

# DOA ESTIMATION WITH HISTOGRAM ANALYSIS OF SPATIALLY CONSTRAINED ACTIVE INTENSITY VECTORS

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## ABSTRACT

The active intensity vector (AIV) is a common descriptor of the sound field. In microphone array processing, AIV is commonly approximated with beamforming operations and utilized as a direction of arrival (DOA) estimator. However, in its original form, it provides inaccurate estimates in sound field conditions where coherent sound sources are simultaneously active. In this work we utilize a higher order intensity-based DOA estimator on spatially-constrained regions (SCR) to overcome such limitations. We then apply 1-dimensional (1D) histogram processing on the noisy estimates for multiple DOA estimation. The performance of the estimator is shown with a 7-channel microphone array, fitted on a rigid mobile-like device, in reverberant conditions and under different signal-to-noise ratios.

**Index Terms**— direction of arrival, higher order active intensity vector, multiple sound sources, microphone arrays

## 1. INTRODUCTION

Direction of arrival (DOA) estimation is one of the fundamental array processing problems that can be applied in many applications such as spatial sound reproduction [1, 2], acoustic analysis of enclosed spaces [3], or spatial filtering [4, 5]. The selection of a DOA estimator depends on the application's requirements in terms of resolution and computational cost. For example, in sound reproduction such as in [1], the accuracy of the DOA estimator is more forgiving than in spatial filtering where estimation errors will result to spatial noise mixing into the target signal. The most popular approaches for DOA estimation are the steered-response power [6, 7], maximum likelihood, subspace-based [8–10], sensor phase-based [11], and intensity-based [12–15].

In our previous work we proposed to apply histogram processing to the active intensity vector (AIV) estimates, aiming

at accurate DOA estimation in the 3D space [13]. The results indicated that very low DOA errors can be achieved. The use of AIV estimates in 2D scenarios requires a minimum of three microphone signals from which the pressure and the particle velocity are approximated. Recent developments in microphone array technology allow the use of much higher number of microphones. Although such arrays can provide beamformers with high directivity, intensity-based DOA estimators utilize the information only up to first order [12]. Hybrid approaches have been proposed in [16, 17]. A higher order AIV has been proposed for signal-dependent spatial sound reproduction where multiple higher order active intensity estimates are utilized to estimate a set of parameters which are then used to re-synthesize the sound field for loudspeaker reproduction in the spherical harmonic domain [18, 19].

In this contribution

- we propose the use of a higher order AIV in spatially constrained regions (SCR),
- we post-process the instantaneous spatially constrained (SC) AIV estimates with 1D histogram processing to obtain accurate final DOA estimates and avoid noisy estimations,
- we show the performance of SC-AIV for a prototype compact microphone array with 7 microphones,
- we demonstrate the advantage of using SC-AIV in DOA estimation of multiple non-coherent sources inside a SCR when coherent sources are active outside the SCR.

The paper is organized as follows. In Section 2 the signal model and AIV background are presented. Section 3 describes the proposed method of estimating the higher-order AIV and post-processing the DOA estimates with 1D histograms. Section 4 presents the experimental setup for evaluation and the results using a real microphone array in reverberant environments with the presence of multiple speech sources. Section 5 presents our conclusions.

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## 2. BACKGROUND

In the current work matrices and vectors are denoted with bold-faced—upper and lower case correspondingly—symbols. The entries of both matrices and vectors are denoted with the same non-bold-faced symbols, appended with a subindex. Let us denote with  $\mathbf{x}(k, n) \in \mathbb{C}^{Q \times 1}$  the time-frequency (TF) domain signals from a microphone array with  $Q$  sensors, where  $k$  is the frequency index and  $n$  is the time index. The output of a signal-independent beamformer is denoted as

$$y(k, n) = \mathbf{w}(k)^H \mathbf{x}(k, n), \quad (1)$$

where  $\mathbf{w}(k) \in \mathbb{C}^{Q \times 1}$  is a set of complex multipliers that mix the microphone signals to provide the output signal  $y$ , and  $(\cdot)^H$  denotes Hermitian transposition.

The AIV is defined as  $\mathbf{I} = 0.5\Re[p^* \mathbf{v}]$ , where  $p$  denotes sound pressure,  $\mathbf{v} = [v_x, v_y, v_z]^T \in \mathbb{C}^{3 \times 1}$  denotes particle velocity,  $\Re$  is the real part operator and  $*$  is the conjugate operator. The AIV corresponds to the direction of the sound energy flow, therefore the DOA can be estimated as a vector pointing to the opposite direction. Instead of measuring the pressure and particle velocity in sound reproduction and DOA estimation methods, the sound intensity is approximated by measuring the pressure and particle velocity components with omnidirectional and dipole microphones [1]. The AIV in the TF domain for the 2D case is

$$\mathbf{I}(k, n) = \frac{1}{2} \Re \left\{ s_p(k, n)^* \begin{bmatrix} s_x(k, n) \\ s_y(k, n) \end{bmatrix} \right\}, \quad (2)$$

where  $s_p$  is a signal originating from the omnidirectional microphone and  $s_x, s_y$  are signals originating from dipole microphones with their negative phase in the x- and y-axis. When using a microphone array, these signals can be synthesized with beamforming operations, as defined in (1), using signal-independent techniques such as the spherical harmonic framework or  $l_2$  minimization [20].

## 3. DOA ESTIMATION WITH SPATIALLY-CONSTRAINED ACTIVE INTENSITY VECTORS

The AIV can be used to provide instantaneous DOA estimates. Recently, a higher-order AIV was introduced for spatial sound reproduction, where the active intensity is estimated for multiple spatially-constrained areas that sum up to an omnidirectional pattern [18]. In this work we investigate the use of the higher order AIV as a robust DOA estimator in the SCR of interest when a coherent source occurs outside, referred to as SC-AIV. We apply 1D histogram post-processing to retrieve accurate DOA estimates of multiple sources. A demonstrative scenario is illustrated in Fig. 1, where multiple talkers are active within a SCR, with a coherent source outside this area. This is a typical scenario where a mobile device is used for recording a sound scene. Using the AIV in such a scenario will provide inaccurate estimates that modulate between the two coherent sources. In contrast SC-AIV

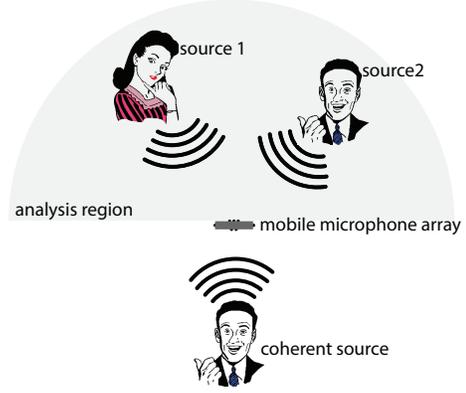


Fig. 1. Recording scenario

cope with the presence of coherent sources as it will be demonstrated in Section 4.

### 3.1. Higher order active intensity vector

The higher order AIV is defined as in (2)

$$\mathbf{I}_{\text{HO}}(k, n) = \frac{1}{2} \Re \left\{ s_{\text{PHO}}(k, n)^* \begin{bmatrix} s_{x\text{HO}}(k, n) \\ s_{y\text{HO}}(k, n) \end{bmatrix} \right\}, \quad (3)$$

with the difference that  $s_{\text{PHO}}, s_{x\text{HO}}, s_{y\text{HO}}$  are signals that approximate the spatially constrained pressure and particle velocity for the x- and y-axis respectively. The directional patterns  $T_{\text{PHO}}(\phi)$ ,  $T_{x\text{HO}}(\phi)$  and  $T_{y\text{HO}}(\phi)$  of the spatially constrained pressure and particle velocity components  $s_{\text{PHO}}, s_{x\text{HO}}, s_{y\text{HO}}$ , with  $\phi \in [-180, 180)$ , are

$$T_{\text{PHO}}(\phi) = c(\phi), \quad (4)$$

$$T_{x\text{HO}}(\phi) = c(\phi) \cos(\phi), \quad (5)$$

$$T_{y\text{HO}}(\phi) = c(\phi) \sin(\phi), \quad (6)$$

where  $c(\phi)$  is a spatial windowing function that focuses on the direction of interest. The advantage of such spatial windowing is that DOA estimates within the spatial window are not affected by sources outside the window while it remains as computationally efficient as the first order intensity estimator. The design of the spatially constrained pressure and particle velocity components is based on signal-independent beamforming techniques via  $l_2$  minimization in the space domain. By setting each function of (4,5,6) as a target pattern, we consider to minimize the squared error between the actual and target response at directions  $\phi$ . The regularized least squares solution is given by [21]

$$\mathbf{w}(k) = \left[ \mathbf{V}^H(k) \mathbf{V}(k) + \lambda \mathbf{I}_Q \right]^{-1} \mathbf{V}^H(k) \mathbf{t}, \quad (7)$$

where  $\mathbf{t} \in \mathbb{R}^{N \times 1}$  is the target pattern defined at  $N$  points, chosen from (4, 5) or (6),  $\mathbf{V} \in \mathbb{C}^{N \times Q}$  is the steering vector,  $\mathbf{I}_Q \in \mathbb{R}^{Q \times Q}$  is the identity matrix, and  $\lambda$  is a regularization parameter.

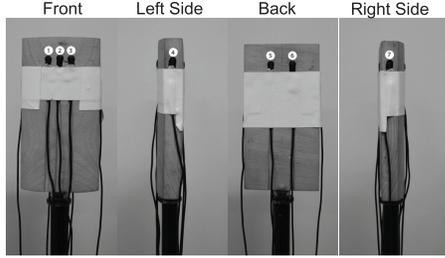


Fig. 2. Photos of the microphone array prototype.

### 3.2. 1D histogram processing

The SC-AIV estimates, obtained according to (3), provide instantaneous DOA estimates at each TF point of interest. We collect such DOA estimates from  $B$  consecutive time frames and post process them by forming 1D histograms for final multiple sources DOA estimation retrieval. The block of  $B$  time frames slides one frame each time. The manipulation of the 1D histograms follows the principles described in [13, 16, 22]. The 1D histogram is further smoothed with a Gaussian window  $\mathbf{h}_A(\phi)$  of zero mean and standard deviation (std) equal to  $\sigma_A$ , leading to

$$\mathbf{y}_s(\phi) = \sum_i \mathbf{y}(i) \mathbf{h}_A(\phi - i), \quad (8)$$

where  $\mathbf{h}(\phi) = \frac{1}{\sqrt{2\pi}\sigma^2} e^{-\frac{1}{2}\frac{\phi^2}{\sigma^2}}$  is the Gaussian window,  $\mathbf{y}(\phi)$  is the original 1D histogram and  $\mathbf{y}_s(\phi)$  is the smoothed one. We then iteratively detect the highest peak of the smoothed histogram  $\mathbf{y}_s^g(\phi)$ , identify its index as the DOA of a source,  $\phi_g = \arg \max_{\phi} \mathbf{y}_s^g(\phi)$  and remove its contribution from the histogram,  $\delta_g = \mathbf{y}_s(\phi) \odot \mathbf{h}_C(\phi - \phi_g)$  by applying a second Gaussian window  $\mathbf{h}_C(\phi)$  of zero mean and std equal to  $\sigma_C$  until we reach the number  $G$  of sources, which is assumed to be known. Thus the smoothed histogram at each next iteration would be  $\mathbf{y}_s^{g+1}(\phi) = \mathbf{y}_s^g(\phi) - \delta_g$ .

## 4. EVALUATION

Seven microphones (DPA 4060) are fitted in a wooden rectangular object, similar to the dimensions of a mobile device, of size  $5.5 \times 2 \times 11$  cm, shown in Fig. 2. The array steering vectors were obtained in an anechoic environment. Measurements in a reverberant environment were performed by placing the microphone array and the rotator in a room of  $RT_{60} = 0.3$  sec and a loudspeaker at 2 m distance. The recording scenarios were generated by convolving the recorded reverberant impulse responses with a dry signal and adding white noise with different signal-to-noise ratios (SNR). The frequency range for DOA estimation was set in [500, 3500] Hz, while the stds in the histogram processing were  $\sigma_A = 10^\circ$  and  $\sigma_C = 40^\circ$ . The spatially constrained pressure and particle velocity beampatterns are calculated by setting

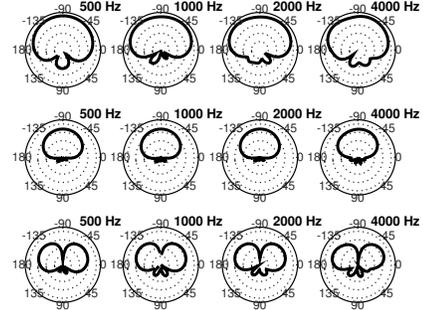


Fig. 3. Synthesized spatially constrained intensity pressure (top) and spatially constrained particle velocity (middle and bottom). Each dotted circle indicates a drop of 10 dB.

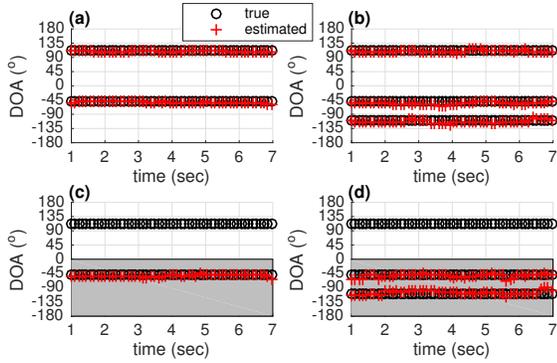
$$c(\phi) = \begin{cases} 1 & \phi \in [-180, 0] \\ 0 & \phi \in (0, 180), \end{cases} \quad (9)$$

as shown in the grayed region in Fig. 1. The synthesized beampatterns are shown in Fig. 3.

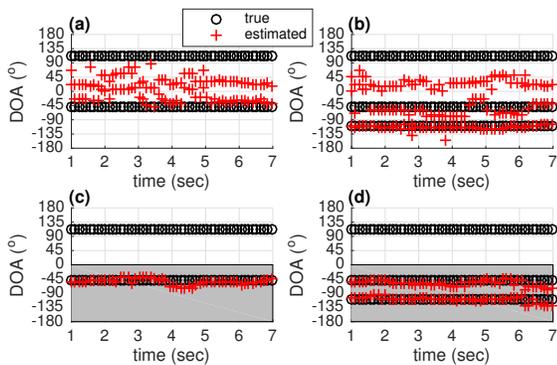
We investigate the performance of the proposed algorithm and the employed microphone array in two different sets of real conditions, i.e., when only incoherent sources are active and when there is one pair of coherent sources. For both sets we show results using the first-order AIV estimator (2) and the SCR-AIV one (3). The advantage of the SC-AIV estimator is that we obtain DOA estimates only for those sources that are in the analysis region and are not affected by a source outside. The number of active sources for each estimator is assumed to be known.

We demonstrate the aforementioned scenarios along with the performance of each estimator in Figs. 4 and 5. For these results the SNR was equal to 20 dB. We observe that when the involved sources are incoherent both the AIV and the SC-AIV estimators exhibit accurate DOA estimation performance (Fig. 4). On the other hand, for coherent sources, the AIV estimator fails to accurately estimate the DOAs as indicated by the estimates in between the true DOAs of the involved sources (Fig. 5 (a) and (b)), while the SC-AIV shows robust performance, providing accurate DOA estimates for the sources in its field of view. The results in Fig. 5 (a) and (c) involve two coherent sources, one in the analysis area and one outside, while the results in Fig. 5 (b) and (d) follow a scenario similar to the one demonstrated in Fig. 1, where the source outside the SCR is coherent with one of the sources in the analysis area.

We proceed the evaluation of the AIV estimator and the proposed SC-AIV estimator with results of the mean absolute estimation error (MAEE) [22] for three different SNR conditions, when two sources are simultaneously active, both for the coherent and incoherent case in Fig. 6. The sources were positioned in 10 random direction pairs around the array, assuring that one source is always outside the analysis area and

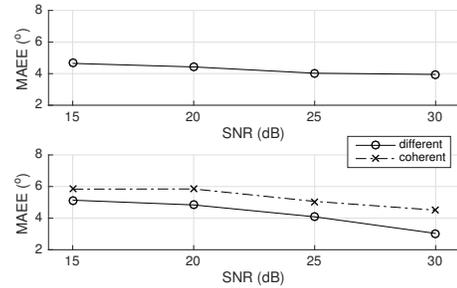


**Fig. 4.** DOA estimation result for two and three simultaneously active incoherent sources with (a)-(b) the AIV estimator, and (c)-(d) the SC-AIV estimator. The gray region in the plots indicates the analysis area.

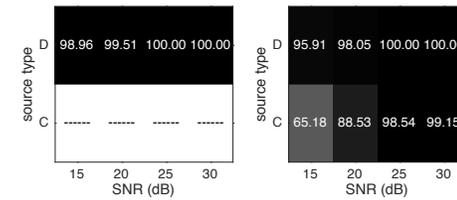


**Fig. 5.** DOA estimation result with coherent sources when two and three source are active with (a)-(b) the AIV estimator, and (c)-(d) the SC-AIV. The gray region in the plots indicates the analysis area.

the other is inside. The MAEE involves estimates that exhibit error not higher than  $15^\circ$ . For the AIV estimator only the case of incoherent sources is presented, since first order AIV fails at providing sensible DOA estimates for coherent sources (see also Fig. 7). For SC-AIV the MAEE refers to the target source, i.e., the source in the analysis area. In Fig. 7 we provide the success scores (SS) of the AIV (left) and the SC-AIV (right) estimators, i.e., the percentage of times that the evaluated DOA is in the range of  $\pm 15^\circ$  from the true DOA. We observe that when the active sources are incoherent both estimators achieve accurate DOA estimation for all different SNR conditions. Moreover, SC-AIV achieves robust DOA estimation of the target source when a coherent source is simultaneously active. The AIV estimator exhibits high SS for incoherent sources (D), but is severely affected by the presence of a coherent source (C), as also demonstrated in Fig. 5. Thus the SS results are not applicable for this scenario. On the other hand the proposed SC-AIV estimator achieves high SS for both different and coherent sources scenarios. Lower



**Fig. 6.** Mean absolute estimation error using AIV for different sources (top) and SC-AIV for different and coherent sources (bottom).



**Fig. 7.** Success scores in DOA estimation using the AIV (left) and the SC-AIV (right) for incoherent (D) and coherent (C) sources.

SNR conditions lead to reduced SS, due to the noise boost caused by the beamforming operations, but the performance of the estimator remains in a functional range of values.

## 5. CONCLUSION

We presented a method to obtain accurate DOA estimates in sound field scenarios with multiple sound sources. We relied on the estimation of a higher order, spatially constrained, active intensity vector and 1D histogram post-processing. The method was evaluated using a real microphone array, mounted on a rigid, mobile-like device, in a reverberant environment with different signal-to-noise ratio conditions. The proposed method achieves to deliver accurate DOA estimates even in scenarios with coherent sources, while its performance is comparable with the first order active intensity for simultaneously active, incoherent sources.

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