Euclidean Calculation of Feature Points of a Rotating Satellite: A Daisy-Chaining Approach

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The occlusion of feature points and/or feature points leaving the field of view of a camera is a significant practical problem that can lead to degraded performance or instability of visual servo control and vision-based estimation algorithms. By assuming that one known Euclidean distance between two feature points in an initial view is available, homography relationships and image geometry are used in this paper to determine the Euclidean coordinates of feature points in the field of view. A new daisy-chaining method is then used to relate the position and orientation of a plane defined by the feature points to other feature-point planes that are rigidly connected. Through these relationships, the Euclidean coordinates of the original feature points can be tracked even as they leave the field of view. This objective is motivated by the desire to track the Euclidean coordinates of feature points on one face of a satellite as it continually rotates and feature points become self-occluded. A numerical simulation is included to demonstrate that the Euclidean coordinates can be tracked even when they leave the field of view. However, the results indicate the need for a method to reconcile any accumulated error when the feature points return to the field of view.

Nomenclature

A	=	intrinsic camera-calibration matrix
d_j^*	=	distance to π_j^* plane along n_j^*
$\mathcal{F}_j, \mathcal{F}_j^*$	=	frames attached to the π_j and π_j^* planes
G_j	=	projective homography matrix of the jth frame
H_j	=	Euclidean homography matrix of the jth frame
$\mathcal{I}$	=	fixed coordinate frame attached to the camera
m_{ji}, m_{ji}^*	=	normalized Euclidean coordinate of the ith feature point of the π_j and π_j^* planes expressed in $\mathcal{I}$
$\bar{m}_{ji}, \bar{m}_{ji}^*$	=	Euclidean coordinate of the ith feature point of the π_j and π_j^* planes expressed in $\mathcal{I}$
n_j^*	=	unit normal vector to the π_j^* plane expressed in $\mathcal{I}$
p_{ji}, p_{ji}^*	=	image-space pixel coordinates for the ith feature point of the π_j and π_j^* planes
R_j, R_j^*	=	rotation from the π_j and π_j^* planes to $\mathcal{I}$
$R_{\mathcal{F}i}^{\mathcal{F}j}$	=	rotation from frame i to frame j
SO(3)	=	set containing all 3 by 3 orthogonal matrices.
s_{ji}	=	coordinates of the ith feature point of the π_j plane expressed in $\mathcal{F}_j^*$
x_{fj}, x_{fj}^*	=	vector to the origin of $\mathcal{F}_j$ and $\mathcal{F}_j^*$ expressed in $\mathcal{I}$
$x_{ij}^{\mathcal{F}k}$	=	vector from the origin of frame i to the origin of frame j, expressed in frame k
α_{ji}	=	depth ratio of the ith feature point of the π_j plane
π_j	=	jth plane after it rotates
π_j^*	=	jth plane when it first comes into the field of view

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I. Introduction

VISION-BASED technologies commonly exploit image processing methods to identify feature points (e.g., corners or centroids) on a target of interest. These feature points are then used to determine the motion of the camera or target for image-based estimation and control methods. If the feature points leave the field of view (FOV) or become occluded, then degraded performance or instability of visual servo control and vision-based estimation algorithms can occur. The fundamental challenge and potential pervasive impact of developing methods to keep the feature points in the FOV has inspired a variety of research efforts. For example, the results in [1,2] exploit partitioned or switching visual servoing methods to keep the object in the FOV. In [3–8], potential fields or navigation functions are used to ensure the visibility of the feature points during closed-loop control. Zoom control is used in [9] to adjust the focal length of the camera to keep all features in the FOV during the control task. Some researchers have also investigated methods to enlarge the FOV. For example, image mosaicing is used in [10–13] to capture multiple images that are stitched together to obtain a larger image, and in [14], multiple images are fused from multiple cameras.

In addition to research focused on keeping the feature points in the FOV, other research has focused on methods that are invariant to occlusion or feature points leaving the FOV. For example, a linear probabilistic recursive estimation method is described in [15] for reconstructing three-dimensional structure and motion from an integrated sequences of images. In [16], a smooth task function with weighted features that allows visibility changes in the image features during the control task is developed. A variety of feature-point-tracking algorithms have also been proposed that can predict feature-point locations (at least for short-time partial occlusions) based on shape information such as a CAD model and/or the time history of the object (i.e., the object dynamics). Some examples of these approaches are provided in [17–22].

An image-based estimation strategy is developed in this paper that uses the preliminary efforts in [23] to determine the Euclidean feature-point coordinates of features on a satellite by using multiple images from a single camera based on knowledge of one geometric length between two feature points. The motivation for this research arises from the need for image-based state estimation and tracking of a satellite, for which multiple feature points may become self-occluded or leave the FOV; however, the development is generic to any rigid body. Image geometry and homography relationships are combined with a new daisy-chaining method [24,25] to achieve the

results. Specifically, image geometry and homography relationships are used to determine the Euclidean coordinates of nonoccluded feature points in the camera FOV, and the daisy-chaining method is used to link the successive images of the rigid body as feature points (i.e., different surfaces of the spinning satellite) come into and leave the FOV. A numeric simulation is included to demonstrate the developed algorithm.

The contribution of the developed method is the ability to estimate the Euclidean coordinates of the feature points even if the feature points (permanently) leave the FOV or become occluded. The developed estimation method is in contrast to previously described visual servo control methods that require camera actuation by switching, potential fields or navigation functions, or focal length adjustment/zoom control to force the feature points to remain in the FOV. Hence, the developed estimation method could be used to augment those methods. Another contribution of this work is that limited geometric knowledge of the object is required, in contrast to methods that exploit a CAD model or a dynamic model of the object.

II. Geometric Model

Consider a single camera observing the motion of a satellite that is initially identified by four coplanar and noncollinear feature points. Image processing techniques can often be used to select coplanar and noncollinear feature points within an image. However, if four coplanar target points are not available, then the subsequent development can also exploit the virtual parallax method [26], in which the noncoplanar points are projected onto a virtual plane.

To facilitate the ability to track the motion of the satellite, several coordinate systems are defined. As depicted in Fig. 1, the frame $\mathcal{I}$ is attached to the camera. Reference frames are denoted by $\mathcal{F}_j^*$ ($j = 1, 2, \ldots, \infty$), which are associated with the planes π_j^* that are attached to the different faces of the satellite. The frames are numbered in ascending order based on the order that they enter the FOV. The feature points have coordinates $s_{ji} \in \mathbb{R}^3$ ($i = 1, 2, 3, 4$) in the $\mathcal{F}_j^*$ coordinate frame. The vector from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_j^*$ is $x_{fj}^* \in \mathbb{R}^3$, where x_{fj}^* is measured in the $\mathcal{I}$ coordinate frame, and the rotation from $\mathcal{F}_j^*$ to $\mathcal{I}$ is $R_j^* \in \mathrm{SO}(3)$. The geometry between the coordinate frames can be used to determine the initial Euclidean positions of the jth frame's feature points:

$$\bar{m}_{ji}^* = x_{fj}^* + R_j^* s_{ji} \tag{1}$$

where $\bar{m}_{ji}^* \in \mathbb{R}^3$ denotes the Euclidean coordinates of the feature points on the plane π_j^* expressed in $\mathcal{I}$:

$$\bar{m}_{ji}^* \triangleq [x_{ji}^* \quad y_{ji}^* \quad z_{ji}^*]^T \tag{2}$$

The planes and coordinate frames that include an asterisk in the notation denote static instances of a moving plane or coordinate frame. Specifically, the asterisk is used to denote the static instant in time that the feature points that define a plane are first visible. As the plane or coordinate frame moves, the asterisk is dropped, to denote the moving plane/frame. For example, as π_j^* moves from its reference position when the feature points that define the plane are first visible, it is denoted by $\pi_j(t)$ and the frame attached to $\pi_j(t)$ is defined as $\mathcal{F}_j(t)$. The vector from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_j(t)$ and its rotation from $\mathcal{F}_j(t)$ to $\mathcal{I}$ are denoted by $x_{fj}(t) \in \mathbb{R}^3$ and $R_j(t) \in \mathrm{SO}(3)$, respectively. The Euclidean coordinates of the jth frame's feature points after any rotation can be defined as

$$\bar{m}_{ji} = x_{fj} + R_j s_{ji} \tag{3}$$

where $\bar{m}_{ji}(t) \in \mathbb{R}^3$ denotes the Euclidean coordinates of the feature points of π_j expressed in $\mathcal{I}$:

$$\bar{m}_{ji} \triangleq [x_{ji} \quad y_{ji} \quad z_{ji}]^T \tag{4}$$

After some algebraic manipulation of Eqs. (1) and (3), the expression for $\bar{m}_{ji}$ in Eq. (3) can be rewritten as
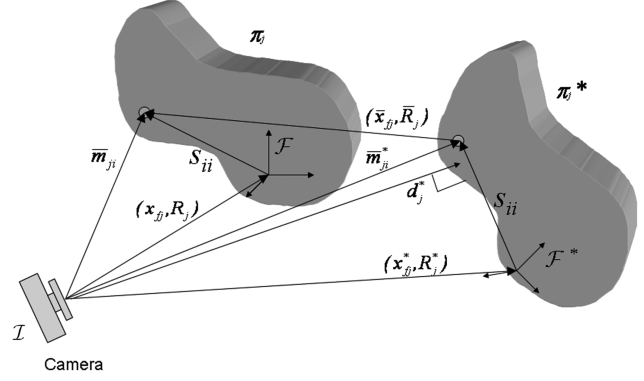

Fig. 1 Relationship between a coordinate frame in its initial position and all subsequent positions.

$$\bar{m}_{ji} = \bar{x}_{fj} + \bar{R}_j \bar{m}_{ji}^* \tag{5}$$

where $\bar{R}_j(t) \in \mathrm{SO}(3)$ and $\bar{x}_{fj}(t) \in \mathbb{R}^3$ are new rotation and translation variables, respectively, defined as

$$\bar{R}_j = R_j R_j^{*T} \tag{6}$$

$$\bar{x}_{fj} = x_{fj} - \bar{R}_j x_{fj}^* \tag{7}$$

By using the projective relationship depicted in Fig. 1,

$$d_j^* = n_j^{*T} \bar{m}_{ji}^* \tag{8}$$

the expression in Eq. (5) can be expressed as

$$\bar{m}_{ji} = \left(\bar{R}_j + \frac{\bar{x}_{fj}}{d_j^*} n_j^{*T} \right) \bar{m}_{ji}^* \tag{9}$$

In Eq. (9), $n_j^* \in \mathbb{R}^3$ denotes the constant unit normal to the plane π_j^* expressed in $\mathcal{I}$, and $d_j^* > 0 \in \mathbb{R}$ is the distance to the plane along n_j^*.

III. Euclidean Reconstruction

A. Homography Decomposition

The relationship in Eq. (9) provides a means to quantify the translation and rotation between a coordinate system's location at two points in time and space. Because the position and orientation (i.e., pose) of $\mathcal{F}_j$ and $\mathcal{F}_j^*$ cannot be directly measured, a Euclidean reconstruction is developed in this section to obtain the position and rotation information by comparing multiple images acquired from the camera. Specifically, comparisons are made between $m_{ji}(t)$ and m_{ji}^* in terms of $\mathcal{I}$. To facilitate the subsequent development, the normalized Euclidean coordinates of the feature points for $\mathcal{F}_j$ and $\mathcal{F}_j^*$ can be expressed in terms of $\mathcal{I}$ as $m_{ji}(t)$ and $m_{ji}^* \in \mathbb{R}^3$, respectively:

$$m_{ji} \triangleq \frac{\bar{m}_{ji}}{z_{ji}} \qquad m_{ji}^* \triangleq \frac{\bar{m}_{ji}^*}{z_{ji}^*} \tag{10}$$

From Eqs. (9) and (10), the rotation and translation between the coordinate systems $\mathcal{F}_j$ and $\mathcal{F}_j^*$ can be related in terms of the normalized Euclidean coordinates:

$$m_{ji} = \underbrace{\frac{z_{ji}^*}{z_{ji}}}_{\alpha_{ji}} \underbrace{\left(\bar{R}_j + \frac{\bar{x}_{fj}}{d_j^*} n_j^{*T} \right)}_{H_j} m_{ji}^* \tag{11}$$

In Eq. (11), $\alpha_{ji}(t) \in \mathbb{R}$ denotes depth ratios, and $H_j(t) \in \mathbb{R}^{3 \times 3}$ denotes Euclidean homographies [27]. Each Euclidean feature point has a projected pixel coordinate expressed as

$$p_{ji} \triangleq [u_{ji} \quad v_{ji} \quad 1]^T \qquad p_{ji}^* \triangleq [u_{ji}^* \quad v_{ji}^* \quad 1]^T \tag{12}$$

where $p_{ji}(t)$ represents the image-space coordinates of the time-varying feature points of $\mathcal{F}_j$, and $p_{ji}^* \in \mathbb{R}^3$ represents the image-space coordinates of the feature points of $\mathcal{F}_j^*$. To calculate the Euclidean homography given in Eq. (11) from pixel information, the projected pixel coordinates are related to $m_{ji}(t)$ and m_{ji}^* by the pinhole-camera model:

$$p_{ji} = A m_{ji} \qquad p_{ji}^* = A m_{ji}^* \tag{13}$$

where $A \in \mathbb{R}^{3 \times 3}$ is a known, constant, invertible, intrinsic camera-calibration matrix. By using Eqs. (11) and (13), the following relationship can be developed:

$$p_{ji} = \alpha_{ji} \underbrace{(A H_j A^{-1})}_{G_j} p_{ji}^* \tag{14}$$

where $G_j(t) \in \mathbb{R}^{3 \times 3}$ denotes a projective homography. From four points, sets of linear equations can be developed from Eq. (14) to determine the projective homographies up to a scalar multiple. Techniques described in [7,28] can be used to decompose the Euclidean homographies to obtain $\alpha_{ji}(t)$, $\bar{x}_{fj}(t)/d_j^*$, $\bar{R}_j(t)$, and n_j^{*T} for $i = 1, 2, 3, 4$ and $j = 1, 2, \ldots, \infty$.

B. Euclidean Reconstruction of the π_1^* Plane

Because of the fact that a distance is assumed to be known on the plane π_1^*, its Euclidean reconstruction is analyzed separately from the other planes. For the Euclidean reconstruction of subsequent planes that do not have an assumed known length, development is presented in Sec. III.C. To solve for the Euclidean coordinates $\bar{m}_{11}^*$ and $\bar{m}_{12}^*$, a new plane $\pi_1^{*'}$ is created parallel to π_1^* containing the point m_{11}^*. This new plane will intersect a line l_1^*, which goes from the origin of $\mathcal{I}$ through m_{12}^* and $\bar{m}_{12}^*$. The plane $\pi_1^{*'}$ intersects l_1^* at a point $m_{12}^{*'} \in \mathbb{R}^3$. As depicted in Fig. 2, the distance between m_{11}^* and $m_{12}^{*'}$ is defined as $\sigma_1 \in \mathbb{R}$. The line l_1^* and the plane $\pi_1^{*'}$ are defined by the sets of all points ξ_1 and $\xi_2 \in \mathbb{R}^3$ that satisfy the implicit functions

$$\pi_1^{*'} = \{\xi_1 | -n_1^* \cdot (\xi_1 - m_{11}^*) = 0\} \tag{15}$$

$$l_1^* = \{\xi_2 | \xi_2 - u m_{12}^* = 0\} \tag{16}$$

where $u \in \mathbb{R}$ is some positive constant. The geometric relationships in Eqs. (15) and (16) indicate that any vector from one of the points ξ_1 on $\pi_1^{*'}$ to m_{11}^* is normal to $-n_1^*$, and that l_1^* is the set of points ξ_2 that are linearly proportional to m_{12}^* by some scalar $u \in \mathbb{R}$. From Eqs. (15) and (16), the point at which the l_1^* and $\pi_1^{*'}$ intersect (i.e., when $\xi_1 = \xi_2 = m_{12}^{*'}$) can be determined by solving Eq. (16) for ξ_2, substituting ξ_2 into Eq. (15) for ξ_1, solving the resulting expression for u, and then substituting the expression for u into Eq. (16):
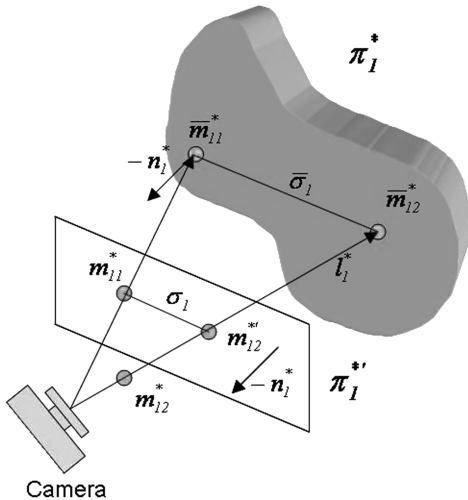

Fig. 2   Geometry used to extract the Euclidean position and orientation of feature points on a plane using a known distance.

$$m_{12}^{*'} = \frac{-n_1^* \cdot m_{11}^*}{-n_1^* \cdot m_{12}^*} m_{12}^* \tag{17}$$

The result in Eq. (17) can be used to solve for σ_1:

$$\sigma_1 = \|m_{12}^{*'} - m_{11}^*\| \tag{18}$$

Because $\bar{\sigma}_1 \in \mathbb{R}$ is assumed to be a known Euclidean distance between $\bar{m}_{11}^*$ and $\bar{m}_{12}^*$ and σ_1, $\|m_{11}^*\|$ and $\|m_{12}^*\|$ can be determined as previously described, the similar triangle relationships derived from Fig. 2:

$$\frac{\sigma_1}{\bar{\sigma}_1} = \frac{\|m_{11}^*\|}{\|\bar{m}_{11}^*\|} = \frac{\|m_{12}^{*'}\|}{\|\bar{m}_{12}^*\|} \tag{19}$$

can be used to recover $\bar{m}_{11}^*$ and $\bar{m}_{12}^*$:

$$\bar{m}_{11}^* = \frac{\|\bar{m}_{11}^*\|}{\|m_{11}^*\|} m_{11}^* \qquad \bar{m}_{12}^* = \frac{\|\bar{m}_{12}^*\|}{\|m_{12}^{*'}\|} m_{12}^{*'} \tag{20}$$

By using Eq. (20), the unknown constant scalar d_1^* defined in Eq. (8) can be determined. Because d_1^* is now known and m_{1i}^* is measurable, Eqs. (8) and (10) can be used to determine z_{1i}^*:

$$z_{1i}^* = \frac{d_1^*}{n_1^{*T} m_{1i}^*} \tag{21}$$

The Euclidean coordinates of the feature points on π_1^* expressed in $\mathcal{I}$ can now be reconstructed by substituting Eq. (21) into Eq. (10):

$$\bar{m}_{1i}^* = \frac{d_1^*}{n_1^{*T} m_{1i}^*} m_{1i}^* \tag{22}$$

To facilitate the subsequent daisy-chaining method, the translation from $\mathcal{I}$ to $\mathcal{F}_1^*$ and the orientation of $\mathcal{F}_1^*$ with respect to $\mathcal{I}$ can also be determined. Without loss of generality, the origin of $\mathcal{F}_1^*$ is assumed to be $\bar{m}_{11}^*$. The orientation of $\mathcal{F}_1^*$ with respect to $\mathcal{I}$ introduced in Eq. (1) can be expressed as

$$R_1^* = [i_{x1} \quad i_{y1} \quad i_{z1}] \tag{23}$$

In Eq. (23), $i_{x1} \in \mathbb{R}^3$ and $i_{z1} \in \mathbb{R}^3$ are defined as

$$i_{x1} = \frac{\bar{m}_{12}^* - \bar{m}_{11}^*}{\bar{\sigma}_1} \tag{24}$$

$$i_{z1} = -n_1^* \tag{25}$$

and $i_{y1} \in \mathbb{R}^3$ is defined as the cross product of i_{x1} and i_{z1}:

$$i_{y1} = -n_1^* \times \frac{\bar{m}_{12}^* - \bar{m}_{11}^*}{\bar{\sigma}_1} \tag{26}$$

In Eqs. (25) and (26), the normal vector n_1^* is known from the homography decomposition of Eqs. (11) and (14). Because i_{z1} is known from the homography decomposition of Eqs. (11) and (14), the results in Eq. (20) can be substituted into Eqs. (24) and (26) to determine i_{x1} and i_{y1}. Based on Eq. (23), the rotation R_1^* can now be determined. Based on the fact that R_1^* can be determined and $\bar{R}_1(t)$ is known from the homography decomposition of Eqs. (11) and (14), $R_1(t)$ can now be determined from Eq. (6). Because the origin of $\mathcal{F}_1^*$ is selected as $\bar{m}_{11}^*$, the translation from $\mathcal{I}$ to $\mathcal{F}_1^*$ introduced in Eq. (1) as x_{f1}^* is equal to $\bar{m}_{11}^*$, by definition. Given that d_1^*, $\bar{R}_1(t)$, $\bar{x}_{f1}(t)/d_1^*$, and x_{f1}^* have been determined, Eq. (7) can be used to solve for $x_{f1}(t)$.

C. Euclidean Reconstruction of the π_j^* Plane

To exploit the daisy-chaining strategy to link the pose of $\mathcal{F}_1$ with the pose of the subsequent frames $\mathcal{F}_j$ ($j = 2, 3, \ldots, \infty$), the pose of $\mathcal{F}_j$ also needs to be determined. However, a known geometric length is not available on π_j, and so a method different from that in Sec. III.B must be developed. Specifically, in lieu of a known geometric length between feature points, the development in this section uses the

previous reconstructed information to determine a geometric distance to the object that can be used to further support the Euclidean reconstruction of the subsequent feature points. Specifically, under the assumption that at some instant in time the π_{j-1} plane and π_j plane are both visible, the pose of $\mathcal{F}_{j-1}$ can be used to solve for the pose of $\mathcal{F}_j^*$, provided that the planes undergo some motion while they are both in the FOV. Let $t^- \in \mathbb{R}$ denote some instant in time when the two adjacent feature-point planes are both visible, and let $t^+ \in \mathbb{R}$ denote some time after some incremental motion has occurred. Because $\mathcal{F}_{j-1}$ and $\mathcal{F}_j$ are part of the same rigid body, the rotation and translations for each of the planes are equal. Therefore, the known rotation

$$R_{j-1}(t^+)R_{j-1}^T(t^-)$$

is equal to $\bar{R}_j(t^+)$. Similarly, the known translation

$$\bar{x}_{f(j-1)}(t^+) - \bar{x}_{f(j-1)}(t^-)$$

is equal to $\bar{x}_{fj}(t^+)$. The facts that $\bar{x}_{fj}(t^+)$ is known and the homography decomposition in Eq. (11) yields $\bar{x}_{fj}(t^+)/d_j^*$ can be used to determine d_j^*, which is the magnitude of the vector $\lambda_j \in \mathbb{R}^3$ that is defined from the origin of $\mathcal{I}$ to the plane π_j^* along the normal n_j^* (see Fig. 3).

Without loss of generality, the origin of the $\mathcal{F}_j^*$ frame is assigned to be $\bar{m}_{j1}^*$. As indicated in Fig. 3, the angle between $\bar{m}_{ji}^*$ and λ_j is defined to be $\theta_{ji} \in \mathbb{S}_1$ ($i = 1, 2, 3, 4$), which can be calculated using the definition of the dot product,

$$\theta_{ji} = \cos^{-1}\left(\frac{m_{ji}^* \cdot n_j^*}{\|m_{ji}^*\|\|n_j^*\|}\right) \quad (27)$$

and hence the magnitude of $\bar{m}_{ji}^*$ can be determined as

$$\|\bar{m}_{ji}^*\| = \frac{d_j^*}{\cos\theta_{ji}} \quad (28)$$

Based on Eq. (28), $\bar{m}_{ji}^*$ can now be calculated as

$$\bar{m}_{ji}^* = \frac{\|\bar{m}_{ji}^*\|}{\|m_{ji}^*\|}m_{ji}^* \quad (29)$$

To facilitate the subsequent daisy-chaining method, the translation from $\mathcal{I}$ to $\mathcal{F}_j^*$ and the orientation of $\mathcal{F}_j^*$ with respect to $\mathcal{I}$ must be determined. As the satellite rotates, the π_1 plane will leave the FOV and a new plane will become visible. The orientation of F_j^* with respect to $\mathcal{I}$ introduced in Eq. (3) can be expressed as

$$R_j^* = [i_{xj} \quad i_{yj} \quad i_{zj}] \quad (30)$$

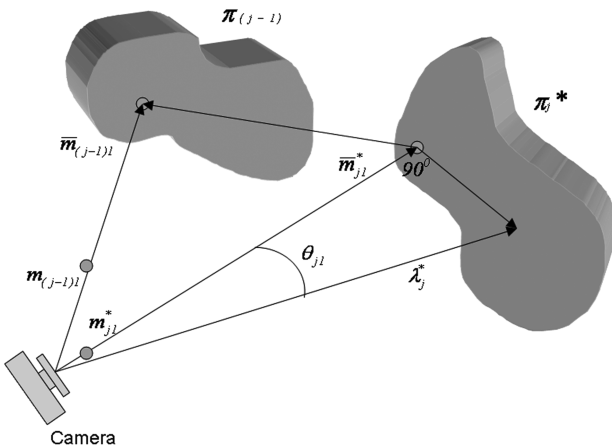In Eq. (30), $i_{xj} \in \mathbb{R}^3$ and $i_{zj} \in \mathbb{R}^3$ are defined as

Fig. 3 Geometry used to extract the Euclidean position and orientation of a plane using a known plane.

$$i_{xj} = \frac{\bar{m}_{j2}^* - \bar{m}_{j1}^*}{\|\bar{m}_{j2}^* - \bar{m}_{j1}^*\|} \quad (31)$$

$$i_{zj} = -n_j^* \quad (32)$$

and $i_{yj} \in \mathbb{R}^3$ is defined as the cross product of i_{xj} and i_{zj}:

$$i_{yj} = -n_j^* \times \frac{\bar{m}_{j2}^* - \bar{m}_{j1}^*}{\|\bar{m}_{j2}^* - \bar{m}_{j1}^*\|} \quad (33)$$

In Eqs. (32) and (33), the normal vector n_j^* is known from the homography decomposition of Eqs. (11) and (14). Because i_{zj} is known from the homography decomposition, the result in Eq. (29) can be substituted into Eqs. (31) and (33) to determine i_{xj} and i_{yj}. Based on Eq. (30), the rotation R_j^* can now be determined. Based on the fact that R_j^* can be determined and $\bar{R}_j(t)$ is known from the homography decomposition of Eqs. (11) and (14), $R_j(t)$ can be determined. Because the origin of $\mathcal{F}_j^*$ is selected as $\bar{m}_{j1}^*$, the translation from $\mathcal{I}$ to $\mathcal{F}_j^*$, introduced in Eq. (3) as x_{fj}^*, is equal to $\bar{m}_{j1}^*$, by definition. The fact that d_j^*, $\bar{R}_j(t)$, $\bar{x}_{fj}(t)/d_j^*$ and x_{fj}^* have been determined can now be used to solve for $x_{fj}(t)$.

IV. Daisy-Chaining

The previous development can be used to determine the pose of $\mathcal{F}_j$ with respect to $\mathcal{I}$ when the feature points on π_j are visible. The daisy-chaining method presented in this section is used to determine the relative pose between $\mathcal{F}_1$ and $\mathcal{F}_j$ so that the pose of $\mathcal{F}_1$ can still be determined even after the feature points on π_1 leave the FOV, provided that the feature points on π_j are visible.

The relative pose between $\mathcal{F}_{j-1}$ and $\mathcal{F}_j$ will not change, because both time-varying coordinate frames are attached to the same rigid body. Hence, the relative pose between $\mathcal{F}_{j-1}$ and $\mathcal{F}_j$ only needs to be determined once. As in the previous sections, the subsequent development is based on the assumption that the feature points on both π_{j-1} and π_j are visible at some moment in time. The first instant when the feature points on both π_{j-1} and π_j are visible is when π_j first enters the FOV, which is denoted as π_j^*. At this instant in time, the pose of $\mathcal{F}_j$ is denoted by $\mathcal{F}_j^*$, with a translation and rotation with respect to $\mathcal{I}$ denoted as x_{fj}^* and R_j^*. At some instant when the feature points on π_1 are visible, a reference image is acquired that contains the geometric length $\bar{\sigma}_1$. Based on the methods in Sec. III.B, the Euclidean coordinates of the feature points on π_1^* can be reconstructed and expressed in $\mathcal{I}$. The subsequent images of the feature points on π_1 can then be used to construct the homography relationship given in Eq. (11), which allows the Euclidean coordinates of feature points on π_1 to continue to be reconstructed. At some other point in time, the feature points on π_1 and π_2^* are both in the FOV, and a second reference image is acquired. Assuming that the next image is acquired when both π_1 and π_2^* have undergone some motion and the feature points on both planes are still visible, the methods in Sec. III.C can be used to reconstruct the Euclidean coordinates of the feature points on π_2^* expressed in $\mathcal{I}$. The homography relationship given in Eq. (11) can then be used to determine the relative pose of $\mathcal{F}_2$ with respect to $\mathcal{F}_2^*$ expressed in $\mathcal{I}$, as well as the pose of $\mathcal{F}_2$ with respect to $\mathcal{I}$ expressed in $\mathcal{I}$. Given the Euclidean coordinates of the feature points on π_1 and π_2^* expressed in $\mathcal{I}$, the constant relative pose of $\mathcal{F}_1$ with respect to $\mathcal{F}_2$ can be determined. That is, the constant vector $x_{21}^{\mathcal{F}_2} \in \mathbb{R}^3$ from the origin of $\mathcal{F}_2$ to the origin of $\mathcal{F}_1$ expressed in $\mathcal{F}_2$ is determined when $\bar{\mathcal{F}}_2$ and $\mathcal{F}_2^*$ are coincident:

$$x_{21}^{\mathcal{F}_2} = R_2^{*T}(x_{f1} - x_{f2}^*) \quad (34)$$

In Eq. (34), R_2^{*T} is used to express the difference $x_{f1} - x_{f2}^*$ in $\mathcal{F}_2$. The vector $x_{21}^{\mathcal{F}_2}$ is constant in $\mathcal{F}_2$, but is time-varying when expressed in $\mathcal{I}$. The constant rotation $R_{\mathcal{F}1}^{\mathcal{F}2} \in SO(3)$ from $\mathcal{F}_1$ to $\mathcal{F}_2$ is determined when $\mathcal{F}_2$ and $\mathcal{F}_2^*$ are coincident:

$$R_{\mathcal{F}1}^{\mathcal{F}2} = R_2^{*T} R_1 \qquad (35)$$

As the satellite continues to rotate, the feature points in π_1 will leave the FOV, and the feature points on π_2 and π_3^* will eventually be in the FOV at the same time. A third reference image is now acquired. To estimate the pose of $\mathcal{F}_1$ and the Euclidean feature points of π_1, the vector x_{f1} from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_1$, as well as the R_1 rotation from $\mathcal{F}_1$ to $\mathcal{I}$, are required. As stated earlier, the pose of $\mathcal{F}_2$ with respect to $\mathcal{I}$ expressed in $\mathcal{I}$ has been determined, and so the vector from the origin of $\mathcal{F}_2$ to the origin of $\mathcal{F}_1$ can be expressed in $\mathcal{I}$ as

$$x_{21}^{\mathcal{I}} = R_2 x_{21}^{\mathcal{F}2} \qquad (36)$$

even though π_1 is no longer in the FOV. The vector from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_1$ is equivalent to the vector from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_2$ plus the vector from the origin of $\mathcal{F}_2$ to the origin of $\mathcal{F}_1$. Both of these vectors are known, and so the vector from the origin of $\mathcal{I}$ to the origin of $\mathcal{F}_1$ can be determined as

$$x_{f1} = x_{f2} + x_{21}^{\mathcal{I}} \qquad (37)$$

The rotation from $\mathcal{F}_1$ to $\mathcal{I}$ is equivalent to the rotation from $\mathcal{F}_2$ to $\mathcal{I}$ multiplied by the rotation from $\mathcal{F}_1$ to $\mathcal{F}_2$. Both of these rotations are known, and so the rotation from $\mathcal{F}_1$ to $\mathcal{I}$ can be determined as

$$R_1 = R_2 R_{\mathcal{F}1}^{\mathcal{F}2}$$

Assuming that the next image is acquired when both π_2 and π_3^* have undergone some motion and the feature points on both planes are still visible, then the methods in Sec. III.C can be used to reconstruct the Euclidean coordinates of the feature points on π_3^* expressed in $\mathcal{I}$. The homography relationship given in Eq. (11) can then be used to determine the relative pose of $\mathcal{F}_3$ with respect to $\mathcal{F}_3^*$ expressed in $\mathcal{I}$, as well as the pose of $\mathcal{F}_3$ with respect to $\mathcal{I}$ expressed in $\mathcal{I}$. Given the Euclidean coordinates of the feature points on π_2 and π_3^* expressed in $\mathcal{I}$, the constant relative pose of $\mathcal{F}_2$ with respect to $\mathcal{F}_3$ can be determined; that is, the constant vector $x_{32}^{\mathcal{F}3} \in \mathbb{R}^3$ from the origin of $\mathcal{F}_3$ to the origin of $\mathcal{F}_2$ expressed in $\mathcal{F}_3$ is determined when $\mathcal{F}_3$ and $\mathcal{F}_3^*$ are coincident:

$$x_{32}^{\mathcal{F}3} = R_3^{*T}(x_{f2} - x_{f3}^*) \qquad (38)$$

The constant rotation $R_{\mathcal{F}2}^{\mathcal{F}3} \in SO(3)$ from $\mathcal{F}_2$ to $\mathcal{F}_3$ that is determined when $\mathcal{F}_3$ and $\mathcal{F}_3^*$ are coincident is

$$R_{\mathcal{F}2}^{\mathcal{F}3} = R_3^{*T} R_2 \qquad (39)$$

The constant relative pose of $\mathcal{F}_1$ with respect to $\mathcal{F}_3$ can also be determined. The constant vector $x_{31}^{\mathcal{F}3} \in \mathbb{R}^3$ from the origin of $\mathcal{F}_3$ to the origin of $\mathcal{F}_1$ expressed in $\mathcal{F}_3$ is equivalent to the vector from the origin of $\mathcal{F}_3$ to the origin of $\mathcal{F}_2$ plus the vector from the origin of $\mathcal{F}_2$ to the origin of $\mathcal{F}_1$, both expressed in $\mathcal{F}_3$. Both of these vectors are known, and so the vector from the origin of $\mathcal{F}_3$ to the origin of $\mathcal{F}_1$ expressed in $\mathcal{F}_3$ can be determined as

$$x_{31}^{\mathcal{F}3} = x_{32}^{\mathcal{F}3} + x_{21}^{\mathcal{F}3} = R_3^{*T}(x_{f2} - x_{f3}^*) + R_3^{*T} R_2 x_{21}^{\mathcal{F}2} \qquad (40)$$

The constant rotation $R_{\mathcal{F}1}^{\mathcal{F}3} \in SO(3)$ from $\mathcal{F}_1$ to $\mathcal{F}_3$ is equivalent to the rotation from $\mathcal{F}_2$ to $\mathcal{F}_3$ multiplied by the rotation from $\mathcal{F}_1$ to $\mathcal{F}_2$. Both of these rotations are known, and so the rotation from $\mathcal{F}_1$ to $\mathcal{F}_3$, determined when $\mathcal{F}_3$ and $\mathcal{F}_3^*$ are coincident, is

$$R_{\mathcal{F}1}^{\mathcal{F}3} = R_{\mathcal{F}2}^{\mathcal{F}3} R_{\mathcal{F}1}^{\mathcal{F}2} \qquad (41)$$

This procedure can be continued indefinitely to calculate the vector from the origin of $\mathcal{I}$ to the origin of the $\mathcal{F}_1$ frame expressed in $\mathcal{I}$. The general equation for $x_{f1}(t)$ after j rotations is

$$x_{f1} = x_{fj} + R_j x_{j1}^{\mathcal{F}j} \qquad (42)$$

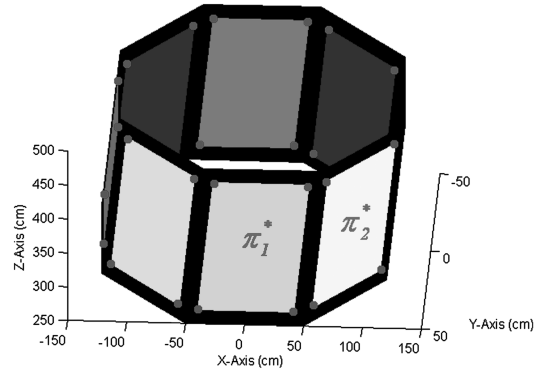Likewise, the general equation for $R_1(t)$ after j rotations is

Fig. 4 Virtual satellite with feature points created in MATLAB.

$$R_1 = R_j R_{\mathcal{F}1}^{\mathcal{F}j} \qquad (43)$$

The Euclidean coordinates of the feature points on π_1 after j rotations can also be determined as

$$\bar{m}_{1i} = x_{fj} + R_j x_{j1}^{\mathcal{F}j} + R_j R_{\mathcal{F}1}^{\mathcal{F}j} s_{1i} \qquad (44)$$

where $x_{j1}^{\mathcal{F}j}(t) \in \mathbb{R}^3$ is the vector from the origin of $\mathcal{F}_j(t)$ to the origin of $\mathcal{F}_1(t)$, and $R_{\mathcal{F}1}^{\mathcal{F}j} \in SO(3)$ is the rotation from $\mathcal{F}_j(t)$ to $\mathcal{F}_1(t)$.

V. Numerical Simulation

A. Simulation Setup

The geometric and daisy-chaining method developed in Sec. IV was implemented in a MATLAB simulation. The uniform octagonal satellite depicted in Fig. 4 was created and rotated 51 times about its axis of symmetry by 0.4363 rad (25 deg). Each of the square sides measures 1 by 1 m. Smaller square sections are centered on each side and the feature points were chosen to be the corners of these sections. The symmetry of the object is coincidental and not required for the feature-point calculations. Also, planar and nonplanar surfaces can exist on the same object, but to form a homography matrix, four feature points on a planar surface or eight nonplanar points are needed. To simplify our analysis, four planar feature points are given without loss of generality. The π_1^* plane rotated a total 30.1069 rad (1275 deg), left and reentered the FOV three times, and formed 29 image chains. The satellite was viewed by a camera with a scaled focal length of 860 pixels, and the pixel coordinates of the principle point were chosen to be [360, 240] pixels. Although the simulation was implemented for a rotating satellite, the developed method can be applied to a general rotating and translating rigid body.

B. Results and Discussion

The Euclidean errors of estimated feature points with no pixel noise and a perfect camera calibration are plotted in Fig. 5 versus the number of daisy chains between images. The errors were calculated by subtracting the estimated Euclidean feature-point location [Eq. (44)] from the actual Euclidean position for each axis. The actual Euclidean position was known for the simulation and was only used to quantify the estimation error. The errors grew as the chain number grew, but were all on the order of 10^{-6} cm, resulting in a near-perfect estimate, and any discrepancies were due to numeric noise. The simulation was also executed assuming a nonperfect camera calibration. Random error was introduced into the calibration in the form of a uniform distribution on the interval $[-5, 5]$ pixels. Motivation for this degree of calibration uncertainty was derived from the fact that typical calibration routines[¶] yield results well below the simulated uncertainty. For this camera-calibration routine, errors in the scaled focal length of ± 1 pixel and errors in the principle point of ± 2 pixels are not uncommon. The Euclidean estimation errors are

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[¶]Data available online at http://www.vision.caltech.edu/bouguetj/calib_-doc/ [retrieved November 2007].
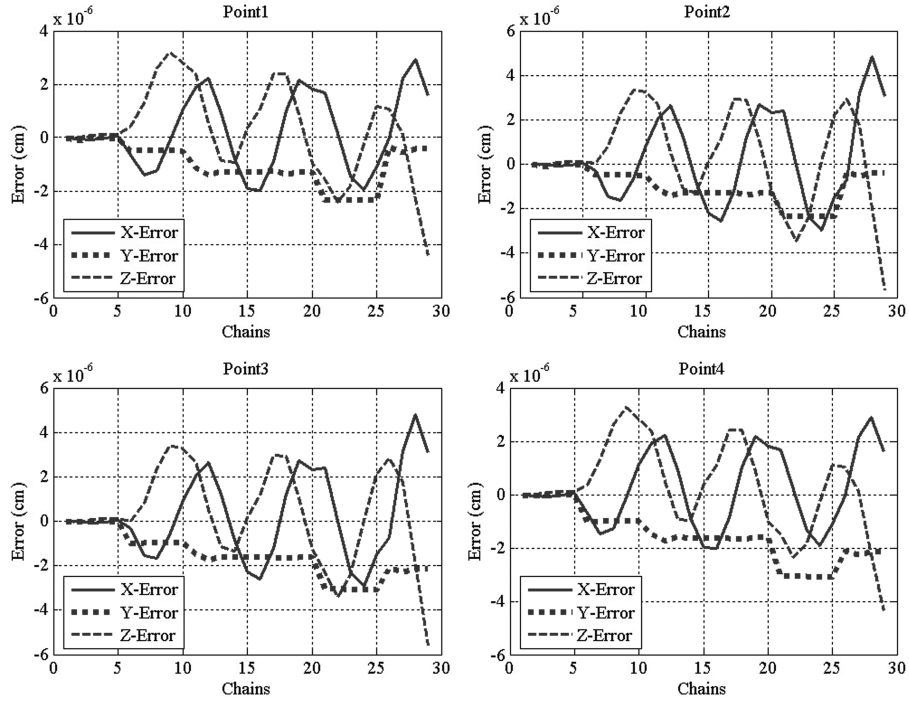
Fig. 5   Errors for each point versus chain number for a perfect camera calibration and no pixel noise.
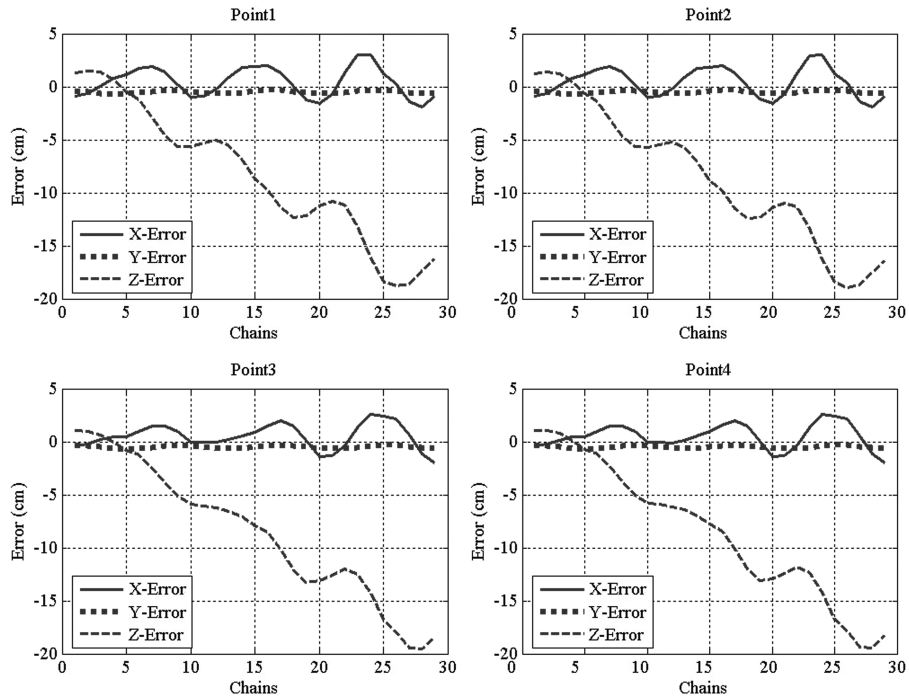

Fig. 6   Errors for each point versus chain number for a nonperfect camera calibration.

plotted versus the chain number in Fig. 6. As in Fig. 5, the errors grew as the chain number increased. This behavior is expected, due to the fact that in any estimation algorithm in which the feature points permanently leave the FOV, the error will continue to propagate. The errors along the Y axis are less than the errors along the other axes, due to the rotation being about the Y axis, which is the axis of symmetry. Future efforts will focus on mitigating the propagation of the estimation error along the X and Z axes. Some possible approaches include resetting the estimate when a previously viewed image returns to the FOV and linear filtering methods. To illustrate the possible utility of this future work, we simulated a simple ad hoc resetting approach for the uncertain camera-calibration case.

Whenever the first frame reenters the FOV, the measured value replaced the estimated value. In this ad hoc demonstration, our knowledge of the exact location of the satellite was used to determine when the satellite reentered the FOV. The Euclidean estimation errors are plotted versus the chain number in Fig. 7. As in Fig. 7 the errors grew as the chain number increased, but due to the estimates being reset (denoted by a circle in Fig. 7), they remain bounded.

VI.   Conclusions

A new daisy-chaining method is combined with new image geometry techniques to track the Euclidean position of the feature
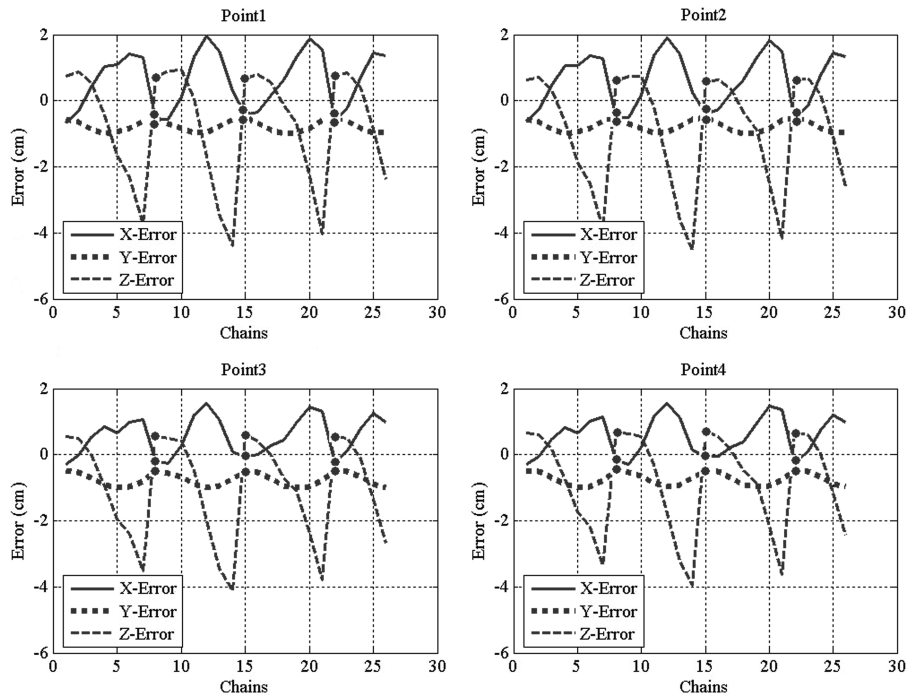
Fig. 7   Errors for each point versus chain number for a nonperfect camera calibration with error resetting.

points of a rotating and translating body despite the potential to leave the field of view or become occluded. These methods allow for relationships between frames to be determined as the rigid body moves. By chaining the developed relationships to the inertial camera frame, the Euclidean position of the feature points can be estimated. This method shows promise, but some limitations are apparent. For example, the numerical simulation demonstrates the effectiveness of the method, but the errors have the potential to accumulate (as in dead-reckoning navigation) if the feature points leave the field of view and never return. The algorithm is also susceptible to errors in the camera-calibration matrix. Future work is required to alleviate these errors.

Acknowledgments

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