FULLY DIGITAL AND HYBRID BEAMFORMING DESIGN FOR MILLIMETER-WAVE MIMO-OFDM TWO-WAY RELAYING SYSTEMS

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ABSTRACT

In this work, we consider the design of hybrid analogdigital (HAD) multi-carrier MIMO-OFDM two-way relaying systems, where the relay station is equipped with a HAD amplify-and-forward architecture and every mobile station is equipped with a fully-digital beamforming architecture. We propose a sub-optimal solution by reformulating the original non-convex problem as a constrained Tucker2 decomposition with the objective of minimizing the sum Euclidean-norm between the HAD amplification matrices and their fully-digital counterparts. For the fully-digital amplification matrix design, we use a Frobenius-norm maximization of the effective channels on every subcarrier and propose an effective solution applicable for multi-stream communication scenarios. After that, we propose an alternating maximization (AltMax) HAD solution by exploiting the tensor structure of the reformulated problem. Simulation results are provided, where we show that the proposed fully-digital and AltMax-based HAD amplification matrix designs outperform some benchmark methods, especially for multi-stream communication scenarios.

Index Terms— Two-way relaying, hybrid beamforming, millimeter-wave communication, Tucker2 tensor decomposition.

1. INTRODUCTION

Recently, the integration of millimeter-wave (mm-wave) frequencies and massive MIMO techniques has been recognized as one of the key solutions to improve the spectral efficiency (SE) of 5G and beyond mobile systems [1, 2]. However, two major practical challenges arise. On the one hand, the conventional fully-digital beamforming architectures become impractical, due to their high-cost and high-energy consumption, as they require a dedicated radio-frequency (RF) chain for each antenna. On the other hand, high-frequency communications are very sensitive to signal-blockage and signalattenuation, which makes mm-wave-based systems mainly applicable to short-range communications. Therefore, hybrid analog-digital (HAD) beamforming architectures [2–6] and relay-assisted communications [7–12] have been proposed to tackle these challenges. In HAD architectures, the number of RF chains can be reduced significantly, compared to the number of the antenna elements. Meanwhile, relay stations (RSs) can be used to increase the communication range.

Among several relaying schemes, two-way relaying (TWR) is known to be more resources efficient [8]. In TWR [7–13], the data transmission between two mobile stations (MSs) occurs in two subsequent transmission phases. First, both MSs transmit to the RS. Then, the RS transmits back to both MSs, either using a decode-and-forward (DF) or an amplify and forward (AF) relaying architecture. In this paper, we focus our attention on the AF scheme. Moreover, it is known that TWR systems can be transformed into two separate single-user MIMO channels if the self-interference at every MS is subtracted [8,9]. This implies that, if the amplification matrix is known, the optimal decoding and encoding matrices at the MSs are given by the dominant singular vectors of the resulting effective channels. Thus, the remaining challenge is how to design the RS amplification matrix. To this end, the authors of [8] proposed a method, called Algebraic norm-maximizing (ANOMAX), which designs the RS amplification matrix that maximizes the weighted sum of the Frobenius norms of the effective channels. However, based on the observations, ANOMAX is mainly applicable to singlestream transmissions. The authors of [9] extended ANOMAX by proposing rank-restored ANOMAX (RR-ANOMAX) to increase the rank of the amplification matrix by adjusting its singular values while preserving its subspaces. On the other hand, the authors of [7] proposed an amplification matrix design using the zero-forcing (ZF) and minimum mean square error (MMSE) filters. However, it was reported in [8], using computer simulations, that the ANOMAX-based solutions outperform the ZF-based and the MMSE-based solutions.

In this paper, we develop a new fully-digital RS amplification matrix design for wide-band multi-carrier MIMO OFDM AF TWR systems, which extends the results of [8] and [9]. To this end, we consider the Frobenius-norm maximization of the effective channels on every subcarrier and propose a different solution than [9] to further enhance the rank of the obtained fully-digital RS amplification matrices, termed enhanced RR-ANOMAX (ERR-ANOMAX). As the

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second contribution of the paper, we design HAD amplification matrix by reformulating the original non-convex problem as a constrained Tucker2 decomposition [14–16] with the objective of minimizing Euclidean-norm between the HAD amplification matrices and their fully-digital counterparts. Then, we propose two HAD solutions, a non-iterative HOSVD-based solution [15] and an iterative alternating maximization (AltMax)-based solution [5]. The simulation results show that ERR-ANOMAX outperforms ANOMAX and RR-ANOMAX in multi-stream communication scenarios.

2. SYSTEM MODEL

As depicted in Fig. 1, we consider¹ an AF TWR mm-wave massive MIMO-OFDM communication system, where two MSs communicate with each other via an intermediate RS over K subcarriers. It is assumed that the RS and MS ℓ are equipped with $M_{\rm RS}$ and M_{ℓ} antennas, respectively. For $\ell \in \{1, 2\}$ and $k \in \{0, \ldots, K-1\}$, let $H_{\ell,k}$ be $M_{\rm RS} \times M_{\ell}$ MIMO channel between MS ℓ and the RS on the kth subcarrier. We assume a TDD system so that the channel reciprocity holds, i.e., the reverse (downlink) channels are the transpose of the forward (uplink) channels. Let $F_{\ell,k}$ and $W_{\ell,k}$ denote the $M_{\ell} \times N_s$ fully-digital precoding and decoding matrices of MS ℓ on the kth subcarrier, respectively, where N_s denotes the number of data streams. Moreover, let G_k denote the $M_{\rm RS} \times M_{\rm RS}$ RS amplification matrix on the kth subcarrier.

In TWR systems, the data transmission occurs in two phases. In phase 1, the MSs transmit their signals to the RS simultaneously so that the received signal at the RS on the kth subcarrier can be written as

$$\boldsymbol{x}_{k} = \boldsymbol{H}_{1,k} \boldsymbol{F}_{1,k} \boldsymbol{s}_{1,k} + \boldsymbol{H}_{2,k} \boldsymbol{F}_{2,k} \boldsymbol{s}_{2,k} + \boldsymbol{n}_{\text{RS},k}, \qquad (1)$$

where $s_{\ell,k}$ is the data vector with $\mathbb{E}\{s_{\ell,k}s_{\ell,k}^H\} = I_{N_s}$ and $n_{\text{RS},k}$ contains zero-mean circularly symmetric complex Gaussian noise with variance σ_{RS}^2 . Here, it is assumed that $\mathbb{E}\{\|F_{\ell,k}\|_2^2\} = P_{\text{MS}}$, where P_{MS} denotes the maximum transmit power of a MS per subcarrier. In phase 2, the RS transmits x_k to both MSs so that the received signal at MS ℓ on the *k*th subcarrier is given as

$$\boldsymbol{y}_{\ell,k} = \boldsymbol{W}_{\ell,k}^{H} \boldsymbol{H}_{\ell,k}^{T} \boldsymbol{G}_{k} \boldsymbol{x}_{k} + \boldsymbol{W}_{\ell,k}^{H} \tilde{\boldsymbol{n}}_{\ell,k}, \qquad (2)$$

where $\tilde{n}_{\ell,k} = H_{\ell,k}^T G_k n_{\text{RS},k} + n_{\ell,k}$ is the total additive noise, in which $n_{\ell,k}$ denotes the additive white Gaussian noise at MS ℓ with variance σ_{MS}^2 . Similarly, we assume that $\mathbb{E}\{\|G_k x_k\|_2^2\} = P_{\text{RS}}$, where P_{RS} denotes the RS maximum transmit power per subcarrier. By expanding (2), we have

$$\boldsymbol{y}_{\ell,k} = \boldsymbol{y}_{\ell,k}^{\mathrm{DS}} + \boldsymbol{y}_{\ell,k}^{\mathrm{SI}} + \boldsymbol{W}_{\ell,k}^{H} \tilde{\boldsymbol{n}}_{\ell,k}, \qquad (3)$$



where $\boldsymbol{y}_{\ell,k}^{\text{SI}} = \boldsymbol{W}_{\ell,k}^{H} \bar{\boldsymbol{H}}_{\ell,\ell,k} \boldsymbol{F}_{\ell,k} \boldsymbol{s}_{\ell,k}$ is the self-interference (SI) and $\boldsymbol{y}_{\ell,k}^{\text{DS}} = \boldsymbol{W}_{\ell,k}^{H} \bar{\boldsymbol{H}}_{\ell,\ell',k} \boldsymbol{F}_{\ell',k} \boldsymbol{s}_{\ell',k}, \ell \neq \ell'$, is the desired-signal (DS), in which we have defined the effective channels

$$\bar{\boldsymbol{H}}_{\ell,\ell',k} = \boldsymbol{H}_{\ell,k}^T \boldsymbol{G}_k \boldsymbol{H}_{\ell',k}, \ \ell,\ell' \in \{1,2\}.$$
(4)

Note that the SI appears in (3) since each MS receives back its own signal from the RS. However, under ideal conditions, as elaborated in [8, Section III-B], the SI term can be subtracted completely by MSs. Consequently, (3) reduces to

$$\boldsymbol{z}_{\ell,k} = \boldsymbol{y}_{\ell,k} - \boldsymbol{y}_{\ell,k}^{\mathrm{SI}} = \boldsymbol{y}_{\ell,k}^{\mathrm{DS}} + \boldsymbol{W}_{\ell,k}^{H} \tilde{\boldsymbol{n}}_{\ell,k}.$$
 (5)

From the above, the SE of MS ℓ on the *k*th subcarrier can be expressed as

$$\mathbf{SE}_{\ell,k} = \frac{1}{2} \log_2 \left| \left(\boldsymbol{I}_{N_s} + \left(\boldsymbol{W}_{\ell,k}^H \boldsymbol{\Phi}_{\ell,k} \boldsymbol{W}_{\ell,k} \right)^{-1} \boldsymbol{R}_{\ell,k} \right|, \quad (6)$$

where $\Phi_{\ell,k} = \mathbb{E}\{\tilde{n}_{\ell,k}\tilde{n}_{\ell,k}^{H}\} = \sigma_{\mathrm{RS}}^{2}H_{\ell,k}^{T}G_{k}G_{k}^{H}H_{\ell,k}^{*} + \sigma_{\mathrm{MS}}^{2}I_{M_{\mathrm{MS}}},$ $R_{\ell,k} = \mathbb{E}\{(\boldsymbol{y}_{\ell,k}^{\mathrm{DS}})(\boldsymbol{y}_{\ell,k}^{\mathrm{DS}})^{H}\} = \boldsymbol{W}_{\ell,k}^{H}\bar{H}_{\ell,\ell',k}F_{\ell',k}F_{\ell',k}^{H}\bar{H}_{\ell,\ell',k}^{H}\boldsymbol{W}_{\ell,k}$ are the effective noise and the desired signal covariance matrices, respectively.

Our goal is to design the beamforming matrices to maximize the total SE of the system, which can be expressed as

$$\max_{\{F_{\ell,k}, W_{\ell,k}, G_k, \forall k\}} \sum_{\ell=1}^{2} \sum_{k=0}^{K-1} SE_{\ell,k}$$

s.t. $\|F_{\ell,k}\|_{\mathrm{F}}^2 = P_{\mathrm{MS}}, \|G_k x_k\|_2^2 = P_{\mathrm{RS}}.$ (7)

Note that (7) is a non-convex optimization function due to the joint optimization of the beamforming matrices at the MSs and the amplification matrix at the RS. To obtain a solution, we propose in the following a sub-optimal non-iterative approach by decoupling the optimization procedure between the beamforming matrices of the MSs and the RS amplification matrix. By noting that for any given G_k on subcarrier k, the system model in (5) reduces to two independent pointto-point MIMO communication systems, one for each MS. It implies that the optimal precoding (resp. decoding) matrix, on every subcarrier, is given by the dominant N_s right (resp. left) singular vectors of the respective effective channel given by (4), with the power allocation given by the waterfilling method [17]. Specifically, by dropping the subcarrier index k, to ease the notation, we assume that MS ℓ first calculates the noise whitening filter $Q_{\ell} = \Phi_{\ell}^{-1/2}$ so that $Q_\ell \Phi_\ell Q_\ell = I_{M_{\mathrm{MS}}}$. Let $\dot{H}_{\ell,\ell'} = Q_\ell \bar{H}_{\ell,\ell'}$ be the whitened effective channel between MS ℓ and MS ℓ' , with $\ell \neq \ell'$. Then, given the SVD of $H_{\ell,\ell'} = U_{\ell,\ell'} \text{diag}\{\lambda_{\ell,\ell'}\} V^H_{\ell,\ell'}$, the precoding matrix of MS ℓ' is given as $F_{\ell'} = [\widetilde{V}_{\ell,\ell'}]_{[1:N_s]}$, while the

¹Notation: The transpose, the Hermitian transpose, the Moore-Penrose pseudo-inverse, the Kronecker product, and the Khatri-Rao product are denoted by $\mathbf{X}^T, \mathbf{X}^H, \mathbf{X}^+, \otimes$, and \diamond , respectively. The Frobenius norm is denoted by $\|\cdot\|_{\mathrm{F}}$. The operator diag $\{x\}$ returns a diagonal matrix with \boldsymbol{x} as the diagonal arguments, $\operatorname{vec}\{X\}$ stacks the columns of matrix \boldsymbol{X} into a vector, and unvec $\{x\}$ is the inverse of the $\operatorname{vec}\{X\}$ operator. The following property is also used: $\operatorname{vec}\{A\operatorname{diag}(b)C\} = (C^T \diamond A)b$.

decoding matrix of the MS ℓ is given as $W_{\ell} = [\widetilde{U}_{\ell,\ell'}]_{[1:N_s]}$. Accordingly, (6) can be simplified as

$$SE_{\ell} = \sum_{i=1}^{N_s} \log_2(1 + ([\widetilde{\lambda}_{\ell,\ell'}]_{[i]})^2 \cdot p_{\ell,\ell',i}),$$
(8)

where $p_{\ell,\ell',i}$ is the power of the *i*th data stream given by $p_{\ell,\ell',i} = \max \{1/\mu_{\ell,\ell'} - 1/[\widetilde{\lambda}_{\ell,\ell'}]_{[i]}, 0\}$, where $\mu_{\ell,\ell'}$ is the real-valued water-level found using, e.g., the bisection method so that $\sum_{i=1}^{N_s} p_{\ell,\ell',i} = P_{\rm MS}$. From the above, the problem that we address in this paper is the design of $G_k, \forall k$.

3. FULLY-DIGITAL-BASED DESIGN

In this section, we drop the subcarrier index k, since the proposed fully-digital design is decoupled between the K subcarriers. From (8), it is clear that the RS amplification matrix G, of any subcarrier, should be designed so that the singular values of the whitened effective channels of both MSs, i.e., $\tilde{\lambda}_{1,2}$ and $\tilde{\lambda}_{2,1}$, are maximized. To achieve this goal, the authors in [8] proposed a heuristic closed-form approach, termed ANOMAX, to design G as

$$\boldsymbol{G} = \max_{\boldsymbol{G}} \left(\left\| \bar{\boldsymbol{H}}_{1,2} \right\|_{F}^{2} + \left\| \bar{\boldsymbol{H}}_{2,1} \right\|_{F}^{2} \right).$$
(9)

After some algebraic manipulations, (9) is rewritten as [8]

$$\boldsymbol{g} = \max_{\boldsymbol{g}} \|\boldsymbol{K}\boldsymbol{g}\|_2^2, \quad \text{s.t.} \quad \|\boldsymbol{g}\|_2 = 1, \quad (10)$$

where $K = [(H_2 \otimes H_1), (H_1 \otimes H_2)]^T$ and $g = \text{vec}\{G\}$. Using the SVD of $K = U_K \text{diag}(\lambda_K) V_K^H$, the optimal solution of (10) is given as $g_{\text{ANOMAX}} = [V_K]_{[:,1]}$. However, it was observed in [8] that the unfolded matrix, i.e., $G_{\text{ANOMAX}} = \text{unvec}\{g_{\text{ANOMAX}}\}$ often exhibits a low-rank structure. To make it applicable for multi-stream communications, the authors extended their framework in [9] by proposing RR-ANOMAX. In RR-ANOMAX, the rank of G_{ANOMAX} is increased by adjusting its singular values while preserving its subspaces. In the following, we build on those results and propose a method that further enhances the rank of G_{ANOMAX} , termed hereafter enhanced RR-ANOMAX (ERR-ANOMAX), by exploiting the structure of problem (10).

In contrast to ANOMAX and RR-ANOMAX, in ERR-ANOMAX, the g vector is constructed by taking the contributions of the first R vectors in V_K as

$$\boldsymbol{g}_{\text{E-ANOMAX}} = [\boldsymbol{V}_{\boldsymbol{K}}]_{[:,1]} + \dots + [\boldsymbol{V}_{\boldsymbol{K}}]_{[:,R]}, \quad (11)$$

where *R* is a design parameter that we investigate numerically in Section 5. Then, for the unfolded matrix $G_{\text{E-ANOMAX}} =$ unvec{ $g_{\text{E-ANOMAX}}$ }, the SVD is given as $G_{\text{E-ANOMAX}} =$ $U_G \text{diag}(\lambda_G) V_G^H$. This implies that $g_{\text{E-ANOMAX}} = (V_G^* \diamond U_G) \lambda_G$. Here, we propose to redesign λ_G while keeping both U_G and V_G fixed, to enhance the rank of $G_{\text{E-ANOMAX}}$. Specifically, by substituting $g_{\text{E-ANOMAX}}$ into (10), we have

$$\lambda_{\boldsymbol{G}}^{*} = \max_{\boldsymbol{\lambda}_{\boldsymbol{G}}} \|\tilde{\boldsymbol{K}}\boldsymbol{\lambda}_{\boldsymbol{G}}\|_{2}^{2} \quad \text{s.t.} \quad \|\boldsymbol{\lambda}_{\boldsymbol{G}}\|_{2} = 1, \quad (12)$$

where $\tilde{K} = K(V_G^* \diamond U_G)$. In contrast to (10), the optimization variable of (12) is a real-valued vector. Therefore, we propose to design λ_G using a water-filling like method [17]. Specifically, given the SVD of $\tilde{K} = U_{\tilde{K}} \operatorname{diag}(\lambda_{\tilde{K}}) V_{\tilde{K}}^H$, the *j*th entry of λ_G is updated as $[\lambda_G^*]_{[j]} = \max \{1/\mu - 1/[\lambda_{\tilde{K}}]_{[j]}, 0\}$, where μ is the real-valued water-level found using, e.g., the bisection method so that $\sum_{j=1} [\lambda_G^*]_{[j]} = 1$. Finally, we calculate $G_{\text{ERR-ANOMAX}} = U_G \operatorname{diag}(\lambda_G^*) V_G^H$, which is then normalized so that $||G_{\text{ERR-ANOMAX}} x||_2^2 = P_{\text{RS}}$.

4. HAD-BASED DESIGN

As mentioned in [18], the fully-digital system is impractical in mm-wave massive MIMO systems due to the large number of RF chains. Therefore, we consider a HAD AF structure with $N_{\rm RS} < M_{\rm RS}$ RF chains, so that the amplification matrix G_k has a structure given as $G_k \stackrel{\text{def}}{=} A_{\rm T} B_k A_{\rm R}^T$, where B_k is the $N_{\rm RS} \times N_{\rm RS}$ baseband beamforming matrix for the kth subcarrier, while $A_{\rm T}$ and $A_{\rm R}$ are the common $M_{\rm RS} \times N_{\rm RS}$ transmit and received analog beamforming matrices, respectively, implemented using phase-shifting networks. Therefore, we have that $|[A_{\rm T}]_{[i,j]}| = 1, \forall i, j$, and $|[A_{\rm R}]_{[i,j]}| = 1, \forall i, j$. Considering the HAD amplification matrix given above, the maximization of the total SE of the system in (7) is more challenging due to the constant modulus constraints of the analog beamforming matrices. Therefore, we propose a heuristic solution to (7), similarly to [19], as

$$\min_{\boldsymbol{A}_{\mathrm{T}},\boldsymbol{A}_{\mathrm{R}},\boldsymbol{B}_{k},\forall k} \sum_{k=0}^{K-1} \left\| \boldsymbol{G}_{\mathrm{FD},k} - \boldsymbol{A}_{\mathrm{T}} \boldsymbol{B}_{k} \boldsymbol{A}_{\mathrm{R}}^{T} \right\|_{F}^{2} \\
\left| [\boldsymbol{A}_{\mathrm{R}}]_{[i,j]} \right| = 1, \forall i, j, \left| [\boldsymbol{A}_{\mathrm{T}}]_{[i,j]} \right| = 1, \forall i, j,$$
(13)

where $G_{\text{FD},k}$ is a given unconstrained fully-digital RS amplification matrix on the *k*th subcarrier. For the known $G_{\text{FD},k}, \forall k$, we form a 3-way tensor \mathcal{G}_{FD} by concatenating $G_{\text{FD},k}, \forall k$, along the third mode, as

$$\boldsymbol{\mathcal{G}}_{\mathrm{FD}} = [\boldsymbol{G}_{\mathrm{FD},0} \sqcup_3 \cdots \sqcup_3 \boldsymbol{G}_{\mathrm{FD},K-1}] \in \mathbb{C}^{M_{\mathrm{RS}} \times M_{\mathrm{RS}} \times K}.$$
(14)

Here, we note that the tensor \mathcal{G}_{FD} in (14) admits a Tucker2 decomposition [14–16] given as

$$\boldsymbol{\mathcal{G}}_{\mathrm{FD}} = \boldsymbol{\mathcal{B}} \times_1 \boldsymbol{A}_{\mathrm{T}} \times_2 \boldsymbol{A}_{\mathrm{R}} \times_3 \boldsymbol{I}_K, \qquad (15)$$

where $\mathcal{B} \in \mathbb{C}^{N_{\text{RS}} \times N_{\text{RS}} \times K}$ is the core tensor formed as $\mathcal{B} = [B_0 \sqcup_3 \cdots \sqcup_3 B_{K-1}]$. Utilizing (15), (13) can be rewritten as a constrained Tucker2 decomposition as

$$\min_{\boldsymbol{A}_{\mathrm{T}}, \boldsymbol{A}_{\mathrm{R}}, \boldsymbol{\mathcal{B}}} \| \boldsymbol{\mathcal{G}}_{\mathrm{FD}} - \boldsymbol{\mathcal{B}} \times_{1} \boldsymbol{A}_{\mathrm{T}} \times_{2} \boldsymbol{A}_{\mathrm{R}} \times_{3} \boldsymbol{I}_{K} \|_{\mathrm{F}}^{2}$$

$$|[\boldsymbol{A}_{\mathrm{R}}]_{[i,j]}| = 1, \forall i, j, \text{ and } |[\boldsymbol{A}_{\mathrm{T}}]_{[i,j]}| = 1, \forall i, j.$$

$$(16)$$

HOSVD-based solution: A direct solution to (16) can be obtained from the HOSVD [15] of the tensor \mathcal{G}_{FD} . Specifically, let the HOSVD of \mathcal{G}_{FD} be written as

$$\boldsymbol{\mathcal{G}}_{\mathrm{FD}} = \boldsymbol{\mathcal{S}} \times_1 \boldsymbol{U}_1 \times_2 \boldsymbol{U}_2 \times_3 \boldsymbol{U}_3, \qquad (17)$$



where U_1 , U_2 , and U_3 are the unitary factor matrices, while S is the core tensor. Then, by utilizing the fact that A_T (resp. A_R) spans the same subspace as U_1 (resp. U_2), the analog matrices and the baseband matrix of the *k*th subcarrier can be obtained as $\mathring{A}_T = \Pi([U_1]_{[1:N_{RS}]})$, $\mathring{A}_R = \Pi([U_2]_{[1:N_{RS}]})$, and $\mathring{B}_k = [S]_{[1:N_{RS},1:N_{RS},k]}$, where $\Pi(\cdot)$ is an element-wise projection function defined as $\Pi(u) = u/|u|$. Therefore, the *k*th HAD RS amplification matrix is given as $G_{\text{HOSVD},k} = \mathring{A}_T \mathring{B}_k \mathring{A}_R^T$, which is then normalized so that $||G_{\text{HOSVD},k} x_k||_2^2 = P_{\text{RS}}$.

AltMax-based solution: Another solution to (16) can be obtained using our recently proposed AltMax approach in [5]. Specifically, let $[\mathcal{G}_{\text{FD}}]_{(1)} = \mathbf{A}_{\text{T}}[\mathcal{B}]_{(1)}(\mathbf{I}_{K} \otimes \mathbf{A}_{\text{R}})^{T}$ denote the one-mode unfolding of \mathcal{G}_{FD} , in which $[\mathcal{B}]_{(1)}$ is formed according to the forward cyclical ordering [20]. Then, a solution to \mathbf{A}_{T} can be obtained as

$$\max_{\boldsymbol{A}_{\mathrm{T}}} \|\boldsymbol{A}_{\mathrm{T}}^{H}[\boldsymbol{\mathcal{G}}_{\mathrm{FD}}]_{(1)}\|_{F}^{2} = \max_{\boldsymbol{A}_{\mathrm{T}}} \operatorname{trace}(\boldsymbol{A}_{\mathrm{T}}^{H}\boldsymbol{G}_{(1)}\boldsymbol{A}_{\mathrm{T}})$$
s.t. $|[\boldsymbol{A}_{\mathrm{T}}]_{[i,j]}| = 1, \forall i, j,$

$$(18)$$

where $G_{(1)} = [\mathcal{G}_{FD}]_{(1)}[\mathcal{G}_{FD}]_{(1)}^H$. Our proposed AltMax technique in [5] can be used to solve (18), which updates A_T column-wise until a convergence is reached. Similarly to (18), the A_R matrix can be calculated utilizing the two-mode unfolding $[\mathcal{G}_{FD}]_{(2)} = A_R[\mathcal{B}]_{(2)}(I_K \otimes A_T)^T$.

From the obtained $\dot{A}_{\rm T}$ and $\dot{A}_{\rm R}$, the core tensor can be calculated as $[\dot{B}]_{(3)} = [\mathcal{G}_{\rm FD}]_{(3)}[(\dot{A}_{\rm R} \otimes \dot{A}_{\rm T})^T]^+$, where $[\mathcal{G}_{\rm FD}]_{(3)} = [\mathcal{B}]_{(3)}(A_{\rm R} \otimes A_{\rm T})^T$. Thus, the *k*th HAD RS amplification matrix is given as $G_{\rm AltMax,k} = \dot{A}_{\rm T}\dot{B}_k\dot{A}_{\rm R}^T$, where \dot{B}_k is the *k*th 3-mode slice of $\dot{\mathcal{B}}$. Finally, we normalize $G_{\rm AltMax,k}$ so that $||G_{\rm AltMax,k} \boldsymbol{x}_k||_2^2 = P_{\rm RS}$.

5. SIMULATION RESULTS

Similarly to [5], we assume that each channel matrix is generated using the classical Saleh-Valenzuela model [21], where we fix the number of channel paths L = 6. We define the signal-to-noise ratio as SNR $= \frac{1}{\sigma^2}$, where we assume that $P_{\rm RS} = P_{\rm MS} = 1$ and $\sigma_{\rm RS}^2 = \sigma_{\rm MS}^2 = \sigma^2$. In all the simulation scenarios, we use $M_{\rm RS} = 64$ and $M_1 = M_2 = 4$.

Example 1: The fully-digital case: Here, we compare the performance of ANOMAX [8], RR-ANOMAX [9], and the proposed ERR-ANOMAX assuming that K = 1 and the RS is equipped with a fully-digital beamforming structure.

From Fig. 2(a), we can see that when $N_s = 1$, the three methods achieve the same performance. However, the rank restoration methods, i.e., RR-ANOMAX and ERR-ANOMAX have a significant performance gain in the $N_s > 1$ scenarios when compared to ANOMAX. For $N_s > 1$, ERR-ANOMAX outperforms the RR-ANOMAX of [9], specially for $N_s = 4$. Here, in Fig. 2(a), we have assumed that R = 2 for ERR-ANOMAX. Using computer simulations, as reported in Fig. 2(b), we have observed that setting R = 2 provides the best performance.

Example 2: The HAD case: Here, we compare RR-ANOMAX and the proposed ERR-ANOMAX assuming that the RS is equipped with a HAD beamforming structure. Fig. 3 shows the SE versus the SNR.

From Fig. 3(a), as expected, we can observe that ERR-ANOMAX maintains its advantages over RR-ANOMAX in the HAD beamforming scenarios as well, where the AltMax method is shown to outperform the HOSVD method, agreeing with our results reported in [5]. However, from Fig. 3(b), we can see that when $N_{\rm RS}$ reduces from 8 to 4, the performance of the HAD methods reduces significantly, where both HAD methods seem to have an equal performance. This implies that, for the HAD architectures, the number of RF chains $N_{\rm RS}$ at the RS should be equal or larger than the total number of data streams, i.e., $N_{\rm RS} \geq 2N_s$ to maintain a close performance to that achieved by the fully-digital counterpart. Finally, Fig. 3(b) also shows that when the number of system subcarriers K increases from 32 to 64, the performance of the HAD methods slightly decreases, which is more evident with the HOSVD method and less with the AltMax method.

6. CONCLUSIONS

In this work, we have enhanced and extended the RR-ANOMAX scheme, originally proposed in [9] for singlecarrier FD AF MIMO TWR systems, to multi-carrier HAD AF MIMO-OFDM TWR systems. Specifically, we have proposed the ERR-ANOMAX scheme that outperforms RR-ANOMAX in multi-stream communications. Moreover, we have shown that the HAD amplification matrix design can be formulated as a constrained Tucker2 decomposition, for which two solutions are proposed, an HOSVD-based solution and an AltMax-based solution. Simulation results show that ERR-ANOMAX AltMax outperforms the other methods.

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