DISTRIBUTIONS OF UPPER PAPR AND LOWER PAPR OF OFDM SIGNALS IN VISIBLE LIGHT COMMUNICATIONS

Zhenhua Yu^{*} Robert J. Baxley[†] G. Tong Zhou^{*}

* School of Electrical and Computer Engineering, Georgia Institute of Technology, Atlanta, GA, 30332 USA [†] Georgia Tech Research Institute, Atlanta, GA, 30332 USA

ABSTRACT

Orthogonal frequency-division multiplexing (OFDM) in visible light communications (VLC) inherits the disadvantage of high peak-to-average power ratio (PAPR) from OFDM in radio frequency (RF) communications. The upper peak power and lower peak power of real-valued VLC-OFDM signals are both limited by the dynamic constraints of light emitting diodes (LEDs). The efficiency and transmitted electrical power are directly related with the upper PAPR (UPAPR) and lower PAPR (LPAPR) of VLC-OFDM. In this paper, we will derive the complementary cumulative distribution function (CCDF) of UPAPR and LPAPR, and investigate the joint distribution of UPAPR and LPAPR.

Index Terms— Visible light communications (VLC), orthogonal frequency-division multiplexing (OFDM), peak-toaverage power ratio (PAPR)

1. INTRODUCTION

Motivated by the rapid progress of solid state lighting technology and increasingly saturated radio frequency (RF) spectrum, visible light communication (VLC) has become a promising candidate to complement conventional RF communication [1, 2, 3]. VLC uses the visible light spectrum to provide illumination and communication simultaneously by way of light emitting diodes (LEDs) [4]. In VLC, simple and low-cost intensity modulation and direct detection (IM/DD) techniques are employed, thus only signal intensity information, not phase information, is modulated.

Recently, orthogonal frequency-division multiplexing (OFDM) has been considered for VLC due to its ability to boost data rates and effectively combat inter-symbolinterference (ISI) [5, 6, 7]. OFDM is also known for its disadvantage of high peak-to-average power ratio (PAPR). Power amplifiers in RF communication systems often have to operate with large power back-off and reduces the power efficiency [8]. The distribution of PAPR of complex-valued RF-OFDM baseband signals has been extensively studied in references [9, 10, 11, 12]. VLC-OFDM inherits the high PAPR from RF-OFDM. However, different from RF-OFDM, VLC-OFDM baseband signals must be real-valued required by IM/DD schemes. Thus, the frequency-domain symbols of OFDM must be Hermitian symmetric to make the timedomain samples real-valued. Additional, rather than peak power constrained in RF-OFDM, VLC-OFDM is dynamic range constrained by the turn-on current and maximum permissible alternating current of LEDs [13]. Furthermore, illumination requirements place a constraint on the average amplitude of the VLC-OFDM signal. For the real-valued VLC-OFDM signal, the square of the maximum value can be seen as the upper peak power, and the square of the minimum value can be seen as the lower peak power. Upper peak and lower peak have individual constraints in VLC. It has been studied in references [14, 15] that the efficiency and transmitted electrical power are directly related with the upper PAPR (UPAPR) and lower PAPR (LPAPR) of VLC-OFDM. Although the distribution of PAPR of real-valued OFDM was shown in reference [16, 17], to the best of our knowledge, the distribution of UPAPR and LPAPR are still unknown.

In this paper, we will derive the complementary cumulative distribution function (CCDF) of UPAPR and LPAPR, and the joint distribution of UPAPR and LPAPR, assuming that VLC-OFDM time-domain signals are independent and identically Gaussian distributed for large number of subcarriers. Simulated results are provided to examine our theoretical analysis.

2. REVIEW OF PAPR IN RF-OFDM

In RF-OFDM systems, let $\{X_k\}_{k=0}^{N-1}$ denote the frequencydomain OFDM signal, where k is the subcarrier index and N is the number of subcarriers. The Nyquist-rate sampled timedomain OFDM signal $\{x[n]\}_{n=0}^{N-1}$ is generated by applying inverse discrete Fourier transform (IDFT) to the frequencydomain signal:

$$x[n] = \frac{1}{\sqrt{N}} \sum_{k=0}^{N-1} X_k e^{j2\pi kn/N}, \quad 0 \le k \le N-1, \quad (1)$$

where $j = \sqrt{-1}$ and n is the discrete-time index. It is wellknown that the OFDM time-domain signal has high peak-to-

This research was supported in part by the Texas Instruments Leadership University Program.

average power ratio (PAPR) [8], which is defined as

$$PAPR = \frac{\max_{0 \le n \le N-1} |x[n]|^2}{E[|x[n]|^2]},$$
(2)

where $E[\cdot]$ stands for the statistical expectation. For a large N, $\{x[n]\}_{n=0}^{N-1}$ are asymptotically independent and approximately complex Gaussian distributed, and the real part and the imaginary part of x[n] are asymptotically independent [10]. Then, the complementary cumulative distribution function (CCDF) of the PAPR can be shown to be [9, 10]

$$Pr\{PAPR > r\} = 1 - (1 - e^{-r})^N.$$
 (3)

3. PAPR IN VLC-OFDM

In VLC systems, intensity modulation (IM) is employed at the transmitter. The forward signal drives the LED which in turn converts the magnitude of the input electric signal into optical intensity. The human eye cannot perceive fast-changing variations of the light intensity, and only responds to the average light intensity. Direct detection (DD) is employed at the receiver. A photodiode (PD) transforms the received optical power into the amplitude of an electrical signal.

IM/DD schemes require the baseband signal in the VLC to be real-valued. Thus, complex-valued RF-OFDM in (1) cannot be used in VLC directly. According to the property of the inverse Fourier transform, a real-valued time-domain signal x[n] corresponds to a frequency-domain signal X_k that is Hermitian symmetric; i.e., $X_k = X_{N-k}^*, 1 \le k \le N - 1$, where * denotes complex conjugate. The 0th and N/2th subcarrier are null; i.e., $X_0 = 0, X_{N/2} = 0$. Then we can obtain the real-valued time-domain signal x[n] as

$$x[n] = \frac{2}{\sqrt{N}} \sum_{k=1}^{N/2-1} \left(\Re(X_k) \cos\left(\frac{2\pi kn}{N}\right) - (4) \\ \Im(X_k) \sin\left(\frac{2\pi kn}{N}\right) \right), n = 0, 1, \dots, N-1,$$

where $\Re(\cdot)$ denotes the real part of X_k , and $\Im(\cdot)$ denotes the imaginary part of X_k . Since the DC component is zero $(X_0 = 0), x[n]$ has zero mean. According to the Central Limit Theorem, for a large N, $\{x[n]\}_{n=0}^{N-1}$ are asymptotically independent and approximately Gaussian distributed [16] with probability density function (PDF) $Pr(x[n] = z) = 1/\sigma_x \cdot$ $\phi(z/\sigma_x)$, where $\phi(x) = \frac{1}{\sqrt{2\pi}}e^{-\frac{1}{2}x^2}$ is the PDF of the standard Gaussian distribution, and σ_x^2 is the variance of x[n]. According to the definition of PAPR in (2), the PAPR of realvalued OFDM signal x[n] is given by

$$\mathcal{P} = \frac{\max_{0 \le n \le N-1} x^2[n]}{\sigma_x^2}.$$
(5)

Assume x[n] is independent and identically distributed, the CCDF of \mathcal{P} can be shown as [16]

$$CCDF_{\mathcal{P}}\{r_p\} = Pr\{\mathcal{P} > r_p\}$$

$$= 1 - Pr\{\mathcal{P} \le r_p\}$$

$$= 1 - Pr\{-\sigma_x \sqrt{r_p} \le x[n] \le \sigma_x \sqrt{r_p}, 0 \le n \le N-1\}$$

$$= 1 - [Pr\{-\sigma_x \sqrt{r_p} \le x[0] \le \sigma_x \sqrt{r_p}\}]^N$$

$$= 1 - [\Phi(\sqrt{r_p}) - \Phi(-\sqrt{r_p})]^N,$$
(6)

where $\Phi(x) = \int_{-\infty}^{x} \phi(t) dt$.

For the real-valued bipolar signal $\{x[n]\}_{n=0}^{N-1}$, the square of the maximum value $\left(\max_{0 \le n \le N-1} x[n]\right)^2$ can be seen as the upper peak power, and the square of the minimum value $\left(\min_{0 \le n \le N-1} x[n]\right)^2$ can be seen as the lower peak power. Let us define the upper PAPR (UPAPR) of x[n] as

$$\mathcal{U} \triangleq \left(\max_{0 \le n \le N-1} x[n]\right)^2 / \sigma_x^2, \tag{7}$$

and define the lower PAPR (LPAPR) of x[n] as

$$\mathcal{L} \triangleq \left(\min_{0 \le n \le N-1} x[n]\right)^2 / \sigma_x^2.$$
(8)

Accordingly, we can derive the CCDF of UPAPR as

$$CCDF_{\mathcal{U}}\{r_u\} = Pr\{\mathcal{U} > r_u\}$$

$$= 1 - Pr\{\mathcal{U} \le r_u\}$$

$$= 1 - Pr\{x[n] \le \sigma_x \sqrt{r_u}, 0 \le n \le N - 1\}$$

$$= 1 - [Pr\{x[0] \le \sigma_x \sqrt{r_u}\}]^N$$

$$= 1 - \Phi^N(\sqrt{r_u}),$$
(9)

and the CCDF of LPAPR is derived as

$$CCDF_{\mathcal{L}}\{r_{l}\} = Pr\{\mathcal{L} > r_{l}\}$$
(10)
= $1 - Pr\{\mathcal{L} \le r_{l}\}$
= $1 - Pr\{x[n] \ge -\sigma_{x}\sqrt{r_{l}}, 0 \le n \le N - 1\}$
= $1 - [Pr\{x[0] \ge -\sigma_{x}\sqrt{r_{l}}\}]^{N}$
= $1 - \Phi^{N}(\sqrt{r_{l}}).$

Note that the UPAPR and the LPAPR have the same CCDF. Fig. 1 shows the simulated CCDF of UPAPR and LPAPR with various constellation orders and numbers of subcarriers. In this paper, all the simulation results are taken from 100000 OFDM symbols with 4-QAM, 64-QAM, and 256-QAM constellations. Theoretical results are plotted as well to examine our analysis. We can observe that the distribution of \mathcal{U} and \mathcal{L} are independent of the constellations orders and increase with more subcarriers. When N = 128, slight differences can be found between the simulated results and the theoretical values. When N = 1024, the simulated results match the



Fig. 1. CCDF of UPAPR and LPAPR with various constellation orders and numbers of subcarriers.

theoretical values very well because the central limit theory holds better.

From the definitions of UPAPR and LPAPR, we can see that UPAPR and LPAPR are not independent distributed. Therefore, it is necessary to know the joint cumulative distribution function of UPAPR and LPAPR, which can be obtained as

$$F_{\mathcal{L},\mathcal{U}}(r_l, r_u) = Pr\{\mathcal{L} \le r_l, \mathcal{U} \le r_u\}$$
(11)
= $Pr\{-\sigma_x \sqrt{r_l} \le x[n] \le \sigma_x \sqrt{r_u}, 0 \le n \le N-1\}$
= $[Pr\{-\sigma_x \sqrt{r_l} \le x[0] \le \sigma_x \sqrt{r_u}]^N$
= $[\Phi(\sqrt{r_u}) - \Phi(-\sqrt{r_l})]^N.$

The joint PDF of UPAPR and LPAPR is

$$= \frac{f_{\mathcal{L},\mathcal{U}}(r_l, r_u)}{\frac{\partial^2 F_{\mathcal{L},\mathcal{U}}(r_l, r_u)}{\partial r_l \partial r_u}}$$

$$= \frac{\phi(\sqrt{r_u})\phi(\sqrt{r_l})}{4\sqrt{r_l r_u}} N(N-1) [\Phi(\sqrt{r_u}) - \Phi(-\sqrt{r_l})]^{N-2}.$$
(12)

4. LINEAR SCALING AND BIASING

LEDs place dynamic range constraints $[I_L, I_H]$ on the input signal, where I_L denotes turn-on current and I_H denotes the maximum input current [13]. The Dynamic range can be denoted by $D \triangleq I_H - I_L$. Since I_L is positive, the bipolar signal x[n] cannot serve as the input of LEDs directly. The forward signal y[n] can be obtained from the OFDM signal x[n] after both a linear scaling and a biasing operation; i.e.,

$$y[n] = \alpha x[n] + B, \quad 0 \le n \le N - 1,$$
 (13)

where α denotes the scaling factor used to control the input power back-off

$$\gamma \triangleq \frac{D^2}{\alpha^2 \sigma_x^2},\tag{14}$$

and B denotes the biasing level. α and B are both real-valued. The resulting signal, y[n], has a mean value B and a variance $\sigma_y^2 = E[\alpha^2]\sigma_x^2$.

Brightness control is essential for the illumination function in VLC. The principle of brightness control is to make the average amplitude of the input forward signal equal to I_{des} , which corresponds to a desired average output optical intensity. Since the mean value of the input forward signal signal y[n] is equal to B, it is straightforward to set biasing level B equal to I_{des} ; i.e., $B = I_{des}$, which is called the biasing adjustment method [15]. Therefore, the biasing level Bis determined by the illumination requirements. Let us define biasing ratio as

$$\varsigma \triangleq \frac{B - I_L}{D}.$$
 (15)

Without loss of generality, we only consider biasing ratio in the range $0 \le \varsigma \le 0.5$, because any forward signal s[n] with biasing ratio $0.5 < \varsigma \le 1$ can be created from y[n], which has biasing ratio $0 \le 1 - \varsigma \le 0.5$ and is within the dynamic range $[I_L, I_H]$, by $s[n] = I_H + I_L - y[n]$.

4.1. Symbol-invariant scaling factor

Assume that the scaling factor α or input power back-off γ is fixed for all OFDM symbols. Given the biasing ratio ς and the input power back-off γ , it is useful to know the probability that the input OFDM symbol $\{y[n]\}_{n=0}^{N-1}$ is beyond the dynamic range of LEDs, which is given by

$$Pr\{\{y[n]\}_{n=0}^{N-1} \text{ is out of dynamic range } | \gamma,\varsigma\}$$
(16)
$$= Pr\{y[n] > I_H, \text{ or } y[n] < I_L | \gamma,\varsigma\}$$

$$= Pr\left\{x[n] > \frac{I_H - B}{\alpha}, \text{ or } x[n] < \frac{I_L - B}{\alpha} | \gamma,\varsigma\right\}$$

$$= 1 - Pr\left\{\frac{I_L - B}{\alpha} \le \{x[n]\}_{n=0}^{N-1} \le \frac{I_H - B}{\alpha} | \gamma,\varsigma\right\}$$

$$= 1 - Pr\left\{\frac{I_L - B}{\alpha\sigma_x} \le \frac{\{x[n]\}_{n=0}^{N-1}}{\sigma_x} \le \frac{I_H - B}{\alpha\sigma_x} | \gamma,\varsigma\right\}$$

$$= 1 - Pr\left\{-\varsigma\sqrt{\gamma} \le \frac{\{x[n]\}_{n=0}^{N-1}}{\sigma_x} \le (1 - \varsigma)\sqrt{\gamma},\right\}$$

$$= 1 - Pr\{\mathcal{L} \le \varsigma^2\gamma, \text{ and } \mathcal{U} \le (1 - \varsigma)^2\gamma\}$$

$$= 1 - F_{\mathcal{L},\mathcal{U}}(\varsigma^2\gamma, (1 - \varsigma)^2\gamma),$$

where $(I_L - B)/\alpha\sigma_x = -\zeta\sqrt{\gamma}$ and $(I_H - B)/\alpha\sigma_x = (1 - \zeta)\sqrt{\gamma}$ are obtained from the Eqs. (14) (15). We can see that the probability in Eq. (16) depends on the joint distribution of UPAPR and LPAPR. Fig. 2 shows simulated and theoretical results for 128 subcarriers. Fig. 3 shows simulated and theoretical results for 1024 subcarriers. We can observe that the joint distribution of UPAPR and LPAPR is independent of constellations, and the simulated results match the theoretical values well. For a biasing ratio $\zeta \in [0, 0.5]$, lower biasing



Fig. 2. Probability that the input symbol $\{y[n]\}_{n=0}^{N-1}$ is beyond the dynamic range of LEDs given power back-off and biasing ratio (128 subcarriers).

ratio requires larger input power back-off to achieve the same probability.

4.2. Symbol-variant scaling factor

Assume that the scaling factor α can be adjusted symbol by symbol. The variance σ_y^2 can be maximized by selecting α with the greatest value for each OFDM symbol. To ensure y[n] is within the dynamic range of the LED, we can obtain an α with the greatest value as

$$\alpha = \min\left\{\frac{I_H - B}{\max_{0 \le n \le N-1} x[n]}, \frac{I_L - B}{\min_{0 \le n \le N-1} x[n]}\right\}$$
(17)

We can obtain the variance of y[n] as

$$\sigma_y^2 = \sigma_x^2 E[\alpha^2]$$

$$= D^2 E_{\mathcal{U},\mathcal{L}} \left[\min\left\{ \frac{(1-\zeta)^2}{\mathcal{U}}, \frac{\zeta^2}{\mathcal{L}} \right\} \right]$$

$$= D^2 \int_0^\infty \int_0^\infty \min\left\{ \frac{(1-\zeta)^2}{r_u}, \frac{\zeta^2}{r_l} \right\} f_{\mathcal{L},\mathcal{U}}(r_l, r_u) dr_l dr_u$$

where $f_{\mathcal{L},\mathcal{U}}(r_l, r_u)$ is the joint PDF of UPAPR and LPAPR from Eq. (12). We can observe that the variance σ_y^2 depends on three factors: biasing ratio, upper PAPR of the OFDM signal and lower PAPR of the OFDM signal. Note that the dynamic range *D* is a fixed value, which is determined by characteristics of LEDs. The scaling factor α varies symbol by symbol since \mathcal{U} and \mathcal{L} are both random variables. We treat α as part of the channel and assume that α for each symbol can be perfectly estimated at the receiver. Fig. 4 is a plot of the variance σ_y^2 versus the biasing ratio with normalized dynamic range. The plots demonstrate that our theoretical analysis matches the simulated results very well. The variances are identical for all three constellation orders since the



Fig. 3. Probability that the input symbol $\{y[n]\}_{n=0}^{N-1}$ is beyond the dynamic range of LEDs given power back-off and biasing ratio (1024 subcarriers).



Fig. 4. Variance σ_y^2 as a function of the biasing ratio with normalized dynamic range.

distributions of LPAPR and UPAPR are independent of constellations. The variance decrease with increasing subcarriers because both the UPAPR and LPAPR will increase when there are more subcarriers. Since the OFDM signal has a symmetric distribution, the maximum variance occurs at biasing ratio 0.5 when the OFDM signal is biased around the middle point of the dynamic range.

5. CONCLUSIONS

In this paper, we derived the CCDF and the joint distribution of UPAPR and LPAPR. The performance of VLC-OFDM with dynamic range and average amplitude constraints are shown to be directly related with UPAPR and LPAPR. Simulation results matched the theoretical analysis well.

6. REFERENCES

- [1] Dominic C. O'Brien, Lubin Zeng, Hoa Le-Minh, Grahame Faulkner, Joachim W. Walewski, and Sebastian Randel, "Visible light communications: Challenges and possibilities," in 2008 IEEE 19th International Symposium on Personal, Indoor and Mobile Radio Communications. Sept. 2008, pp. 1–5, IEEE.
- Hany Elgala, Raed Mesleh, and Harald Haas, "Indoor optical wireless communication: potential and state-of-the-art," *IEEE Communications Magazine*, vol. 49, no. 9, pp. 56–62, Sept. 2011.
- [3] Mohammad Noshad and Maite Brandt-Pearce, "Can Visible Light Communications Provide Gb/s Service?," arXiv:1308.3217, pp. 1–7, Aug. 2013.
- [4] IEEE Standard for Local and Metropolitan Area Networks–Part 15.7: Short-Range Wireless Optical Communication Using Visible Light, 2011.
- [5] H. Elgala, R. Mesleh, H. Haas, and B. Pricope, "OFDM Visible Light Wireless Communication Based on White LEDs," in 2007 IEEE 65th Vehicular Technology Conference. Apr. 2007, pp. 2185–2189, IEEE.
- [6] Jean Armstrong, "OFDM for Optical Communications," *Journal of Lightwave Technology*, vol. 27, no. 3, pp. 189–204, Feb. 2009.
- [7] Z. Yu, R. J. Baxley, and G. T. Zhou, "EVM and achievable data rate analysis of clipped OFDM signals in visible light communication," *EURASIP Journal on Wireless Communications and Networking*, vol. 2012, Oct. 2012.
- [8] R. J. Baxley and G. T. Zhou, "Peak-to-Average Power Ratio Reduction," in *Digital Signal Processing Handbook*, Vijay Madisetti, Ed. CRC Press, 2nd edition, 2009.
- [9] R.W. Bauml, R.F.H. Fischer, and J.B. Huber, "Reducing the peak-to-average power ratio of multicarrier modulation by selected mapping," *Electronics Letters*, vol. 32, no. 22, pp. 2056, 1996.
- [10] Hideki Ochiai and Hideki Imai, "On the distribution of the peak-to-average power ratio in OFDM signals," *IEEE Transactions on communications*, vol. 49, no. 2, pp. 282–289, 2001.
- [11] D.L. Goeckel and P.E. Kelly, "A modern extreme value theory approach to calculating the distribution of the peak-to-average power ratio in OFDM systems," in 2002 IEEE International Conference on Communications. 2002, vol. 3, pp. 1686–1690, Ieee.

- [12] Tao Jiang, Mohsen Guizani, and Hsiao-hwa Chen, "Derivation of PAPR Distribution for OFDM Wireless Systems Based on Extreme Value Theory," *IEEE Transactions on Wireless Communications*, vol. 7, no. 4, pp. 1298–1305, 2008.
- [13] H. Elgala, R. Mesleh, and H. Haas, "Non-linearity effects and predistortion in optical OFDM wireless transmission using LEDs," *International Journal of Ultra Wideband Communications and Systems*, vol. 1, no. 2, pp. 143–150, 2009.
- [14] Z. Yu, R.J. Baxley, and G.T. Zhou, "Peak-to-Average Power Ratio and Illumination-to-Communication Efficiency Considerations in Visible Light OFDM Systems," in *IEEE Intl. Conference on Acoustics, Speech,* and Signal Processing, Vancouver, Canada, 2013.
- [15] Z. Yu, R. J. Baxley, and G. T. Zhou, "Brightness Control in Dynamic Range Constrained Visible Light OFDM Systems," *arXiv*:1304.0193, Mar. 2013.
- [16] Hua Yu, Min Chen, and Gang Wei, "Distribution of PAR in DMT systems," *Electronics Letters*, vol. 39, no. 10, pp. 799, 2003.
- [17] Chao Ma, Hongming Zhang, Minyu Yao, Zhengyuan Xu, and Kaiyun Cui, "Distributions of PAPR and crest factor of OFDM signals for VLC," 2012 IEEE Photonics Society Summer Topical Meeting Series, vol. 5, no. 1, pp. 119–120, July 2012.