a typical knee implant was adopted in the present study. Although this implant has been widely used in  
286 literature (Clayton et al., 2006, Dalury et al., 2008, Ranawat et al., 2004, Willing and Kim, 2011) , its dimensions  
287 were different from the original knee prosthesis by which the subject was implanted. In fact, the subject was  
288 implanted with a custom-made sensor-based prosthesis which was specifically produced to measure in vivo knee  
289 joint loading(Fregly et al., 2012). Accordingly, in this study , a typical commercial knee implant was preferred to test  
the

290 efficiency of the proposed knee rehabilitation patterns. Nevertheless, the proposed methodology should be equally  
291 applicable to other implant geometries and (4) the knee joint was modelled with only one DOF (flexion-extension).  
292 Although six DOFs are possible for the knee joint, the dominant movement of the knee joint takes place in the  
293 sagittal plane and knee joint has been mostly simplified as a hinge joint, especially for the knee rehabilitation design  
294 purposes (Ackermann and van den Bogert, 2010, Anderson and Pandy, 2001, Fregly et al., 2007).

## 295 **5. Conclusion**

296 A time-delay neural network was embedded in a genetic algorithm to predict a gait pattern that would  
297 minimize the contact pressure at the knee joint bearing surfaces. The proposed algorithm suggested an optimum gait  
298 pattern in which hip adduction, ankle flexion, subtalar eversion , pelvis posterior rotation and pelvis medial-lateral  
299 rotation were slightly increased during the stance phase. Compared to the available gait rehabilitations, the proposed  
300 gait pattern could decrease the knee contact pressure by up to 25%. Compared to the conventional MBD-based  
301 framework in gait rehabilitation design, the present methodology facilitated a more practical and reliable design  
302 procedure at a lower computational cost :(1) instead of using knee adduction moment, contact pressure was  
303 considered as a more accurate criterion which led to a more efficient gait modification, (2) using the time-delay  
304 neural network, the proposed computational framework was considerably faster and time-efficient. The  
305 computational framework therefore can be easily repeated for any given subject. Moreover, (3) the conflicting effect  
306 of the knee flexion was addressed through two systematic optimization frameworks: (i) knee joint may be offloaded  
307 without any changes in the knee flexion angle (ii) a slight increase in the knee flexion angle might better reduce  
308 contact pressure but at the cost of ankle joint over loading and (iii) large increase in the knee flexion angle reduced  
309 the contact area and yielded to an increase in the contact pressure.

310 Various future direction from this study can be considered: (1) on the methodological level, more rigorous  
311 tribological metrics (e.g. wear), constraints (e.g. energy expenditure) or gait balance requirements can be included  
312 into the computational framework to enhance the predications; (2) on the validation level, further clinical studies are  
313 required to validate the finding of such studies; (3) on a wider application level, the proposed methodology in this  
314 study has wider implications in design and development of rehabilitation protocols for broader numbers of subjects  
315 and other joints such as hip and ankle.

**316 Conflict of interest statement**

317 The authors have no conflict of interests to be declared.

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465

466

Table 1 Description of gait kinematic features

Joint	Kinematic feature	Description
Hip	H1	Hip flexion at initial contact
Hip	H2	Maximum hip extension at stance
Hip	H3	Maximum hip flexion at swing phase
Hip	H4	Hip abduction at initial contact
Hip	H5	Maximum hip adduction at midstance phase
Hip	H6	Maximum hip adduction at stance phase
Hip	H7	Hip external rotation at initial contact
Hip	H8	Maximum hip internal rotation at swing phase
Knee	K1	Knee flexion at initial contact
Knee	K2	Maximum knee flexion at stance
Knee	K3	Maximum knee extension at stance
Knee	K4	Maximum knee flexion at swing phase
Ankle	A1	Ankle flexion at initial contact
Ankle	A2	Maximum ankle dorsiflexion at midstance
Ankle	A3	Maximum ankle dorsiflexion at stance
Ankle	A4	Maximum ankle plantar flexion at swing phase
Subtalar	S1	Subtalar inversion at initial contact
Subtalar	S2	Maximum subtalar eversion at stance
Subtalar	S3	Maximum subtalar inversion at stance
Subtalar	S4	Maximum subtalar eversion at swing
Pelvis	PP1	Maximum posterior tilt of pelvis
Pelvis	PP2	Maximum anterior tilt of the pelvis
Pelvis	PP3	Maximum lateral obliquity of the pelvis
Pelvis	PP4	Maximum medial obliquity of the pelvis
Pelvis	PP5	Pelvis vertical position at initial contact
Pelvis	PP6	Maximum pelvis upward position at stance
Pelvis	PP7	Maximum pelvis downward position at stance
Pelvis	PP8	Maximum pelvis upward position at swing
Pelvis	PR1	Pelvis anterior rotation at initial contact
Pelvis	PR2	Maximum pelvis posterior rotation at stance
Pelvis	PR3	Maximum pelvis posterior rotation at swing
Pelvis	PR4	Pelvis medial rotation at initial contact
Pelvis	PR5	Maximum pelvis lateral rotation at stance
Pelvis	PR6	Maximum pelvis medial rotation at stance
Pelvis	PR7	Maximum pelvis lateral rotation at swing
Pelvis	PR8	Pelvis axial rotation at initial contact
Pelvis	PR9	Maximum pelvis axial rotation to the left at stance
Pelvis	PR10	Minimum pelvis axial rotation to the right at stance
Pelvis	PR11	Maximum pelvis axial rotation to the left at swing

Table 2 Genetic algorithm settings in MATLAB

<b>Genetic algorithm parameter</b>	<b>Value</b>
Population size	50
Scaling function	Rank
Selection function	Tournament
Elite count	2
Crossover fraction	0.85
Crossover function	Single point
Mutation function	Adaptive feasible
Maximum number of generations	100

**Figure 1**

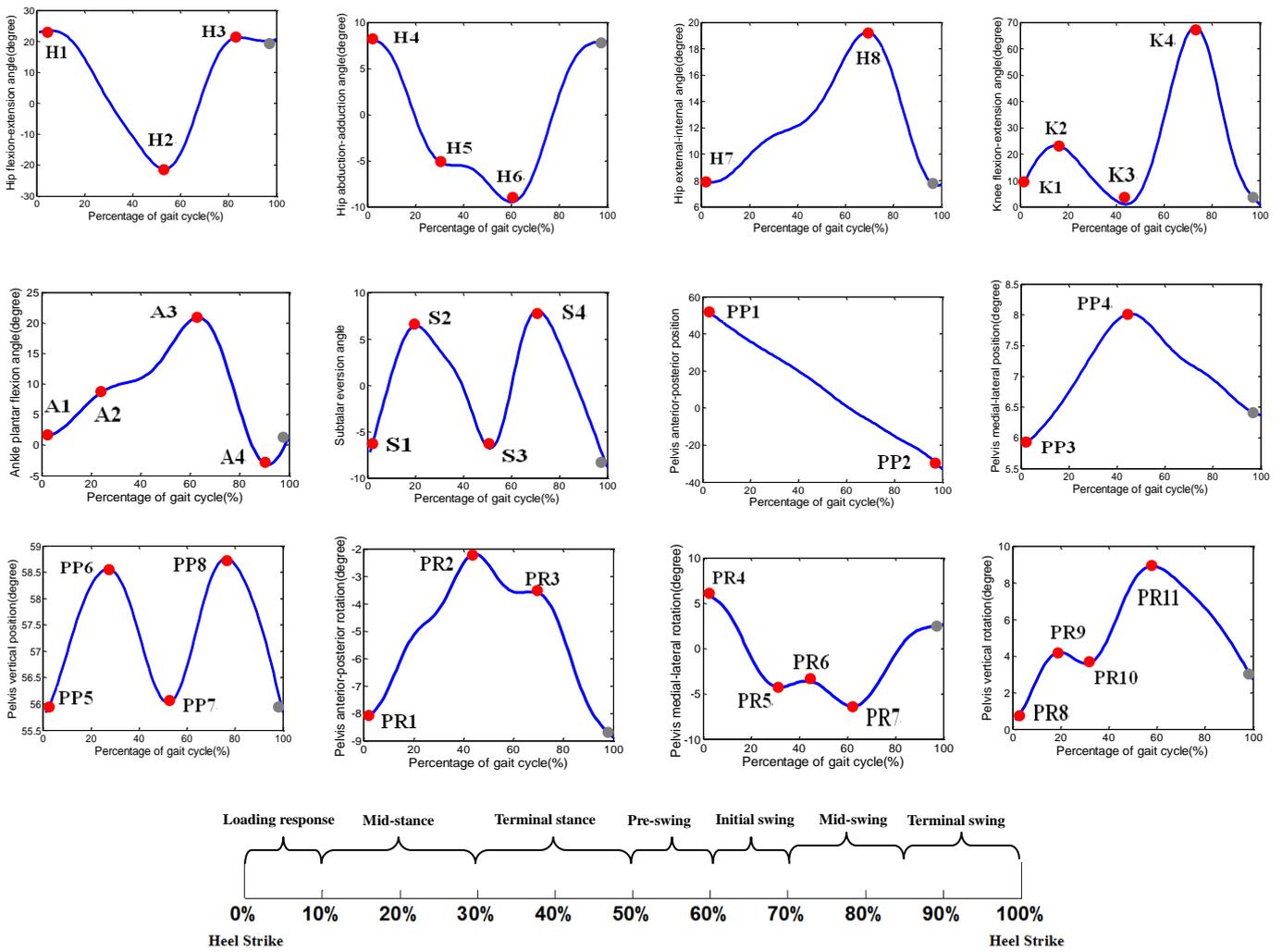
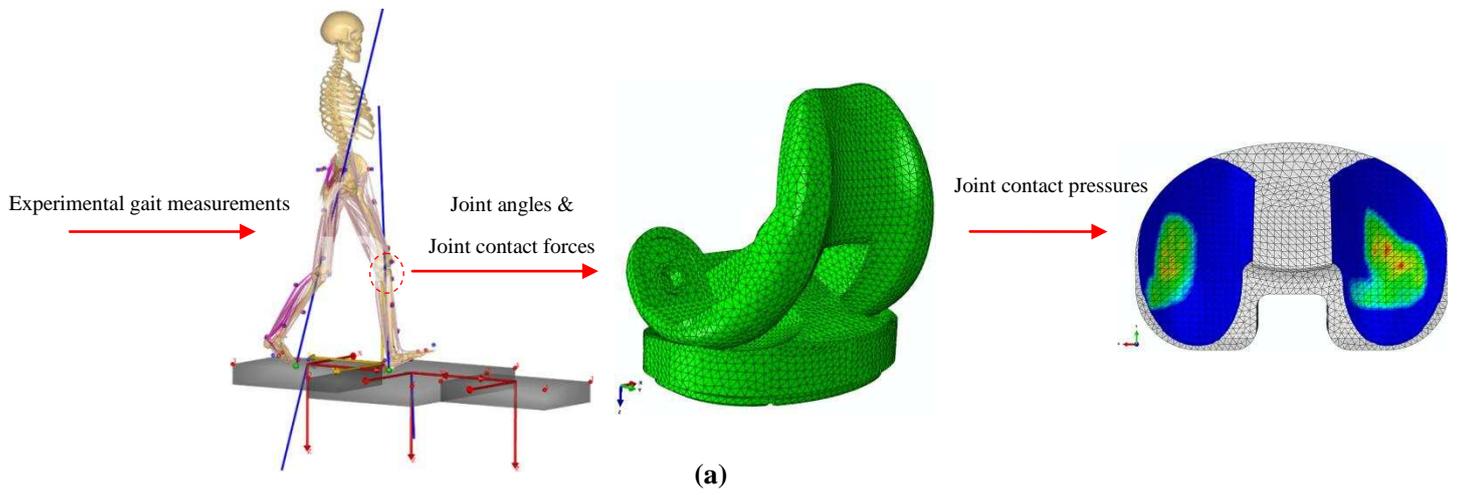


Figure 1 (a) Experimental gait measurements were imported into multi-body dynamics analysis to calculate joint kinematics/kinetics which were then used by finite element analysis to calculate contact pressure (b) Joint angles were parameterized by extremum features (red circles). Due to the periodicity of the gait, joint angle values at the end of the gait cycle (gray points) were equal to the initial values at 0% of the gait cycle except for pelvis anterior-posterior position.

Figure 2

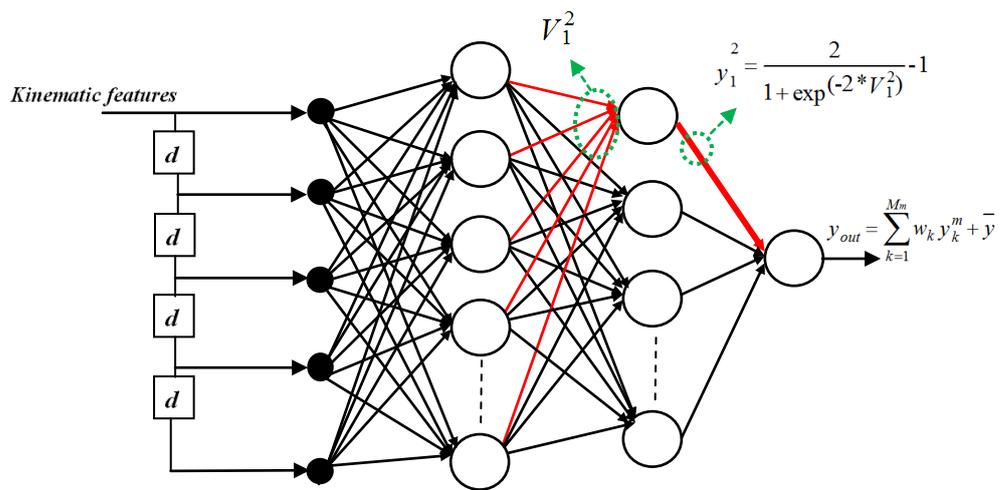


Figure 2 A schematic diagram of a four-layer TDNN used in this study. The network calculated the maximum values of contact pressure (output) based on gait features (inputs).

Figure 3

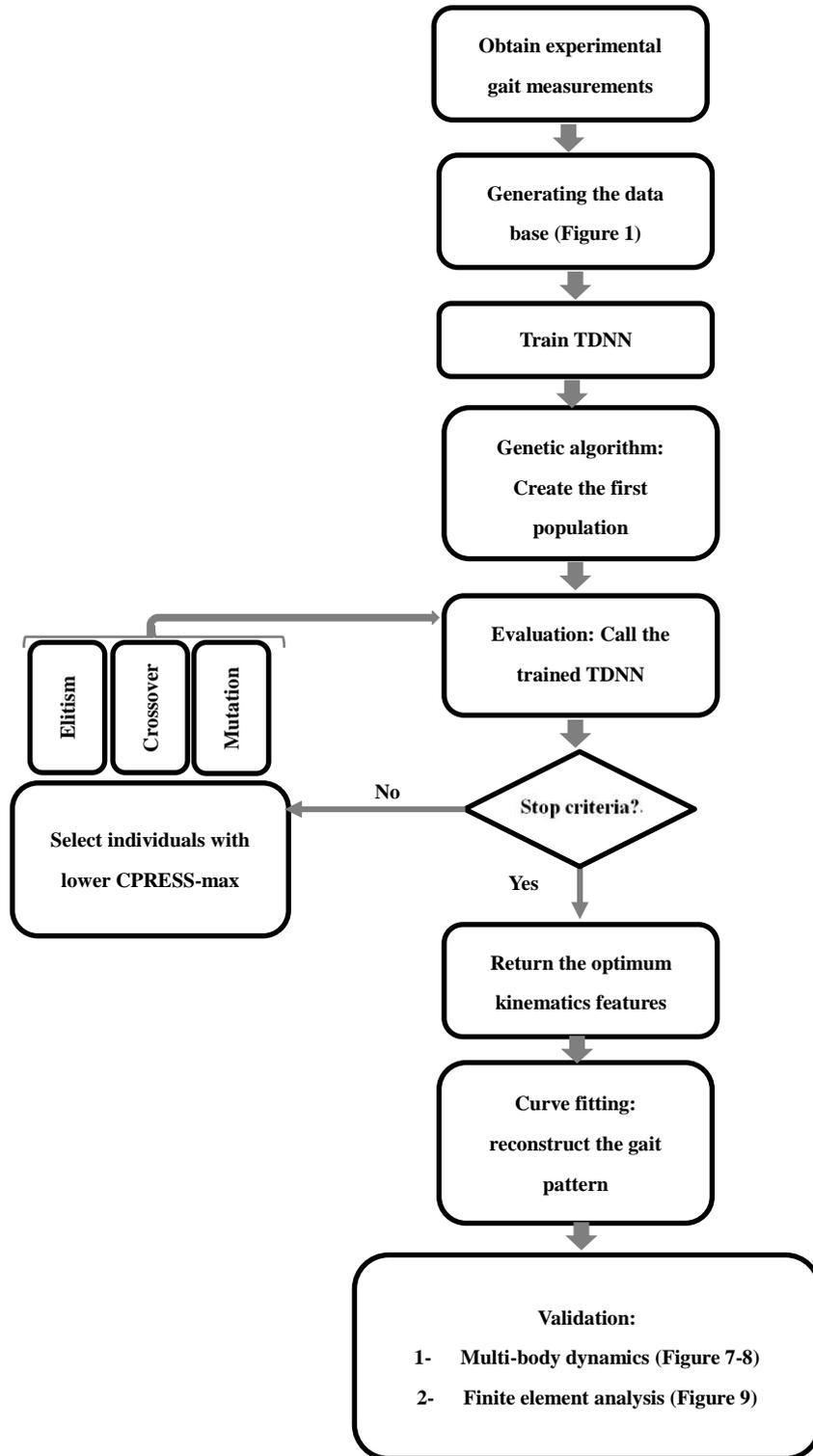


Figure 3 The flowchart of the proposed TDNN-GA.

Figure 4

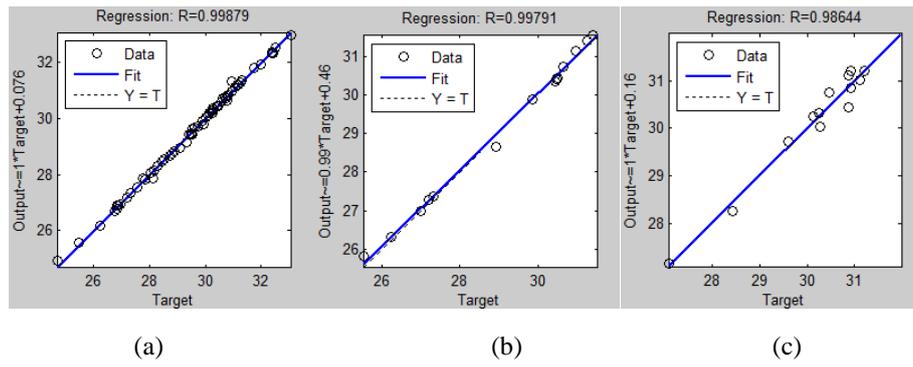


Figure 4 Network predictions versus actual CPRESS-max values for (a) train (b) validation and (c) test subsets.

Figure 5

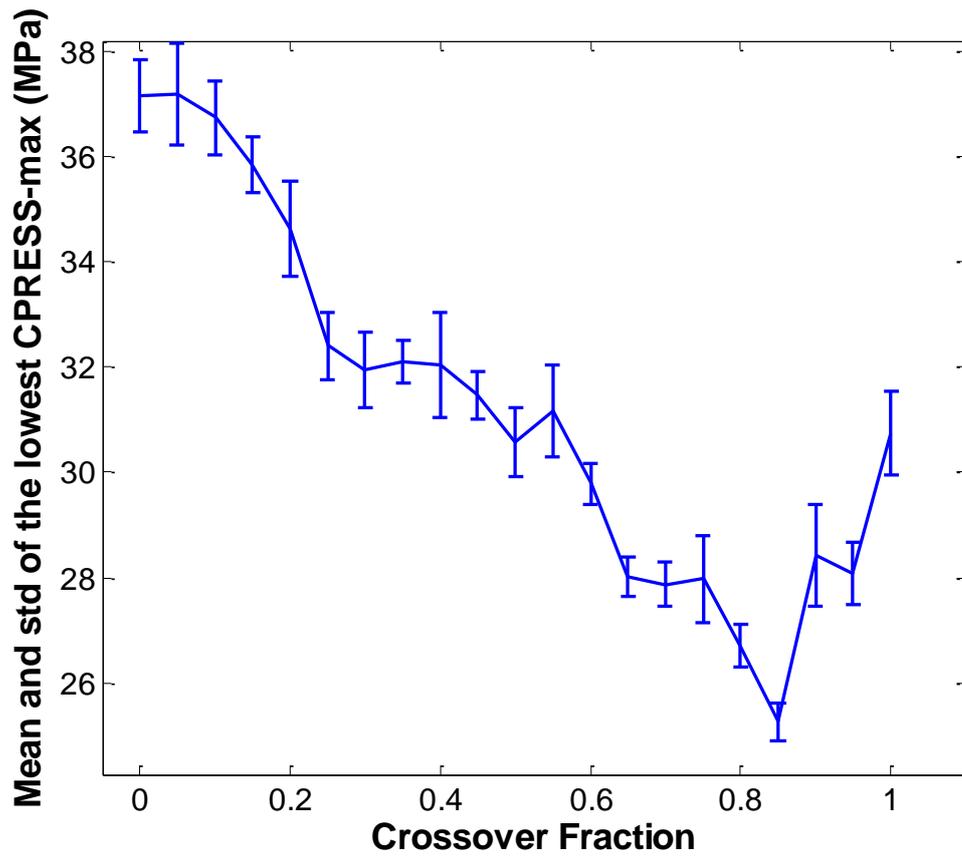
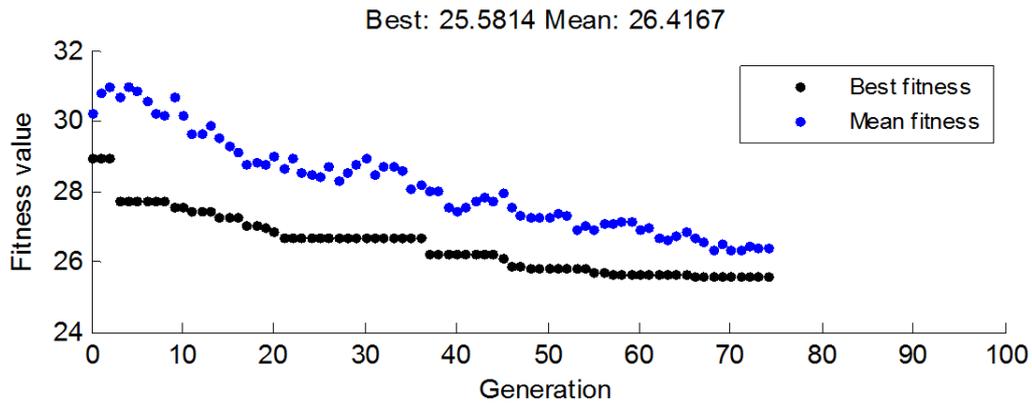
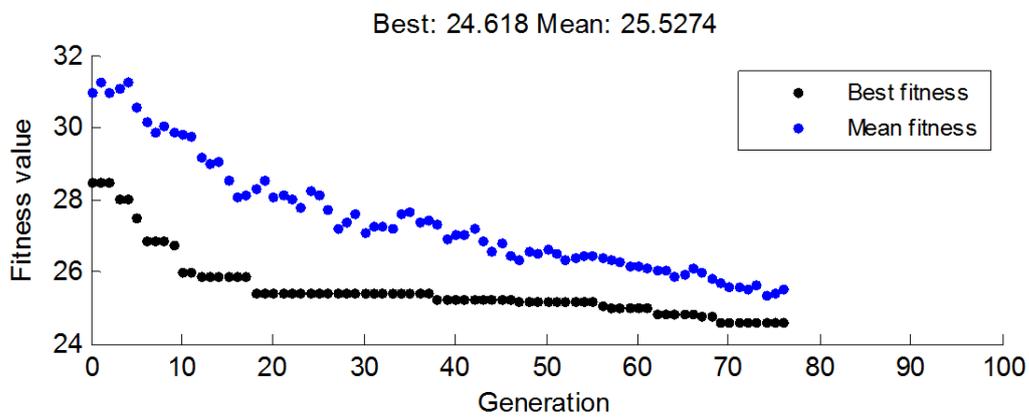


Figure 5 Mean and standard deviation of the optimized CPRESS-max for different values of crossover fraction in the GA process.

Figure 6



(a)



(b)

Figure 6 Convergence of the GA for (a) the first optimization problem in which the knee flexion angle was bounded to normal patterns,(b) the second optimization problem in which the knee flexion angle was allowed to increase beyond normal pattern. “fitness” refers to the calculated value of CPRESS-max for each individual.

Figure 7

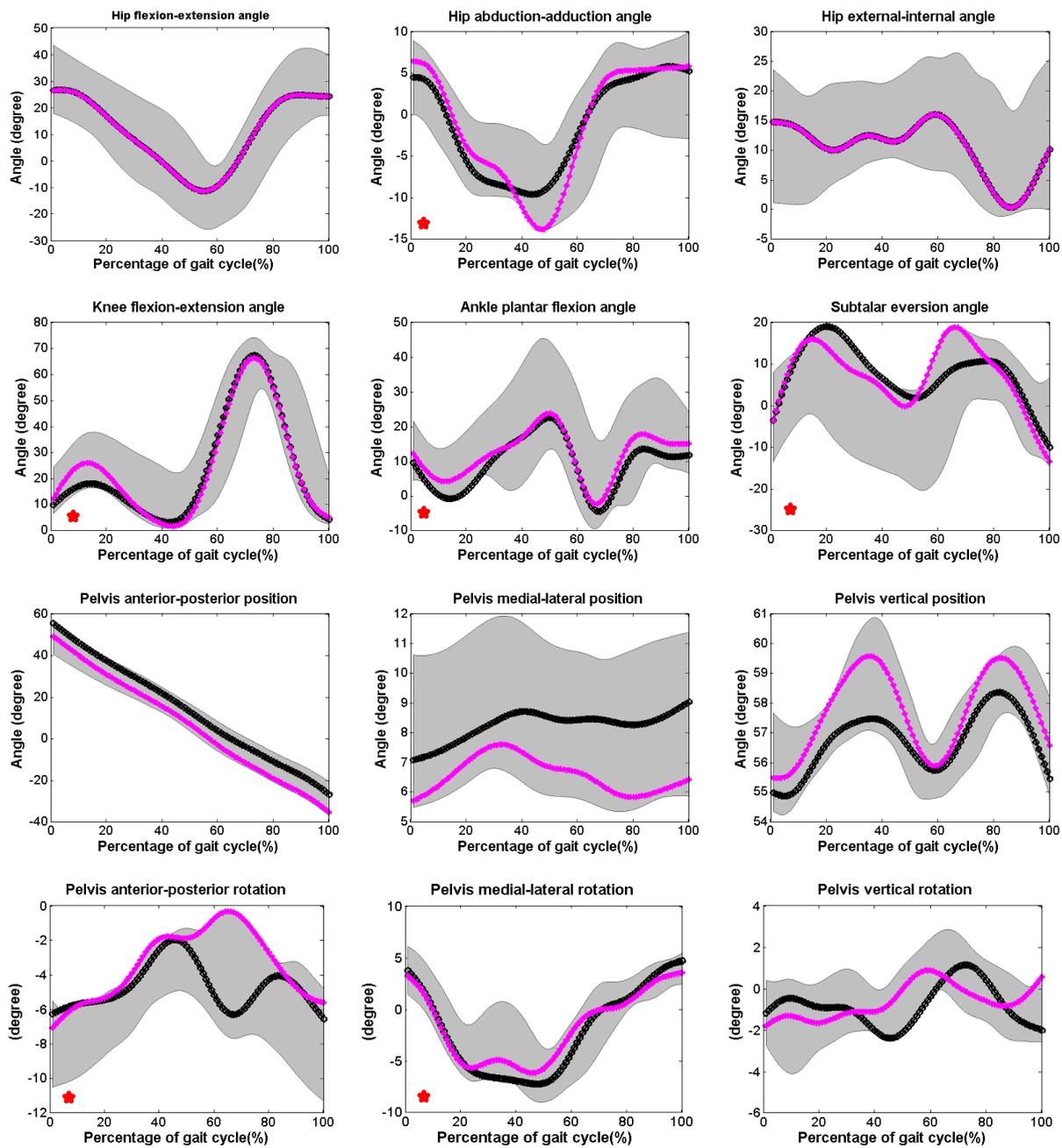


Figure 7 Kinematics of the first optimized gait pattern (black line) and the second optimized pattern (pink line) laid within the extent of experimental gait trials (gray span). Those kinematics that underwent considerable changes have been marked by \*

Figure 8

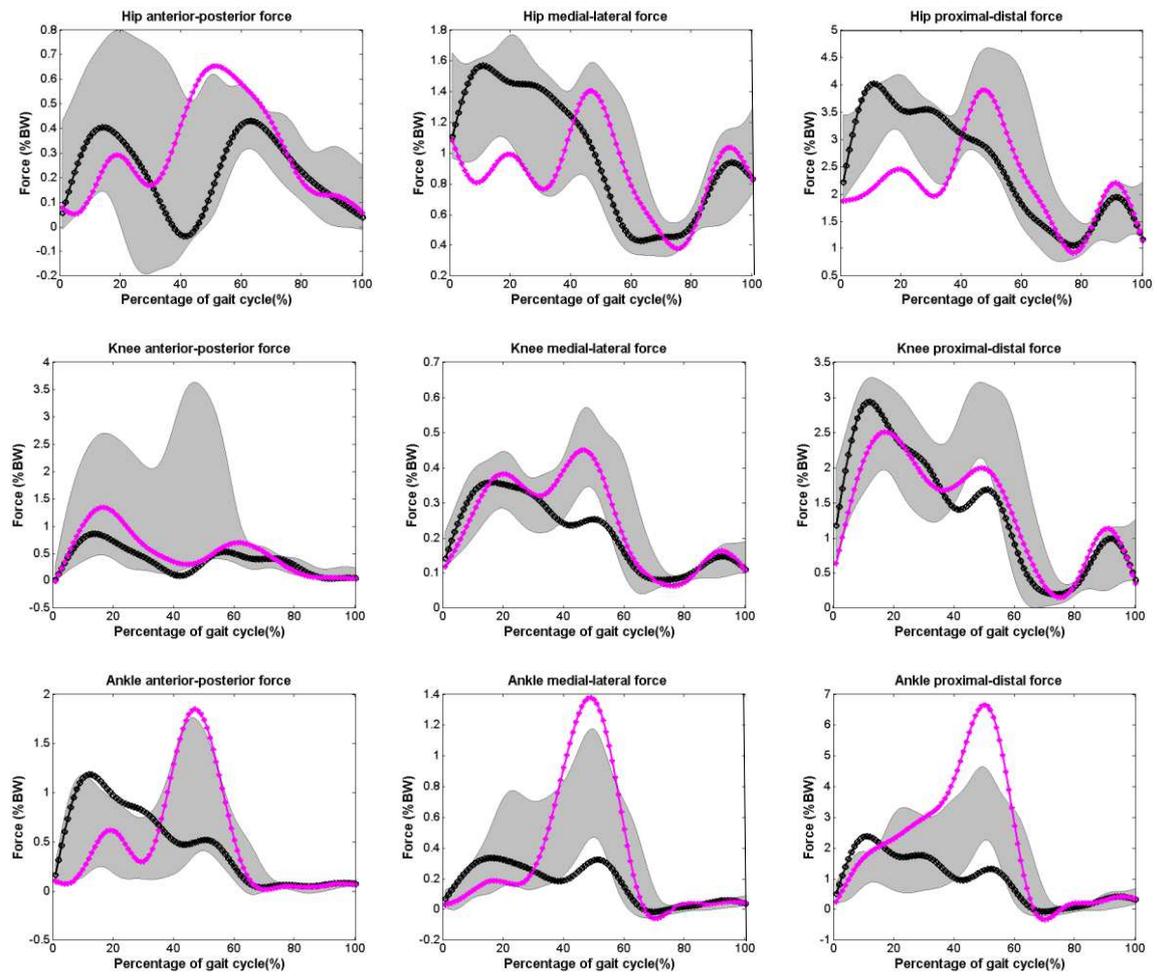


Figure 8 Resultant joint contact forces of the first optimized gait pattern (black line) and the second optimized pattern (pink line) laid within the extent of experimental gait trials (gray span).

Figure 9

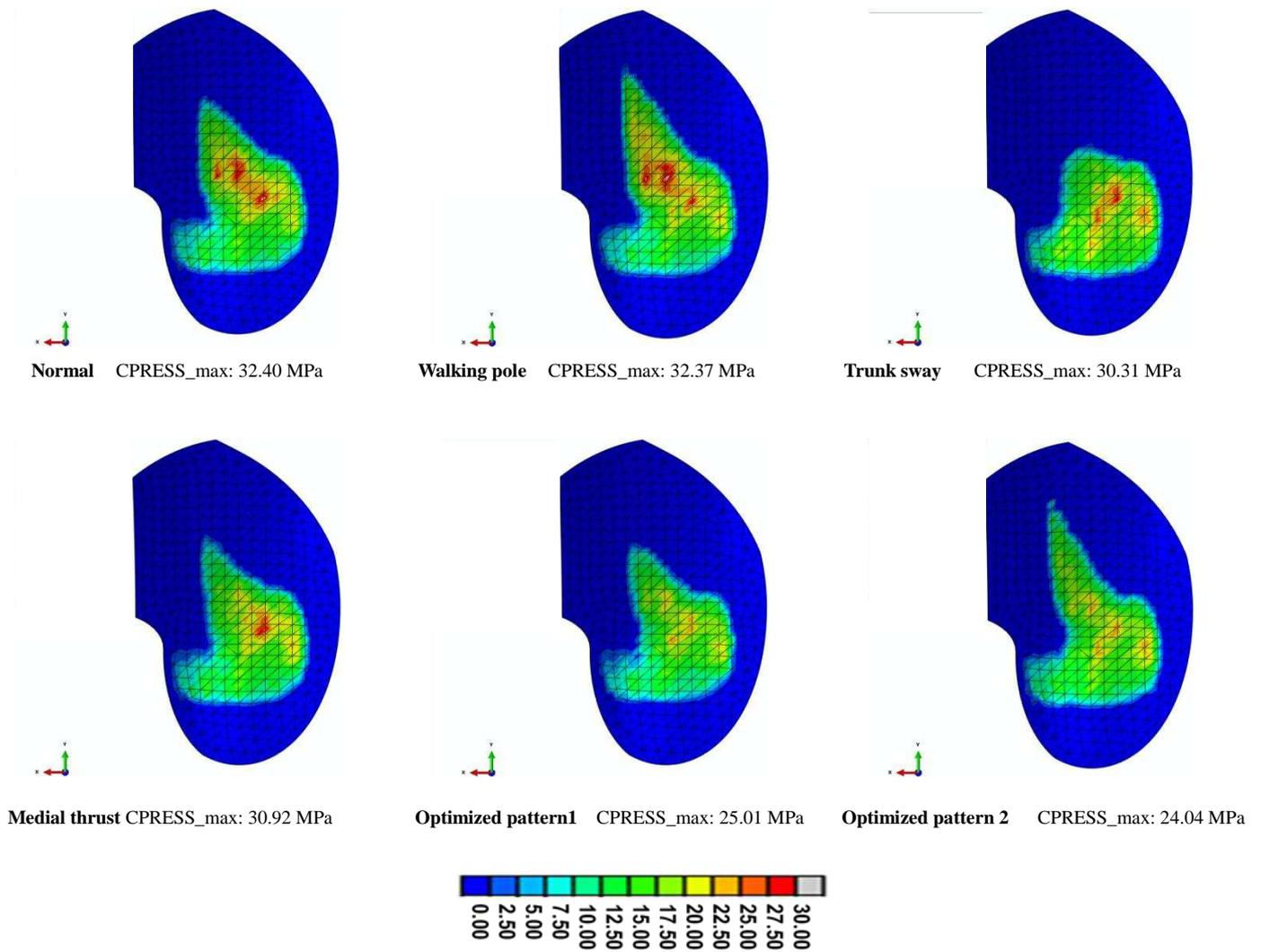


Figure 9 The resultant maximum values of contact pressures for the optimized gait patterns versus contact pressures obtained from normal gait and other previously published gait modifications.

**Supplementary Material**

[Click here to download Supplementary Material: Appendix.docx](#)