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Integration of Range Split Spectrum Interferometry and Conventional InSAR to

Monitor Large Gradient Surface Displacements

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Abstract: Incorrect unwrapping of dense interferometric fringes caused by large gradient displacements make 12 it difficult to measure mining subsidence using conventional Interferometric Synthetic Aperture Radar (InSAR). 13 14 This paper presents a Range Split Spectrum Interferometry assisted Phase Unwrapping (R-SSIaPU) method for 15 the first time. The R-SSIaPU method takes advantage of (i) the capability of Range Split Spectrum Interferometry of measuring surface displacements with large spatial gradients, and (ii) the capability of 16 conventional InSAR of being sensitive to surface displacements with limited spatial gradients. Both simulated 17 and real experiments show that the R-SSIaPU method can monitor large gradient mining-induced surface 18 movements with high precision. In the case of the Tangjiahui mine, the R-SSIaPU method agreed with GPS 19 with differences of approximately 4.2 cm, whilst conventional InSAR deviated from GPS with differences of 20 nearly 1 m. The R-SSIaPU method makes phase unwrapping less challenge, especially in the cases with large 21 surface displacements. In addition to mining subsidence, it is believed that the R-SSIaPU method can be used 22 to monitor surface displacements caused by landslides, earthquakes, volcanic eruptions, and glacier movements. 23

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Key Words: Mining-induced Surface Displacements; Large Gradient Displacements; Range Split Spectrum
 Interferometry; InSAR; Phase Unwrapping

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29 **1 Introduction**

Interferometric Synthetic Aperture Radar (InSAR) has been proved to be a powerful geodetic tool to monitor surface displacements caused by natural and anthropogenic processes such as earthquakes, landslides, volcanic eruptions, and mine subsidence (Cheloni et al., 2017; Cigna et al., 2014, 2017; Du et al., 2017; Simran et al., 2017; Dai et al., 2016; Tomas et al., 2014; Reinisch et al., 2017; Werner et al., 2017; Ng et al., 2017). One major limitation of InSAR is its inability to measure surface diplacements with large spatial gradients (Massonnet et al, 1998; Singleton et al., 2014).

In the region of large gradient surface diplacements caused by underground mining, unwrapping a SAR interferogram using conventional methods is difficult or even fails (Chen et al, 2001). That makes it difficult to measure large gradient surface diplacements using conventional InSAR. SAR pixel offset, also known as SAR feature tracking, was proposed to monitor large gradient surface displacements (Werner et al., 2001; Pathier et

40 al., 2006; Yang et al., 2017). SAR pixel offset can measure large gradient surface displacements using SAR

- amplitude images, which has several advantages over conventional InSAR, e.g. not requiring phase unwrapping, 41 and not being strongly limited to regions of high coherence. Note that ionosphere can impact on both phase 42 measurements and azimuth offsets (Chen and Zebker, 2014). SAR pixel offset can measure displacement vectors 43 44 in the radar line of sight (i.e. range) direction as well as the satellite flight (i.e. azimuth) direction, which are 45 complementary to conventional InSAR since the latter only provides LOS surface displacements (Singleton et al., 2014). However, the precision of the pixel offsets depends on the pixel size of the SAR images, typically 46 1/20-1/30 of a pixel under the precondition of precise registration (Casu et al, 2011; Chen et al, 2015; Zhao et 47 al., 2013). Furthermore it can only be applicable to areas with contrasting surface features (natural or man-made) 48 and may fail in areas with limited terrain features (Singleton et al., 2014). 49
- Range Split Spectrum Interferometry (R-SSI) applies InSAR to sub-range images obtained by splitting the 50 51 available range bandwidth and explores the double differential phase through the partial interferograms to 52 measure large gradient displacements, which cannot be measured by conventional InSAR. R-SSI has been 53 applied successfully to measure large gradient displacements caused by earthquakes (Jiang et al, 2017) and landslides (Shi et al, 2017). Note, R-SSI has a low sensitivity to surface displacements compared with the InSAR 54 method, as well as a high sensitivity to a pixel's signal to clutter ratio (SCR), which prevents the R-SSI method 55 from measuring small displacements. But R-SSI has advantages over SAR pixel offset since it is less dependent 56 57 on surface features. In order to monitor mining-induced surface displacements with fewer terrain features in 58 detail, a new method, integrating R-SSI with conventional InSAR, which we denote as Range Split Spectrum 59 Interferometry assisted Phase Unwrapping method (R-SSIaPU), is proposed. Different from the existing methods (Libert et al, 2017a, 2017b) which first unwrap conventional InSAR interferogram and then connect 60 disconnected unwrapped patches using split spectrum interferometry, the R-SSIaPU method removes the first-61 order surface displacements estimated with the split spectrum interferometry, unwrap the residual interferogram 62 63 and then add back the first-order displacements. The R-SSIaPU method avoids to unwrap interferograms with large gradient displacements, which makes phase unwrapping less challenge. The test shows the R-SSIaPU 64 method can measure precisely the mining displacement in both the subsidence centre and edge. 65
- The paper is organized as follows. In Section II, the principle of the R-SSIaPU method is presented. In Sections
 III and IV, the performance of the R-SSIaPU method is analysed by simulated and real experiments respectively.
 In Section V, conclusions are given.

69 2 Method

70 2.1 Large gradient displacements estimated using Range Split Spectrum Interferometry (R-SSI)

For any SAR image, its full range-spectrum, acquired at a centre frequency of f_0 can be split into two nonoverlapping sub-bands at different carrier frequencies, f_H and f_L (indices *H* for the high sub-band and *L* for the low sub-band), using band-pass filtering (Fabio et al., 2013; Fattahi et al., 2017). A pair of SAR images (indices *M* for master and *S* for slave) at each sub-band can be used to generate two sub-band interferograms:

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$$\Phi_{H}^{W} = Angle \left(I_{M,H} \mathbf{g} \mathbf{f}_{S,H}^{*} \right) = -2\pi \mathbf{g} K_{H} - \frac{4\pi}{c} \mathbf{g} \Delta d \mathbf{g} f_{H}$$
(1)

$$\Phi_L^W = Angle \left(I_{M,L} g f_{S,L}^* \right) = -2\pi g K_L - \frac{4\pi}{c} g \Delta d g f_L$$
⁽²⁾

where $Angle(\Box)$ is an operator computing the phase angles, the asterisk indicates conjugate, K is the integer cycle number, c is the velocity of light, Δd is the ground displacement between the acquisitions. So the 80 double difference phase Φ_{Split}^{W} is given by:

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$$\Phi_{Split}^{W} = \Phi_{H}^{W} - \Phi_{L}^{W} = -2\pi \mathbf{g} (K_{H} - K_{L}) - \frac{4\pi}{c} \mathbf{g} \Delta d \mathbf{g} (f_{H} - f_{L})$$

$$= -2\pi \mathbf{g} K_{Split} - \frac{4\pi}{c} \mathbf{g} \Delta d \mathbf{g} f_{Split}$$
(3)

82 If f_{split} is smaller than f_H and f_L , the interferometric fringe density of Φ_{split}^W is sparser than Φ_H^W and 83 Φ_L^W . It is easier to unwrap Φ_{split}^W than unwrap Φ_H^W and Φ_L^W . It is important to measure large gradient 84 displacements which often lead to too dense interference fringes to be unwrapped. Then, the displacement can 85 be computed as follows:

$$\Delta d = -\frac{Unwrap(\Phi_{split}^{W} + 2\pi \Box K_{split})}{4\pi} \Box \frac{c}{f_{split}}$$

$$= -\frac{Unwrap(\Phi_{split}^{W})}{4\pi} \Box \frac{c}{f_{split}}$$
(4)

87 where $Unwrap(\Box)$ is an unwrapping operator.

88 Measurement uncertainty is calculated as (Bamler and Eineder, 2005):

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$$\sigma_{\Delta d} = \frac{1}{4\pi} \Box \frac{c}{f_{Split}} \Box \sigma_{\Phi^{W}_{Split}}$$
(5)

90 where $\sigma_{\Delta d}$ and $\sigma_{\Phi^W_{Split}}$ are the standard deviations of Δd and Φ^W_{Split} , respectively. $\sigma_{\Phi^W_{Split}}$ is given by:

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$$\sigma_{\Phi_{Split}^{W}} = \sqrt{\sigma_{\Phi_{H}}^{2} + \sigma_{\Phi_{L}}^{2}}$$
(6)

92 where $\sigma_{\Phi_{H}^{W}}^{2}$ and $\sigma_{\Phi_{L}^{W}}^{2}$ are the variances of Φ_{H}^{W} and Φ_{L}^{W} , respectively. $\sigma_{\Phi_{H}^{W}}^{2}$ can be approximated by 93 (Rodriguez et al., 1992):

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$$\sigma_{\Phi_{H}^{W}}^{2} \approx \frac{1}{2N} \Box \frac{1-\rho^{2}}{\rho^{2}}$$
(7)

95 where *N* is the effective number of looks and ρ is the total correlation of Φ_H^W . The variance of Φ_L^W can 96 be also defined by Equation (7) similar to Φ_H^W .

97 2.2 The R-SSIaPU method

Despite the R-SSI method being able to measure the large gradient displacements, it has a lower accuracy than
 the InSAR method. The InSAR method can measure small displacements precisely, but it cannot measure large

gradient displacements precisely due to phase unwrapping errors caused by over dense interference fringes. A 100 concept proposed by Yun et al. (2007) is to unwrap the residual phase after a large gradient displacement phase 101 has been subtracted from a low-frequency and low-accuracy measurement, e.g. SAR pixel offsets. Based on this 102 concept, we proposed the Range Split Spectrum Interferometry assisted Phase Unwrapping (R-SSIaPU) method. 103 Fig. 1 shows the workflow of the R-SSIaPU method. The R-SSI displacement is given by the R-SSI method. 104 105 De Zan et al. (2015) reported that a pure late-multilooking (i.e. multilooking is done at double differential interferogram level rather than at standard interferogram level) fails to reach the theoretical performance bound 106 of Delta-k methods, but combining the late-multilooking with some multilooking at standard interferogram level 107 can significantly improve the efficiency. As shown in Fig 1, an adaptive filter (Goldstein and Werner, 1998) is 108 applied to both high and low band interferograms before generating the double differential interferogram, and 109 110 then a minimum cost-flow (MCF) algorithm (Costantini, 1998) is used for spatial phase unwrapping. Due to the low precision of the unwrapped double differential interferogram, a non-local filter is applied to reduce noise 111 112 before converting it to surface displacements. Unlike local filters, non-local mean filtering takes a mean of all pixels in the image, weighted by how similar these pixels are to the target pixel. This results in much greater 113 post-filtering clarity, and less loss of detail in the image compared with local algorithms (Buades et al., 2005). 114 Then the surface displacements are converted to an initial InSAR unwrapped interferogram using the original 115 116 radar wavelength. The full resolution wrapped interferogram is given by conventional InSAR processing. Then the wrapped residual interferogram is generated by complex conjugate multiplication between the full resolution 117 InSAR wrapped interferogram and the R-SSI derived initial InSAR unwrapped interferogram. The wrapped 118 residual interferogram is filtered and unwrapped by the MCF method. Note that the noise level of the wrapped 119 residual interferogram is low since the InSAR wrapped interferogram is filtered at the step of the DInSAR 120 processing and the R-SSI derived initial InSAR unwrapped interferogram is derived from the filtered unwrapped 121 122 double differential interferogram. Therebefore, the adaptive filter (Goldstein and Werner, 1998) instead of non-123 local mean filter is used to improve the efficiency of the algorithm. The final unwrapped interferogram is obtained by adding the unwrapped residual interferogram with the R-SSI derived InSAR unwrapped 124 interferogram. Then the final unwrapped interferogram is converted to surface displacements using the original 125 126 radar wavelength.

127 It should be noted that the performance of the R-SSIaPU method depends on the precision of the R-SSI 128 displacement map to some extent. If the precision is low, the R-SSIaPU might not work adequately. The 129 precision of the R-SSI displacement map is given by the high-band interferograms phase noise, low-band 130 interferograms phase noise and the total available range bandwidth. The lower the phase noise is, the higher the 131 precision is. The larger the total available range bandwidth is, which gives a smaller wavelength of split

132 spectrum (c/f_{Split}) , the higher the precision is. Moreover, the performance of the R-SSIaPU method depends

on the radar wavelength. If the radar wavelength is shorter, which requires higher precise initial surface
displacements, the R-SSIaPU could not work adequately. Consequently, the R-SSIaPU method is more
appropriate to L-band ALOS-2, which has a longer radar wavelength than X-band TerraSAR-X or C-band
Sentinel-1. This is proved by the following simulated test.



Fig. 1 The workflow of the R-SSIaPU method. Note that the workflow of the R-SSI method is indicated bythe red dashed box.

142 3 Case Study 1: simulated mining-induced surface displacements

In order to assess the performance of the R-SSIaPU method, according to the probability integral model (Fan et al, 2014; Zhang et al, 2009), the horizontal and vertical displacements caused by coal mining are simulated on a 50×60 grid. The size of the grid point is 20×20 m. The simulated north, east and vertical displacements are shown in Fig. 2 (a), (b) and (c), respectively.





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Fig. 2. Simulated mining-induced surface displacements for three different SAR sensors: (a) Northing
displacements; (b) Easting displacements; (c) Vertical displacements; (d) LOS displacements for TerraSAR-X;
(e) LOS displacements for Sentinel-1; (f) LOS displacements for ALOS-2; (g) wrapped interferogram for

TerraSAR-X; (h) wrapped interferogram for Sentinel-1; (i) wrapped interferogram for ALOS-2; (j) LOS
displacements for TerraSAR-X derived from (g); (k) LOS displacements for Sentinel-1 derived from (h); (l)
LOS displacements for ALOS-2 derived from (i).

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It is clear in Fig. 2 (a) and (b) that the simulated horizontal displacements are mainly distributed at the edge of the subsidence bowl, and the displacement direction points to the centre of the subsidence bowl. The maximum displacement in the south-north direction is 110 cm, and the maximum displacement in the east-west direction is 102 cm. It is clear in Fig. 2 (c) that the centre of the subsidence bowl is dominated by vertical displacement, and the maximum displacement is 406 cm. The horizontal and vertical displacements are rescaled based on the spatial resolution listed in Table 1 and then are converted to displacements in the LOS direction (Fig 2 (d)-(f)) using Equation (8) in a matrix form.

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$$d_{los} = -\left[\sin\left(\theta_{i}\right)\csc\left(\theta_{h} - \frac{3}{2}\pi\right) \quad \sin\left(\theta_{i}\right)\csc\left(\theta_{h} - \frac{3}{2}\pi\right) \quad \cos\left(\theta_{i}\right)\right]\left[d_{sn} \quad d_{ew} \quad d_{v}\right]^{\mathrm{T}}$$
(8)

164 where d_{los} is the displacement in the LOS direction, θ_i and θ_h are the incidence angle and heading angle

165 respectively, d_{sn} , d_{ew} and d_v are the displacements in south-north, east-west and vertical direction 166 respectively.

167 The LOS surface displacements (Fig 2(d)-(f)) were converted into phase and then wrapped to generate 168 conventional InSAR interferograms (Fig 2(g)-(i)). Obvious phase discontinuities can be observed in the 169 subsidence trough in the simulated TerraSAR-X, Sentinel-1 and ALOS-2 interferograms (Fig 2(g)-(i)), which is 170 entirely due to the fact that the phase gradients exceed the maximum detectable phase gradient i.e. one fringe 171 per pixel (Massonnet and Feigl, 1998). Comparing Fig 2(j)-(l) with Fig 2(d)-(f), it is clear that conventional 172 InSAR failed to recover the simulated mining-induced surface displacements with all the three different SAR 173 images.

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Table 1. SAR satellite characteristics relevant to simulation studies.

Bands		Satellites	Mode	Spatial resolution (m)	Heading angle (°)	Incidence angle (°)	Bandwidth (MHz)	Radar Frequency (GHz)
	Х	TerraSAR-X	SM	2	189.49	42.79	100	9.65
	С	Sentinel-1	IWS	20	346.80	39.18	48	5.40
	L	ALOS-2	SM	6.7	357.88	27.80	38	1.24

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It is reported in Bamler and Eineder (2005) that the accuracy of the surface displacements estimated by the R-176 177 SSI method is maximized when the bandwidth of each sub-band is one third of the total bandwidth. Therefore, a band-pass filtering was employed to split the range bandwidth listed in Table 1 to form the sub-bands at $\pm B/3$ 178 (B is range bandwidth) from the radar frequencies with the sub-band bandwidth of B/3 (Furuya et al., 2017). 179 This band-pass filtering was done before the co-registration of the SLCs to avoid the impacts of spectral shifts 180 at the step of the resampling of the slave SLC image. The sub-band SLCs were demodulated to shift the spectrum 181 to the center of the sampled spectrum with a phase ramp and to change the center frequencies to the new values. 182 Using the centric frequencies of each sub-bands, the LOS displacements are transformed into phases and then 183 wrapped into wrapped interferograms. Gaussian noise of a form $N = (0, \sigma = 10^{\circ})$ was added to each 184 simulated sub-band wrapped interferogram. Then, the simulated high band, low band and conventional InSAR 185

wrapped interferograms are processed as the workflow presented in Fig. 1. The residual errors are presented inFig. 3 and the RMS statistics are listed in Table 2.



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Fig. 3. Residuals between the simulated and calculated LOS displacements: (a)-(c) are derived from
conventional InSAR, the R-SSI method and the R-SSIaPU method for TerraSAR-X; (d)-(f) are the same as (a)(c), but for Sentinel-1; (g)-(i) are the same as (a)-(c), but for ALOS-2.

Table 2. Maximum detectable displacements over a distance of 100 m and the corresponding RMS statistics
 for different approaches

Satellites	d _{max,LOS} of InSAR ^(a) (m)	d _{max,LOS} of R-SSI (m)	Radar wavelength (m)	Wavelength of R-SSI ^(b) (m)	Accuracy of InSAR displacements (mm)	Accuracy of R-SSI displacements (mm)	Accuracy of R-SSIaPU displacements (mm)
TerraSAR- X	0.388	56.213	0.031	4.497	743.8	19.4	24.1
Sentinel-1	0.070	11.638	0.056	9.310	784.5	40.1	47.3
ALOS-2	0.896	44.157	0.240	11.834	764.9	52.5	21.1
					7.00 H		2 1

195 (a) $d_{max,LOS}$ is the maximum detectable displacement in the LOS direction which is given by $d_{max,LOS} \approx \frac{w}{g_{resolution}} \frac{\lambda}{4}$, where,

196 $g_{resolution}$ is the pixel resolution and W (100 m in this paper) is the radius of the subsidence bowl, λ is the wavelength (Ng et al., 197 2017). (b) Wavelength of R-SSI= c/f_{Split} .

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It can be seen that for all the three satellites, the conventional InSAR method gives large residual errors (Fig. 3 (a), (d) and (g)) in the centre of the subsidence bowl, where phase unwrapping errors occur due to the dense fringes caused by the large gradient displacements which exceed the maximum detectable phase gradients of conventional InSAR i.e. one fringe per pixel (Massonnet and Feigl, 1998). The residual errors (Fig. 3 (b), (e)

and (h)), derived from the R-SSI method are small. The smallest R-SSI RMS is given by the TSX-1 satellite 203 since it has the smallest wavelength of R-SSI while the same noise level as that of Sentinel-1 and ALOS-2 (see 204 equation 5). For the TSX-1 and S1-A satellites the R-SSIaPU method cannot improve the accuracies (Fig. 3 (c) 205 and (f)). This is because the shorter wavelength (3.1 cm for TSX-1 and 5.6 cm for S1-A) requires higher 206 sensitivity to the displacement gradient provided by the R-SSI method. For the ALOS-2 pair, a significant 207 208 improvement can be seen in most areas and the improvement ratio of RMS is 59.7%. However, there are large residuals (Fig. 3 (i)) in some small areas resulting from the uncertainties in the R-SSI derived surface 209 displacements. These residuals are an integer multiple of half of the radar wavelength and may be corrected 210 manually in some cases. 211

4 Case Study 2: Subsidence at the Tangjiahui coal mine, China

The study area is located in the Tangjiahui coal mining area in the Inner Mongolia autonomous region, China 213 214 (Fig. 4). The TangJiahui coal mine is located in the northeastern margin of the Ordos syncline in the North China platform. The basic structure is a monoclinic structure with undulating waves and a near north-south 215 strike. The northern strata strike of the structure is nearly the east-west whilst its southern strata strike changes 216 to the northwest. The outline of the structure likes an ear. The dip angle at the edge of the basin is slightly larger 217 218 and a short back syncline whose axial direction is approximately parallel to the edge of the basin exists. The dip 219 in the basin is small, usually below 10 degrees, and there is a sublevel fold which is perpendicular to the strata strike. The sublevel fold is generally small and has little extension, resulting in the relative fluctuation of the 220 seam floor contour. Fractures in the coalfield are not developed, and only a few small tensile faults exist. In the 221 TangJiahui coal mine, the elevation at the north is greater than that at the south. The highest point is located in 222 the northeast of the well field and the lowest point located in the south of the well field. The maximum elevation 223 difference is 195.57 m and the average elevation is 1220-1300 m. As part of the Ordos Plateau, the area is 224 covered by quaternary loess with ravines and gullies. Coal mining began in December 2015, and the mining 225 direction is from southeast to northwest (Fig 4(a)). The mine face has a length of 962 m, a width of 230m, and 226 a depth of approximately 521 m. The overlying bedrock is mainly composed of detrital sedimentary rocks with 227 layered structure, the mechanical strength of rock is low, and the stability is poor. Therefore, coal mining 228 activities can easily result in the collapse of mined voids and then large subsidence. 229

230 We used the ascending ALOS-2 pair of 25 December 2015 and 4 March 2016, path 140, frame 790, both 231 acquired in the sm2 operation mode. The perpendicular baseline is 44 m. Two GPS stations were located along 232 the mining direction to monitor surface displacements. During the period from 25 December 2015 to 4 March 2016, the northing, easting and vertical displacements measured by GPS were -0.0279 m, 0.0178 m and -0.0150 233 m at Station #1 and -0.2029 m, 0.3399 m and -0.9941m at Station #2. The LOS displacements converted from 234 235 the three dimensional displacements at Stations #1 and #2 are -0.0190 m and -1.0115 m, respectively. The large 236 displacement at GPS Station #2 makes it difficult to monitor the displacements with the conventional InSAR 237 method.



Fig. 4 Case Study 2: (a) The mine face and GPS stations overlaid on SRTM DEM. Note that (i) the mine face is indicated by the red solid rectangle; (ii) the mining direction is implied by the red arrow; and (iii) the blue dashed box represents the coverage of ALOS-2 images. (b) Location of the study area in a China map; (c) A photo showing the overall mine face; (d) A photo of GPS Station #1.



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Fig. 5 Case Study 2: (a) ALOS-2 coherence map; (b) ALOS-2 wrapped interferogram (unit: radians)

Fig. 5 shows the ALOS-2 coherence map as well as the wrapped interferogram. It is clear in Fig 5(a)-(b) that coherence is generally high except for the deforming area with dense fringes (e.g. GPS Stations #2 and its surrounding area), which makes phase unwrapping a big challenge for conventional InSAR.

250 As mentioned in the simulated analysis, we split the range bandwidth using a band pass filter to form the sub-

bands at $\pm B/3$ (B is the range bandwidth) from the radar frequencies with the sub-band bandwidth of B/3. Then the filtered data are processed as seen in the workflow presented in Fig. 1. The results are shown in Fig. 6. The result given by the conventional InSAR is presented together for comparison.





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Fig. 6 LOS surface displacements derived from (a) conventional InSAR, (b) R-SSI, and (c) R-SSIaPU. The white dashed line represents the rough boundries of the deforming area.

258 Conventional InSAR can measure small surface displacements with higher precision than R-SSI, which can be 259 evidenced by the smoother signals in the far field (i.e. those outside the white ellipse) in Fig 6(a) than those in Fig 6(b). However, due to the incorrect unwrapping in the subsidence centre, its maximum displacement is only 260 about -0.133 m, which deviated significantly from the magnitude of the surface displacements measured by 261 GPS. The R-SSI method measures a larger displacement, -1.3749 m, in the subsidence centre. The R-SSIaPU 262 263 method (Fig. 6(c)) integrates the advantages of the two methods above, suggesting a similar displacement shape to conventional InSAR and gives the max displacement of -1.3624 m, which is approximately equal to that of 264 the R-SSI method. 265

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Table 3. The maximum LOS displacements, residuals and RMS given by conventional InSAR, the R-SSI method and the R-SSIaPU method.

Mathada	Max LOS	Difference (r	with GPS n)	Displacement RMS in			
Methods	(m)	Station 1 (-0.0190 ^(a))	Station 2 (-1.0115 ^(a))	(m)			
InSAR	-0.133	0.019	-0.979	0.002			
R-SSI	-1.375	0.047	0.073	0.036			
R-SSIaPU	-1.362	0.039	0.042	0.006			



(a) The surface displacements measured by GPS

Table 3 lists the residual displacements of three methods at GPS Stations #1 and #2. At GPS Station #1 which 271 272 has a small displacement, conventional InSAR gives the minimum residual due to its high precision. The R-SSI method gives a maximum residual due to its large wavelength and interferometric phase noise which is 273 approximately $\sqrt{2}$ times that of InSAR. The R-SSIaPU method improves the results of the R-SSI method and 274 275 gives smaller residual. At GPS Station #2 which has a large displacement, conventional InSAR gives the 276 maximum residual due to the error in phase unwrapping. The R-SSI method gives the smaller residual and the R-SSIaPU gives the minimum residual. In order to measure the precision of the three methods, the non-277 278 deforming area, whose displacements given by InSAR are smaller than 0.02 m, are separated. Assuming a zero 279 displacement in the non-deforming area, we can compute the RMS of the non-deforming area for each method. The InSAR method gives the minimum RMS and the R-SSIaPU method improved R-SSI RMS from 0.036 m
to 0.006 m. The real data analysis fully proves that the R-SSIaPU method has a higher accuracy than the R-SSI
method.

283 **5 Discussion and conclusions**

284 Large gradient displacements of the Earth's surface caused by natural hazards and utilization of natural resources have been observed in many places. Examples include the following: earthquakes (e.g. Pathier et al., 285 2006); landslides (e.g. Singleton et al., 2014), volcanos (e.g. Yun et al., 2007), exploitation of groundwater (e.g., 286 Chen et al., 2016; Liu et al., 2016), and coals (e.g. Yan et al., 2016; Yang et al., 2017). All of these can cause 287 288 damages to buildings or infrastructure, and loss of life and injury to citizens. Hence it is crucial to detect and monitor large gradient displacements. The R-SSIaPU method has been presented in this paper by integrating 289 290 Range Split Spectrum Interferometry and conventional InSAR to monitor large gradient surface displacements with high precision. The proposed method unwraps the InSAR residual phase after a complex and large gradient 291 292 displacement phase (initial unwrapped phase) is subtracted from a low-precision displacement map derived 293 from the Range Split Spectrum Interferometry method. Then the final displacement map is generated by converting the total unwrapped phase (residual unwrapped phase + initial unwrapped phase) to LOS surface 294 displacements with the original radar wavelength. The proposed R-SSIaPU method has been applied to 295 investigate the surface displacements caused by mining activities in Tangjiahui, and a good agreement is 296 297 observed with GPS measurements. It is also found from the simulated test that the total range bandwidth and 298 the original radar wavelength are the two controlling factors of the performance of the R-SSIaPU method. The greater the range bandwidth and the radar wavelength, the better the R-SSIaPU method performs. 299

300 The R-SSIaPU method is easy to implement using conventional InSAR software, and can be applicable to areas 301 with few characteristic objects where SAR pixel offset may fail, for example the Tangjiahui mine presented in the real data analysis. The R-SSIaPU method has inherent advantages over the SAR pixel offset based phase 302 303 unwrapping as demonstrated in Yun et al (2007): (i) R-SSI is less sensitive to the pixel size of the SAR images 304 than SAR pixel offset, and (ii) the former is much faster in terms of computational efficiency. However, it should be noted that the performance of the R-SSIaPU method is also dependent upon the coherence of the SAR images, 305 306 which limits its application to a densely vegetated region where rapid decorrelation happens between SAR 307 acquisitions. Nevertheless, the results showed that the R-SSIaPU method makes phase unwrapping less 308 challenge, especially in the cases with large surface displacements.

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