

Envelope Level Crossing Rate and Average Fade Duration of Nonisotropic Vehicle-to-Vehicle Ricean Fading Channels

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Abstract—This paper proposes a generic geometry-based stochastic model for nonisotropic scattering vehicle-to-vehicle (V2V) Ricean fading channels. With the proposed model, the level crossing rate (LCR) and average fade duration (AFD) are derived. The resultant expressions are sufficiently general and subsume many well-known existing LCRs and AFDs as special cases. The derived LCR and AFD are further investigated in terms of some important parameters, e.g., the shape of the scattering region (two-ring or ellipse), mean angle, angle spread, and directions of movement of the Tx and Rx (same or opposite direction). More importantly, in this paper, the impact of the vehicular traffic density on the LCR and AFD for nonisotropic scattering V2V Ricean fading channels is investigated for the first time. Excellent agreement is observed between the theoretical LCRs/AFDs and corresponding measured data, thus demonstrating the validity and utility of the proposed model.

Index Terms—Average fade duration (AFD), level crossing rate (LCR), nonisotropic scattering environments, Ricean fading, vehicle-to-vehicle (V2V) channels.

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I. INTRODUCTION

IN MOBILE communications with time-variant fading, e.g., vehicular communications in intelligent transportation systems (ITSs) [1], [2], two important second-order statistics associated with envelope fading are the envelope level crossing rate (LCR) and average fade duration (AFD). The LCR describes how often the envelope crosses a certain threshold, whereas AFD indicates how long the envelope stays below a given threshold. The LCR and AFD characterize various aspects of the dynamic temporal behavior of envelope fluctuations. Therefore, they can be used to investigate the disturbing effects of signal fades and consequently appear in a variety of applications.

In recent years, vehicle-to-vehicle (V2V) communications have received increasing attention and have been considered as an integral part of the next-generation ITSs [4]–[8]. The important benefits of V2V communications in ITSs include its potential in improving road safety, enhancing traffic efficiency, and offering infotainment. Such V2V systems consider that both the transmitter (Tx) and receiver (Rx) are in motion and equipped with low-elevation antennas. To analyze and design a V2V system, it is necessary to have detailed knowledge of the V2V channel and its statistical properties. As mentioned in [9] and [10], in terms of the modeling approach, V2V channel models can be categorized as geometry-based deterministic models, nongeometrical stochastic models, and geometry-based stochastic models (GBSMs) that can be further classified as regular-shaped GBSMs (RS-GBSMs) and irregular-shaped GBSMs. RS-GBSMs assume that all effective scatterers are located on a regular shape [e.g., one/two-ring (TR) or ellipse (EL)] and can often preserve the mathematical tractability. Akki and Haber [11] first proposed an RS-GBSM for narrow-band 2-D isotropic scattering single-input single-output (SISO) V2V Rayleigh fading channels. TR-based RS-GBSMs were studied in [12] and [13] for narrow-band 2-D nonisotropic multiple-input multiple-output (MIMO) V2V channels. The 2-D TR narrow-band model in [12] was further extended to a 3-D two-cylinder narrow-band and two-concentric-cylinder wideband model in [14] and [15], respectively. Recently, new generic nonisotropic MIMO V2V RS-GBSMs have been also proposed for narrow-band [16] and wideband channels [17].

However, all the aforementioned RS-GBSMs focused on the investigation of correlation properties and power

spectral densities. Although the LCR and AFD are of extreme importance for a V2V channel due to its greater dynamics, only a few papers [18]–[21] investigated the LCR and AFD for V2V channels. In [18], the LCR and AFD for isotropic scattering V2V Rayleigh fading channels in 2-D large spatial scale (LSS) scenarios (i.e., the Tx–Rx distance is larger than 1 km) were studied. In [19] and [20], the authors investigated the LCR and AFD for nonisotropic scattering V2V Ricean fading channels in 3-D LSS and moderate spatial scale (MSS) scenarios (i.e., the Tx–Rx distance ranges from 300 m to 1 km) and also gave the corresponding experimental validation. However, none of the two has studied the LCR and AFD in small spatial scale (SSS) scenarios (i.e., the Tx–Rx distance is smaller than 300 m), which are currently receiving more and more attention due to the increasing applications of dedicated short-range communications to V2V communications. Moreover, due to the unique feature of V2V communication environments, the impact of the vehicular traffic density (VTD) on channel characteristics in MSS and SSS scenarios cannot be neglected [10], unlike in LSS scenarios. More recently, in [21], we have performed some preliminary work on the impact of VTD on LCR and AFD. However, the work in [21] simply assumed that the moving scatterers and static scatterers have the same Doppler frequency. This unrealistic assumption underestimates the temporal behavior of envelope fluctuations, and thus, the derived LCR and AFD in [21] are inaccurate.

To fill the aforementioned gaps, this paper proposes a new RS-GBSM and derives the corresponding LCR and AFD. The main contributions and novelties of this paper are as follows.

- 1) We propose a new V2V RS-GBSM that corrects the unrealistic assumption used in [21] by properly capturing different Doppler frequencies for moving scatterers and static scatterers. The newly developed V2V RS-GBSM is suitable for a wide variety of scenarios, i.e., LSS, MSS, and SSS scenarios, thus enabling the analysis of the VTD impact on channel characteristics. This model employs a combined TR model and EL model, where the received signal is constructed as a sum of the line-of-sight (LoS), single-, and double-bounced rays at different envelope levels.
- 2) Based on the developed RS-GBSM, we derive the LCR and AFD for nonisotropic scattering V2V Ricean fading channels. Our analysis shows several limitations in the derivation and investigation of the LCR and AFD in [19], revealing some easily neglected but important issues. We stress that the derived LCR and AFD subsume several existing LCRs and AFDs as special cases, e.g., those in [18] and [22]–[25].
- 3) Based on the derived LCR and AFD, we study in more detail the behavior of the LCR and AFD in terms of some important parameters and, for the first time, practically investigate the impact of VTD on LCR and AFD. In addition, comparisons of the obtained theoretical LCR and AFD with measurement data in [26] are presented. Excellent agreement between these corroborates the validity and utility of the proposed model.

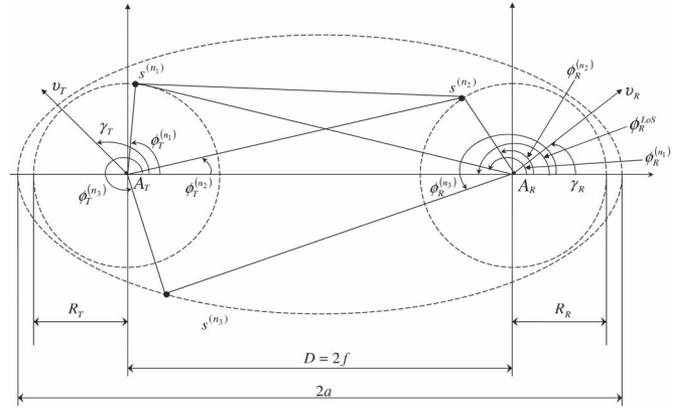


Fig. 1. Generic channel model combining a TR model and an EL model with LoS components and single- and double-bounced rays for a SISO V2V channel.

The remainder of this paper is organized as follows. Section II presents a new generic RS-GBSM for 2-D nonisotropic scattering narrow-band SISO V2V Ricean fading channels. In Section III, based on the proposed model, we derive the corresponding LCR and AFD. Numerical results and analysis, as well as the comparison of the analytical LCR and AFD with the measurement data, are presented in Section IV. Finally, conclusions are drawn in Section V.

II. NEW GENERIC RS-GBSM FOR NONISOTROPIC V2V RICEAN FADING CHANNELS

Let us now consider a narrow-band single-user SISO V2V communication system. Both the Tx and Rx are equipped with low-elevation antennas. The propagation scenario is characterized by nonisotropic scattering with a LoS component between the Tx and Rx. Fig. 1 illustrates the geometry of the SISO V2V model, which is the combination of a LoS component, a single-bounce (SB) and double-bounce (DB) TR model, and an SB EL model. The TR model defines two rings of effective scatterers, i.e., one around the Tx and the other around the Rx. Note that effective scatterers are used to represent the effect of many scatterers with similar spatial location. Suppose there are N_1 effective scatterers around the Tx lying on a ring of radius R_T and the n_1 th ($n_1 = 1, \dots, N_1$) effective scatterer is denoted by $s^{(n_1)}$. Similarly, assume there are N_2 effective scatterers around the Rx lying on a ring of radius R_R and the n_2 th ($n_2 = 1, \dots, N_2$) effective scatterer is denoted by $s^{(n_2)}$. For the EL model, N_3 effective scatterers lie on an EL with the Tx and Rx located at the foci. The semimajor axis of the EL and the n_3 th ($n_3 = 1, \dots, N_3$) effective scatterer are denoted by a and $s^{(n_3)}$, respectively. The distance between the Tx and Rx is $D = 2f$ with f denoting the half length of the distance between the two focal points of the EL. To make the proposed model able to investigate the impact of the VTD on channel statistics, the TR model is used to present moving scatterers, e.g., moving cars around the Tx and Rx, and the EL model is applied to present static scatterers, e.g., static roadside environment. Unlike the previous RS-GBSM in [21], the proposed model actually considers the movement of the moving scatterers by defining different effective velocities of the Tx/Rx with respect to moving scatterers and static

scatterers. Therefore, the effective velocities of the Tx and Rx with respect to static scatterers are denoted as v_T and v_R in directions determined by the directions of motion γ_T and γ_R , respectively. Whereas, the effective velocities of the Tx and Rx with respect to moving scatterers are denoted as v'_T and v'_R in directions determined by the directions of motion γ'_T and γ'_R , respectively. For clarity purposes, only the effective velocities of the Tx and Rx with regard to static scatterers are shown in Fig. 1. Symbol $\phi_{R_q}^{\text{LoS}}$ denotes the angle of arrival (AoA) of a LoS path. The AoA of the wave traveling from the effective scatterer $s^{(n_i)}$ ($i \in \{1, 2, 3\}$) toward the Rx is denoted by $\phi_R^{(n_i)}$. The angle of departure (AoD) of the wave that impinges on the effective scatterer $s^{(n_i)}$ is designated by $\phi_T^{(n_i)}$.

From the above model, the received complex fading envelope is the superposition of the LoS component and diffuse components, consisting of single- and double-bounced rays, and can be expressed as

$$\begin{aligned} h(t) &= h^{\text{LoS}}(t) + h^{\text{DIF}}(t) \\ &= h^{\text{LoS}}(t) + h^{\text{SB}}(t) + h^{\text{DB}}(t) \end{aligned} \quad (1)$$

where $h^{\text{LoS}}(t)$, $h^{\text{SB}}(t)$, and $h^{\text{DB}}(t)$ are expressed in (2a)–(2b), shown at the bottom of the page. $I = 3$; $f_{T_{\max}} = v_T/\lambda$ and $f_{R_{\max}} = v_R/\lambda$ are the maximum Doppler frequencies of the Tx and Rx, respectively, with respect to static scatterers; $f'_{T_{\max}} = v'_T/\lambda$ and $f'_{R_{\max}} = v'_R/\lambda$ are the maximum Doppler frequencies of the Tx and Rx, respectively, with respect to moving scatterers; $f_{T_{\max}}^1 = f_{T_{\max}}^2 = f_{T_{\max}}^3 = f_{T_{\max}}$; $f_{R_{\max}}^1 = f_{R_{\max}}^2 = f_{R_{\max}}^3 = f_{R_{\max}}$; and $f_{R_{\max}}^3 = f_{R_{\max}}$. Symbol K designates the Ricean factor, and Ω denotes the total power. Parameters η_{SB_i} and η_{DB} specify how much the single- and double-bounced rays contribute to the total scattered power $\Omega/(K+1)$, respectively. Note that these energy-related parameters satisfy $\sum_{i=1}^I \eta_{\text{SB}_i} + \eta_{\text{DB}} = 1$. Phases ψ_{n_i} and ψ_{n_i, n_j} are independent and identically distributed random variables with uniform distributions over $[-\pi, \pi)$, and λ is the carrier wavelength. Note that AoD $\phi_T^{(n_i)}$ and AoA $\phi_R^{(n_i)}$ are independent random vari-

ables for double-bounced rays, whereas they are interdependent for single-bounced rays.

By using the results in [16], we can express the general relationships between the AoD and AoA for the SB TR model as $\phi_R^{(n_1)} = \arcsin[R_T \sin \phi_T^{(n_1)} / (R_T^2 + D^2 - 2R_T D \cos \phi_T^{(n_1)})^{1/2}]$ and $\phi_T^{(n_2)} = \arcsin[R_R \sin \phi_R^{(n_2)} / (R_R^2 + D^2 + 2R_R D \cos \phi_R^{(n_2)})^{1/2}]$ and for the EL model as $\phi_T^{(n_3)} = \arcsin[b^2 \sin \phi_R^{(n_3)} / (a^2 + f^2 + 2af \cos \phi_R^{(n_3)})]$, where b denotes the semiminor axis of the EL and equality qq holds. The above exact relationships are sufficiently general and thus suitable for a wide variety of scenarios. For LSS and MSS scenarios, since assumption $D \gg \max\{R_T, R_R\}$ holds, the aforementioned exact relationships of $\phi_R^{(n_1)} \leftrightarrow \phi_T^{(n_1)}$ and $\phi_R^{(n_2)} \leftrightarrow \phi_T^{(n_2)}$ can reduce to the following widely used approximate relationships [19]: $\phi_R^{(n_1)} \approx \pi - \Delta_T \sin \phi_T^{(n_1)}$ and $\phi_T^{(n_2)} \approx \Delta_R \sin \phi_R^{(n_2)}$, respectively, with $\Delta_T \approx R_T/D$ and $\Delta_R \approx R_R/D$.

Since we assume that the numbers of effective scatterers N_i tend to be infinite, the discrete AoA $\phi_R^{(n_i)}$ and AoD $\phi_T^{(n_i)}$ can be replaced by continuous random variables $\phi_R^{\text{SB}_i}$ and $\phi_T^{\text{SB}_i}$, respectively. In this paper, the von Mises probability density function (PDF) [27] is used to describe AoA/AoD. The von Mises PDF is defined as $f(\phi) \triangleq \exp[k \cos(\phi - \mu)] / [2\pi I_0(k)]$, where $\phi \in [-\pi, \pi)$, $I_0(\cdot)$ is the zeroth-order modified Bessel function of the first kind, $\mu \in [-\pi, \pi)$ accounts for the mean value of the angle ϕ , and k ($k \geq 0$) is a real-valued parameter that controls the angle spread of the angle ϕ . For $k = 0$ (isotropic scattering), the von Mises PDF reduces to the uniform distribution, whereas for $k > 0$ (nonisotropic scattering), the von Mises PDF approximates different distributions based on the values of k [27]. In this paper, for the angles of interest, e.g., the AoD $\phi_T^{\text{SB}_1}$ for the one ring around the Tx, the AoA $\phi_R^{\text{SB}_2}$ for the one ring around the Rx, and the AoA $\phi_R^{\text{SB}_3}$ for the EL, we will replace the relevant parameters μ and k of the von Mises PDF in (6) as μ_T^{TR} and k_T^{TR} , μ_R^{TR} and k_R^{TR} , and μ_R^{EL} and k_R^{EL} , respectively.

Based on the same approach on how to adjust the important model parameters (i.e., distance D , power-related parameters

$$h^{\text{LoS}}(t) = \sqrt{\frac{K\Omega}{K+1}} e^{j2\pi f_{T_{\max}} t \cos(\pi - \phi_R^{\text{LoS}} + \gamma_T)} e^{2\pi f_{R_{\max}} t \cos(\phi_R^{\text{LoS}} - \gamma_R)} \quad (2a)$$

$$\begin{aligned} h^{\text{SB}}(t) &= \sum_{i=1}^I h^{\text{SB}_i}(t) \\ &= \sum_{i=1}^I \sqrt{\frac{\eta_{\text{SB}_i} \Omega}{K+1}} \lim_{N_i \rightarrow \infty} \sum_{n_i=1}^{N_i} \frac{1}{\sqrt{N_i}} e^{j\psi_{n_i}} e^{j[2\pi f_{T_{\max}}^i t \cos(\phi_T^{(n_i)} - \gamma_T^i) + 2\pi f_{R_{\max}}^i t \cos(\phi_R^{(n_i)} - \gamma_R^i)]} \end{aligned} \quad (2b)$$

$$h^{\text{DB}}(t) = \sqrt{\frac{\eta_{\text{DB}} \Omega}{K+1}} \lim_{N_1, N_2 \rightarrow \infty} \sum_{n_1, n_2=1}^{N_1, N_2} \frac{1}{\sqrt{N_1 N_2}} e^{j\psi_{n_1, n_2}} e^{j[2\pi f_{T_{\max}}' t \cos(\phi_T^{(n_1)} - \gamma_T') + 2\pi f_{R_{\max}}' t \cos(\phi_R^{(n_2)} - \gamma_R')]} \quad (2c)$$

η_{SB_1} and η_{DB} , and Ricean factor K) as in [16], the proposed model is suitable for a wide variety of scenarios, i.e., LSS ($D \geq 1000$ m), MSS ($300 < D < 1000$ m), and SSS scenarios ($D \leq 300$ m). It is worth mentioning that the assumption $D \gg \max\{R_T, R_R\}$ widely used in LSS and MSS scenarios cannot be applied to SSS scenarios since distance D is relatively small. As mentioned in [16], for a low VTD environment, the value of K is large and the power-related parameters fulfill $\eta_{\text{SB}_3} > \max\{\eta_{\text{SB}_1}, \eta_{\text{SB}_2}\} > \eta_{\text{DB}}$, whereas for a high VTD environment, we have a relatively small K and $\eta_{\text{DB}} > \max\{\eta_{\text{SB}_1}, \eta_{\text{SB}_2}, \eta_{\text{SB}_3}\}$.

III. ENVELOPE LCR AND AFD FOR V2V CHANNELS

In this section, based on the proposed RS-GBSM in (1) and (2a)–(2c), we will derive the LCR and AFD for a nonisotropic scattering environment. LCR $L_\xi(r_l)$ is by definition the average number of crossings per second that the signal envelope $\xi(t) = |h(t)|$ crosses a specified level r_l with positive/negative slope. Using the traditional PDF-based method [28], we derive the general expression of the LCR for V2V Ricean fading channels as

$$\begin{aligned} L_\xi(r_l) &= \frac{2r_l}{\pi^{3/2}} \sqrt{\frac{B(K+1)}{b_0}} e^{-K-(K+1)r_l^2} \\ &\quad \times \int_0^{\pi/2} \cosh\left(2\sqrt{K(K+1)}r_l \cos\theta\right) \\ &\quad \times \left[e^{-\left(\frac{\zeta \sin\theta}{\sqrt{2B}}\right)^2} + \sqrt{\frac{\pi}{2B}} \zeta \sin\theta \cdot \operatorname{erf}\left(\frac{\zeta \sin\theta}{\sqrt{2B}}\right) \right] d\theta \end{aligned} \quad (3)$$

where $\cosh(\cdot)$ is the hyperbolic cosine, $\operatorname{erf}(\cdot)$ denotes the error function, $B = b_2 - b_1^2/b_0$, $\zeta = \sqrt{K\Omega}/(K+1)$, and $\zeta = E + b_1/b_0$ with $E = 2\pi f_{T_{\max}} \cos(\pi - \phi_R^{\text{LoS}} + \gamma_T) + 2\pi f_{R_{\max}} \cos(\phi_R^{\text{LoS}} - \gamma_R)$. Finally, the key parameters b_m ($m = 0, 1, 2$) are defined as $b_m = (d^m \rho_{h^{\text{DIF}}}(\tau)/2j^m d\tau^m)|_{\tau=0}$ with $\rho_{h^{\text{DIF}}}(\tau) = \mathbf{E}[h^{\text{DIF}}(t)h^{\text{DIF}*}(t-\tau)]/\Omega$, where $j^2 = -1$, $\rho_{h^{\text{DIF}}}(\tau)$ is the time autocorrelation function (ACF) of the diffuse component $h^{\text{DIF}}(t)$ of the complex channel fading envelope, $(\cdot)^*$ denotes the complex conjugate operation, and $\mathbf{E}[\cdot]$ designates the statistical expectation operator.

Before we derive the key parameters b_m ($m = 0, 1, 2$) of the LCR in (3), let us first clarify the relationship of different LCR expressions for Ricean fading channels, i.e., (3) in this paper, [19, eq. (6)] or [20, eq. (43)], and [22, eq. (2.99)]. These expressions were given separately in different papers and should be used carefully for different propagation environments. It is obvious that (3) is a general expression and can reduce to [19, eq. (6)] and [20, eq. (43)] by setting $E = 0$. If we further assume that $b_1 = 0$ in (3) (it follows that $\zeta = 0$), we can obtain the closed-form LCR expression [22, eq. (2.99)]. We can therefore conclude that, for a nonisotropic scattering environment ($b_1 \neq 0$) with a time-dependent LoS component ($E \neq 0$), we

can only choose (3) as the LCR expression. Whereas, for a nonisotropic scattering environment with a time-independent LoS component ($E = 0$), either (3) here with $E = 0$ or [19, eq. (6)] and [20, eq. (43)] can be used. However, in [19] and [20], the authors have misused (6) and (43), respectively, as the expressions to study the LCR for a nonisotropic scattering environment but with a time-dependent LoS component. The LCR expression in [22, eq. (2.99)] is suitable only for an isotropic scattering environment ($b_1 = 0$) with a time-independent LoS component.

A. Derivation of b_m for a Wide Variety of Scenarios

Based on the presented model in Section II, we now derive the key parameters b_m . Substituting (1), (2b), and (2c) into the expression of b_m and setting $m = 0$, we can obtain parameter b_0 as

$$b_0 = b_0^{\text{SB}_1} + b_0^{\text{SB}_2} + b_0^{\text{SB}_3} + b_0^{\text{DB}} = \frac{1}{2(K+1)} \quad (4)$$

where $b_0^{\text{SB}_1} = \eta_{\text{SB}_1}/(2(K+1))$, $b_0^{\text{SB}_2} = \eta_{\text{SB}_2}/(2(K+1))$, $b_0^{\text{SB}_3} = \eta_{\text{SB}_3}/(2(K+1))$, and $b_0^{\text{DB}} = \eta_{\text{DB}}/(2(K+1))$. Note that (4) corrects the expression of b_0 in [19, eq. (10)], where $b_0 = (1/K+1)$. Similarly, we can express parameters b_1 and b_2 as

$$b_m = b_m^{\text{SB}_1} + b_m^{\text{SB}_2} + b_m^{\text{SB}_3} + b_m^{\text{DB}}, \quad m = 1, 2. \quad (5)$$

Considering the von Mises PDFs for the TR model, we can express parameters $b_m^{\text{SB}_{1(2)}}$ ($m = 1, 2$) as

$$\begin{aligned} b_1^{\text{SB}_{1(2)}} &= b_0^{\text{SB}_{1(2)}} \int_{-\pi}^{\pi} \frac{e^{k_{T(R)}^{\text{TR}} \cos(\phi_{T(R)}^{\text{SB}_{1(2)}} - \mu_{T(R)}^{\text{TR}})}}{I_0(k_{T(R)}^{\text{TR}})} \\ &\quad \times \left[f_{T_{\max}} \cos(\phi_T^{\text{SB}_{1(2)}} - \gamma_T) \right. \\ &\quad \left. + f_{R_{\max}} \cos(\phi_R^{\text{SB}_{1(2)}} - \gamma_R) \right] d\phi_{T(R)}^{\text{SB}_{1(2)}} \end{aligned} \quad (6a)$$

$$\begin{aligned} b_2^{\text{SB}_{1(2)}} &= b_0^{\text{SB}_{1(2)}} \int_{-\pi}^{\pi} \frac{2\pi e^{k_{T(R)}^{\text{TR}} \cos(\phi_{T(R)}^{\text{SB}_{1(2)}} - \mu_{T(R)}^{\text{TR}})}}{I_0(k_{T(R)}^{\text{TR}})} \\ &\quad \times \left[f_{T_{\max}} \cos(\phi_T^{\text{SB}_{1(2)}} - \gamma_T) \right. \\ &\quad \left. + f_{R_{\max}} \cos(\phi_R^{\text{SB}_{1(2)}} - \gamma_R) \right]^2 d\phi_{T(R)}^{\text{SB}_{1(2)}}. \end{aligned} \quad (6b)$$

Based on the general relationship between the AoA and AoD for the SB TR model, the parameters $\phi_R^{\text{SB}_1}$ and $\phi_T^{\text{SB}_2}$ in (6a) and (6b) can be expressed by $\phi_T^{\text{SB}_1}$ and $\phi_R^{\text{SB}_2}$, respectively. Similarly, considering the von Mises PDF for the EL model, we can express parameters $b_m^{\text{SB}_3}$ ($m = 1, 2$) as

$$\begin{aligned} b_1^{\text{SB}_3} &= b_0^{\text{SB}_3} \int_{-\pi}^{\pi} \frac{e^{k_R^{\text{ER}} \cos(\phi_R^{\text{SB}_3} - \mu_R^{\text{ER}})}}{I_0(k_R^{\text{ER}})} \\ &\quad \times \left[f_{T_{\max}} \cos(\phi_T^{\text{SB}_3} - \gamma_T) \right. \end{aligned}$$

$$\begin{aligned}
& + f_{R_{\max}} \cos(\phi_R^{\text{SB}_3} - \gamma_R) \Big] d\phi_R^{\text{SB}_3} \quad (7a) \\
b_2^{\text{SB}_3} = & b_0^{\text{SB}_3} \int_{-\pi}^{\pi} \frac{2\pi e^{k_R^{\text{ER}} \cos(\phi_R^{\text{SB}_3} - \mu_R^{\text{ER}})}}{I_0(k_R^{\text{ER}})} \\
& \times \left[f_{T_{\max}} \cos(\phi_T^{\text{SB}_3} - \gamma_T) \right. \\
& \left. + f_{R_{\max}} \cos(\phi_R^{\text{SB}_3} - \gamma_R) \right]^2 d\phi_R^{\text{SB}_3}. \quad (7b)
\end{aligned}$$

According to the general relationship between the AoA and AoD for the EL model, the parameter $\phi_T^{\text{SB}_3}$ in (7a) and (7b) can be expressed as a function of $\phi_R^{\text{SB}_3}$. Considering the von Mises PDF for the TR model and applying the following equalities $\int_{-\pi}^{\pi} e^{a \sin c + b \cos c} dc = 2\pi I_0(\sqrt{a^2 + b^2})$, $dI_V(z)/dz = [I_{V-1}(z) + I_{V+1}(z)]/2$, and $zI_{V-1}(z) - zI_{V+1}(z) = (V+1)I_V(z)$ [29], where $I_V(\cdot)$ is the V th-order modified Bessel function of the first kind, we can get the following closed-form expressions of parameters b_m^{DB} ($m = 1, 2$):

$$\begin{aligned}
b_1^{\text{DB}} = & b_0^{\text{DB}} \frac{2\pi f_{T_{\max}} \cos(\gamma_T - \mu_T^{\text{TR}}) I_1(k_T^{\text{TR}})}{I_0(k_T^{\text{TR}})} \\
& + b_0^{\text{DB}} \frac{2\pi f_{R_{\max}} \cos(\gamma_R - \mu_R^{\text{TR}}) I_1(k_R^{\text{TR}})}{I_0(k_R^{\text{TR}})} \quad (8a)
\end{aligned}$$

$$\begin{aligned}
b_2^{\text{DB}} = & b_0^{\text{DB}} 4\pi^2 f_{T_{\max}}^2 \frac{1 + \cos(2(\gamma_T - \mu_T^{\text{TR}})) I_2(k_T^{\text{TR}})}{2I_0(k_T^{\text{TR}})} \\
& + b_0^{\text{DB}} 4\pi^2 f_{R_{\max}}^2 \frac{1 + \cos(2(\gamma_R - \mu_R^{\text{TR}})) I_2(k_R^{\text{TR}})}{2I_0(k_R^{\text{TR}})} \\
& + b_0^{\text{DB}} 8\pi^2 f_{T_{\max}} f_{R_{\max}} \cos(\gamma_T - \mu_T^{\text{TR}}) \\
& \times \cos(\gamma_R - \mu_R^{\text{TR}}) \frac{I_1(k_T^{\text{TR}}) I_1(k_R^{\text{TR}})}{I_0(k_T^{\text{TR}}) I_0(k_R^{\text{TR}})}. \quad (8b)
\end{aligned}$$

Since the derivations of (8a) and (8b) are similar, only a brief outline for the derivation of (8b) is given in Appendix A. Numerical integration methods are needed to evaluate the integrals in (6a)–(7b).

B. Derivation of b_m for LSS and MSS Scenarios

For LSS and MSS scenarios, the widely used assumption $D \gg \max\{R_T, R_R\}$ can be used in the derivation of b_m . This results in the closed-form solution of the integrals in (6a) and (6b), whereas the expressions of other parameters b_m remain unchanged. According to the expressions of $\phi_R^{(n_1)}$ and $\phi_T^{(n_2)}$ and using approximate relations $\sin \chi \approx \chi$ and $\cos \chi \approx 1$, when χ is small, the parameters $b_m^{\text{SB}_{1(2)}}$ ($m = 1, 2$) in (6a) and (6b) can be further simplified as

$$\begin{aligned}
b_m^{\text{SB}_1} = & b_0^{\text{SB}_1} \int_{-\pi}^{\pi} \frac{(2\pi)^{m-1} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})}}{I_0(k_T^{\text{TR}})} \\
& \times \left[f_{R_{\max}} \left(\Delta_T \sin \phi_T^{\text{SB}_1} \sin \gamma_R - \cos \gamma_R \right) \right.
\end{aligned}$$

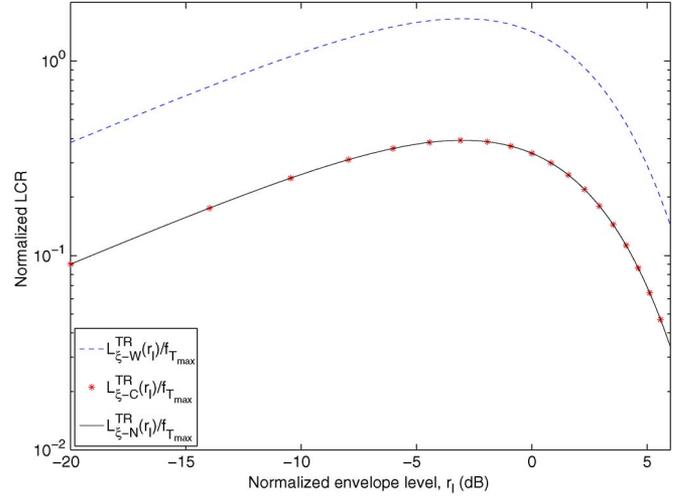


Fig. 2. Comparison of the LCRs $L_{\xi-W}^{\text{TR}}(r_l)$, $L_{\xi-C}^{\text{TR}}(r_l)$, and $L_{\xi-N}^{\text{TR}}(r_l)$.

$$+ f_{T_{\max}} \cos(\phi_T^{\text{SB}_1} - \gamma_T) \Big]^m d\phi_T^{\text{SB}_1} \quad (9a)$$

$$\begin{aligned}
b_m^{\text{SB}_2} = & b_0^{\text{SB}_2} \int_{-\pi}^{\pi} \frac{(2\pi)^{m-1} e^{k_R^{\text{TR}} \cos(\phi_R^{\text{SB}_2} - \mu_R^{\text{TR}})}}{I_0(k_R^{\text{TR}})} \\
& \times \left[f_{T_{\max}} \left(\Delta_R \sin \phi_R^{\text{SB}_2} \sin \gamma_T + \cos \gamma_T \right) \right. \\
& \left. + f_{R_{\max}} \cos(\phi_R^{\text{SB}_2} - \gamma_R) \right]^m d\phi_R^{\text{SB}_2}. \quad (9b)
\end{aligned}$$

The integrals in (9a) and (9b) can be further simplified, and thus, the closed-form expressions of parameters $b_m^{\text{SB}_{1(2)}}$ can be obtained as (10a) and (10b), shown at the bottom of the next page. In Appendix B, we only provide a brief outline for the derivation of (10b) since the derivations of (10a) and (10b) are similar. Note that the expressions of parameters b_m in (6a)–(8b) make the LCR expression in (3) suitable for a wider variety of scenarios, whereas the expressions in (10a) and (10b) limit the application of (3) to only LSS and MSS scenarios. The parameters $b_m^{\text{SB}_{1(2)}}$ for 3-D narrow-band and wideband M2M channels were derived in [19] and [20], respectively. The expressions of $b_m^{\text{SB}_{1(2)}}$ in [20] can reduce to the ones in [19] by setting $R_{t(r)1} = R_{t(r)2}$. If we further assume elevation-related parameters $\beta_{T(R)} = \Delta_H = 0$ in the closed-form expressions of parameters $b_m^{\text{SB}_{1(2)}}$ in [19, eqs. (19) and (21)], the resulting parameters $b_m^{\text{SB}_{1(2)}}$ for a 2-D LSS or MSS scenario can be expressed as (11a) and (11b), shown at the next page below (10a) and (10b). It is obvious that the closed-form expressions for the same parameters $b_m^{\text{SB}_{1(2)}}$ in (10a)–(11b) are different. To determine which closed-form expressions of $b_m^{\text{SB}_{1(2)}}$ are correct, in Fig. 2, we compare the LCRs having the same expression (3) but with different expressions of parameters $b_m^{\text{SB}_{1(2)}}$: 1) $L_{\xi-C}^{\text{TR}}(r_l)$ having $b_m^{\text{SB}_{1(2)}}$ calculated by (10a) and (10b); 2) $L_{\xi-W}^{\text{TR}}(r_l)$ having $b_m^{\text{SB}_{1(2)}}$ in (11a) and (11b); and 3) $L_{\xi-N}^{\text{TR}}(r_l)$ having the numerically computed $b_m^{\text{SB}_{1(2)}}$ in (9a) and (9b). The parameters used in Fig. 2 are $f_{T_{\max}} = f_{R_{\max}} = 500$ Hz, $K = 0$, $\Delta_T = \Delta_R = 0.01$, $\mu_T^{\text{TR}} = 31.2^\circ$, $k_T^{\text{TR}} = 18.2$, $\mu_R^{\text{TR}} = 216.3^\circ$,

and $k_R^{\text{TR}} = 10.6$. Fig. 2 shows excellent agreement between $L_{\xi-C}^{\text{TR}}(r_l)$ and $L_{\xi-N}^{\text{TR}}(r_l)$, demonstrating the correctness of our derivations (10a) and (10b).

It is worth emphasizing that the LCR $L_{\xi-C}^{\text{TR}}(r_l)$, which is based on the closed-form expressions of parameters $b_n^{\text{SB}_{1(2)}}$

in (10a) and (10b), is obtained by applying the widely used assumption $D \gg \max\{R_T, R_R\}$ in LSS and MSS scenarios. To fulfill this assumption, the values of parameters Δ_T and Δ_R should be chosen carefully due to the relationships $\Delta_T \approx R_T/D$ and $\Delta_R \approx R_R/D$ (in general, the smaller, the better).

$$b_1^{\text{SB}_{1(2)}} = b_0^{\text{SB}_{1(2)}} \left\{ 2\pi \left[f_{T(R)\text{max}} \cos \left(\gamma_{T(R)} - \mu_{T(R)}^{\text{TR}} \right) + f_{R(T)\text{max}} \Delta_{T(R)} \sin \mu_{T(R)}^{\text{TR}} \sin \gamma_{R(T)} \right] \right. \\ \left. \times \frac{I_1 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \mp 2\pi f_{R(T)\text{max}} \cos \gamma_{R(T)} \right\} \quad (10a)$$

$$b_2^{\text{SB}_{1(2)}} = b_0^{\text{SB}_{1(2)}} \left\{ 2\pi^2 \left(2f_{R(T)\text{max}}^2 \cos^2 \gamma_{R(T)} + f_{T(R)\text{max}}^2 + f_{R(T)\text{max}}^2 \Delta_{T(R)}^2 \sin^2 \gamma_{R(T)} + 2f_{T\text{max}} f_{R\text{max}} \Delta_{T(R)} \sin \gamma_T \sin \gamma_R \right) \right. \\ \mp 4\pi^2 \left[2f_{T\text{max}} f_{R\text{max}} \cos \gamma_{R(T)} \cos \left(\gamma_{T(R)} - \mu_{T(R)}^{\text{TR}} \right) + f_{R(T)\text{max}}^2 \Delta_{T(R)} \sin(2\gamma_{R(T)}) \sin \mu_{T(R)}^{\text{TR}} \right] \frac{I_1 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \\ \left. + 2\pi^2 \left[f_{T(R)\text{max}}^2 \cos \left(2 \left(\gamma_{T(R)} - \mu_{T(R)}^{\text{TR}} \right) \right) - f_{R(T)\text{max}}^2 \Delta_{T(R)}^2 \sin^2 \gamma_{R(T)} \cos \left(2\mu_{T(R)}^{\text{TR}} \right) \right. \right. \\ \left. \left. - 2f_{T\text{max}} f_{R\text{max}} \Delta_{T(R)} \sin \gamma_{R(T)} \sin \left(\gamma_{T(R)} - 2\mu_{T(R)}^{\text{TR}} \right) \right] \frac{I_2 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \right\}. \quad (10b)$$

$$b_1^{\text{SB}_{1(2)}} = b_0^{\text{SB}_{1(2)}} \left\{ 2\pi \left[f_{T(R)\text{max}} \cos \left(\gamma_{T(R)} - \mu_{T(R)}^{\text{TR}} \right) - f_{R(T)\text{max}} \Delta_{T(R)} \sin \mu_{T(R)}^{\text{TR}} \sin \gamma_{R(T)} \right] \right. \\ \left. \times \frac{I_1 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \pm 2\pi f_{R(T)\text{max}} \cos \gamma_{R(T)} \right\} \quad (11a)$$

$$b_2^{\text{SB}_{1(2)}} = b_0^{\text{SB}_{1(2)}} \left\{ 2\pi^2 \left(2f_{R(T)\text{max}}^2 \cos^2 \gamma_{R(T)} + \frac{2}{\pi^2} f_{T\text{max}} f_{R\text{max}} \Delta_{T(R)} \sin \gamma_{R(T)} \cos \gamma_T \mp 4f_{T\text{max}} \times f_{R\text{max}} \cos \gamma_{R(T)} \right) \right. \\ \left. + 2\pi^2 \left(f_{T(R)\text{max}}^2 + f_{R(T)\text{max}}^2 \Delta_{T(R)}^2 \sin^2 \gamma_{R(T)} \right) \frac{1}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \right. \\ \left. \pm 4\pi^2 f_{R(T)\text{max}}^2 \Delta_{T(R)} \sin(2\gamma_{R(T)}) \sin \mu_{T(R)}^{\text{TR}} \frac{I_1 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \right. \\ \left. - 2\pi^2 \left[f_{T(R)\text{max}}^2 \cos \left(2 \left(\gamma_{T(R)} - \mu_{T(R)}^{\text{TR}} \right) \right) + f_{R(T)\text{max}}^2 \Delta_{T(R)}^2 \sin^2 \gamma_{R(T)} \cos \left(2\mu_{T(R)}^{\text{TR}} \right) \right. \right. \\ \left. \left. + \frac{2}{\pi^2} f_{T\text{max}} f_{R\text{max}} \Delta_{T(R)} \sin \gamma_{R(T)} \cos \left(2\mu_{T(R)}^{\text{TR}} - \gamma_{T(R)} \right) \right] \frac{I_2 \left(k_{T(R)}^{\text{TR}} \right)}{I_0 \left(k_{T(R)}^{\text{TR}} \right)} \right\}. \quad (11b)$$

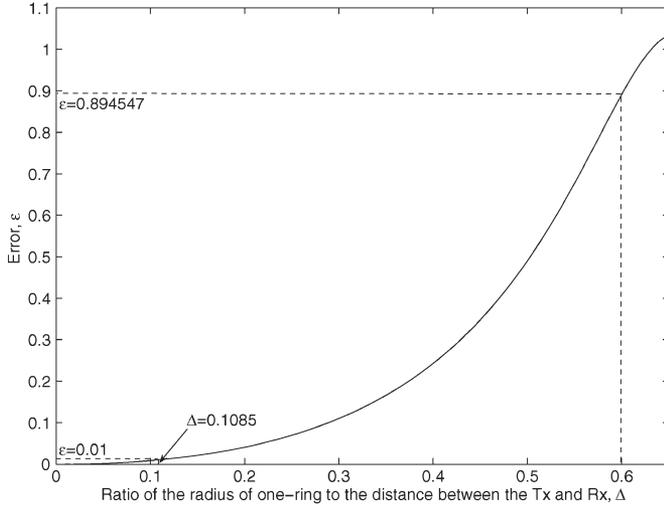


Fig. 3. Error ε between the LCRs $L_{\xi-G}^{\text{TR}}(r_l)$ and $L_{\xi-C}^{\text{TR}}(r_l)$.

However, the values of parameters Δ_T and Δ_R are chosen comparatively large ($\Delta_T = \Delta_R = 0.6$) in [19]. This raises several questions, such as whether $\Delta_T = \Delta_R = 0.6$ violates assumption $D \gg \max\{R_T, R_R\}$; if so, how inaccurate the LCR $L_{\xi-C}^{\text{TR}}(r_l)$ is; and whether this inaccuracy is acceptable. To address the above questions, we define an error function to measure the error between the LCR $L_{\xi-G}^{\text{TR}}(r_l)$, having the expression of (3) with the general expressions of parameters $b_m^{\text{SB}_1(2)}$ in (6a) and (6b), and $L_{\xi-C}^{\text{TR}}(r_l)$ as $\varepsilon = L^{-1} \sum_{l=1}^L |L_{\xi-G}^{\text{TR}}(r_l) - L_{\xi-C}^{\text{TR}}(r_l)| / |L_{\xi-G}^{\text{TR}}(r_l)|$, where L is the total number of the investigated specified level r_l . Fig. 3 illustrates the error ε versus the parameter Δ ($\Delta_T = \Delta_R = \Delta$) by using the same parameters as in Fig. 2. In Fig. 3, the investigated levels r_l were obtained by taking $L = 200$ equal-distance samples between -20 and 5 dB. As expected, it is shown that the inaccuracy of $L_{\xi-C}^{\text{TR}}(r_l)$ increases with the increase in parameter Δ . From Fig. 3, it is obvious that at $\Delta = 0.6$, we have very high error $\varepsilon = 0.894547$. This demonstrates that the chosen parameters $\Delta_T = \Delta_R = 0.6$ in [19] may result in extremely inaccurate $L_{\xi-C}^{\text{TR}}(r_l)$. Therefore, it is desirable to propose a criterion on how to choose parameters Δ_T and Δ_R to guarantee the acceptable accuracy of $L_{\xi-C}^{\text{TR}}(r_l)$. In this paper, we assume that the accuracy of $L_{\xi-C}^{\text{TR}}(r_l)$ is acceptable if the error $\varepsilon \leq 0.01$. In such a case, the LCR $L_{\xi-C}^{\text{TR}}(r_l)$ can be applied under the condition that $\Delta_T = \Delta_R \leq 0.1085$. In other words, when $\Delta_T = \Delta_R > 0.1085$, the LCR $L_{\xi-G}^{\text{TR}}(r_l)$ can only be used instead of $L_{\xi-C}^{\text{TR}}(r_l)$.

AFD $T_{\xi-}(r_l)$ is the average time over which the signal envelope $\xi(t)$ remains below a certain level r_l . In general, the AFD $T_{\xi-}(r_l)$ for Ricean fading channels is defined by [22]

$$T_{\xi-}(r_l) = \frac{P_{\xi-}(r_l)}{L_{\xi}(r_l)} = \frac{1 - Q\left(\sqrt{2K}, \sqrt{2(K+1)}r_l\right)}{L_{\xi}(r_l)} \quad (12)$$

where $P_{\xi-}(r_l)$ indicates a cumulative distribution function of $\xi(t)$ with $Q(\cdot, \cdot)$ denoting the generalized Marcum Q function.

Many existing LCRs and AFDs are special cases of the nonisotropic V2V LCR and AFD in (3) and (12), respectively. The simplest case is Clarke's LCR $\sqrt{2\pi}f_{R_{\max}}r_l \exp(-r_l^2)$ and

AFD $(\exp(r_l^2) - 1)/(\sqrt{2\pi}f_{R_{\max}}r_l)$ [22], which can be obtained from (3) and (12), respectively, by setting $K = 0$ (non-LoS condition), $k_R^{\text{TR}} = 0$ (isotropic scattering around Rx), and $f_{T_{\max}} = k_T^{\text{TR}} = \eta_{\text{SB}_1} = \eta_{\text{SB}_3} = \eta_{\text{DB}} = 0$ (fixed Tx, no scattering around Tx). Expressions for other LCRs and AFDs based on the isotropic one-ring model only around the Rx, e.g., those in [23] and [24], can be similarly obtained. The LCR and AFD based on the nonisotropic TR model with single-bounced rays [25] are obtained from (3) and (12), respectively, by setting $K = f_{T_{\max}} = \eta_{\text{SB}_3} = \eta_{\text{DB}} = 0$. Finally, the LCR and AFD for isotropic V2V Rayleigh channels [18] are obtained from (3) and (12), respectively, by setting $K = k_T^{\text{TR}} = k_R^{\text{TR}} = \eta_{\text{SB}_1} = \eta_{\text{SB}_2} = \eta_{\text{SB}_3} = 0$.

IV. NUMERICAL RESULTS AND ANALYSIS

In this section, based on the derived LCR and AFD in Section III, these two second-order statistics of the nonisotropic V2V Ricean fading channel are numerically analyzed in more detail in terms of some important parameters, e.g., the scattering assumption (single- or double-bounced rays), shape of the scattering region (TR or EL), mean angle, angle spread, and directions of movement of the Tx and Rx [same direction (SD) or opposite direction (OD)]. In addition, we compare the theoretical results of the LCR and AFD with the measured data in [26]. Without loss of generality, we assume that the effective directions of motion of the Tx/Rx with respect to moving scatterers and static scatterers are the same, i.e., $\gamma_T = \gamma'_T$ and $\gamma_R = \gamma'_R$. The following parameters are used for our numerical analysis: $f_c = 5.2$ GHz, $f_{T_{\max}} = f_{R_{\max}} = 500$ Hz, $f'_{T_{\max}} = f'_{R_{\max}} = 560$ Hz, $a = 200$ m, $D = 300$ m, and $R_T = R_R = 40$ m.

Fig. 4 presents the impact of different models (e.g., SB TR model, DB TR model, and SB EL model) and directions of movement of the Tx and Rx (SD or OD) on the LCR and AFD in a nonisotropic scattering scenario, respectively. Results show that the behavior of the LCRs and AFDs for different models is different. We can also observe that the impact of the directions of movement of the Tx and Rx on LCR and AFD exists for single-bounced rays, whereas it disappears for double-bounced rays due to the independent relationship between the AoA and AoD.

Fig. 5 illustrates the LCRs and AFDs of the SB and DB TR models and SB EL model for different nonisotropic scattering scenarios, respectively. It is obvious that the LCR and AFD significantly vary according to the changes of angle spread (related to the values of k_T^{TR} , k_R^{TR} , and k_R^{EL}) and mean angle (related to the values of μ_T^{TR} , μ_R^{TR} , and μ_R^{EL}). Therefore, these two parameters play an important role in the behavior of the LCR and AFD for a nonisotropic scattering scenario.

Fig. 6(a) and (b) depicts the theoretical LCRs and AFDs for different VTDs (low or high) in V2V Ricean fading channels when the Tx and Rx move in the SD, respectively. For further comparison, the measured results taken from [26] are also plotted in Fig. 6(a) and (b). In [26], the measurement campaigns were performed at a carrier frequency of 5.2 GHz on a highway with a low VTD in Germany, and the maximum Doppler frequencies were $f_{T_{\max}} = f_{R_{\max}} = 500$ Hz. The distance between

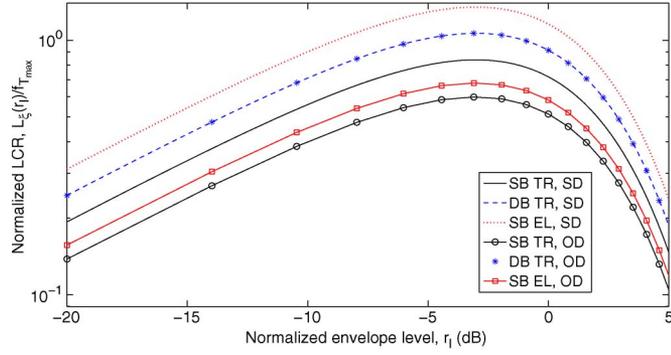


Fig. 4. LCRs of the SB TR model, DB TR model, and SB EL model for different directions of movement of the Tx and Rx in a V2V nonisotropic scenario ($k_T^{TR} = k_R^{TR} = k_R^{EL} = 3$, $\mu_T^{TR} = 45^\circ$, and $\mu_R^{TR} = \mu_R^{EL} = 145^\circ$). SD: ($\gamma_T = \gamma'_T = \gamma_R = \gamma'_R = 0$); OD: ($\gamma_T = \gamma'_T = 0$ and $\gamma_R = \gamma'_R = \pi$).

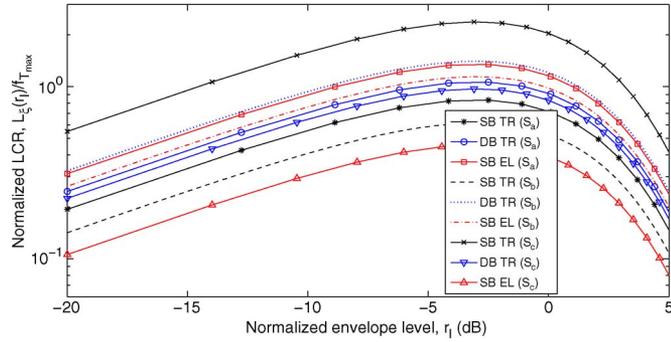
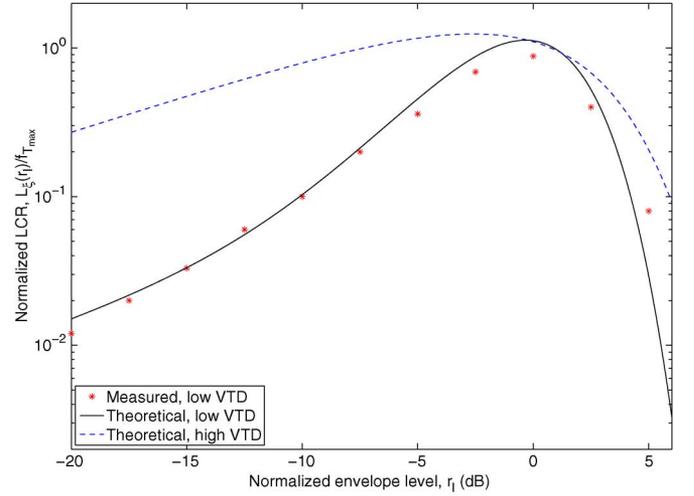
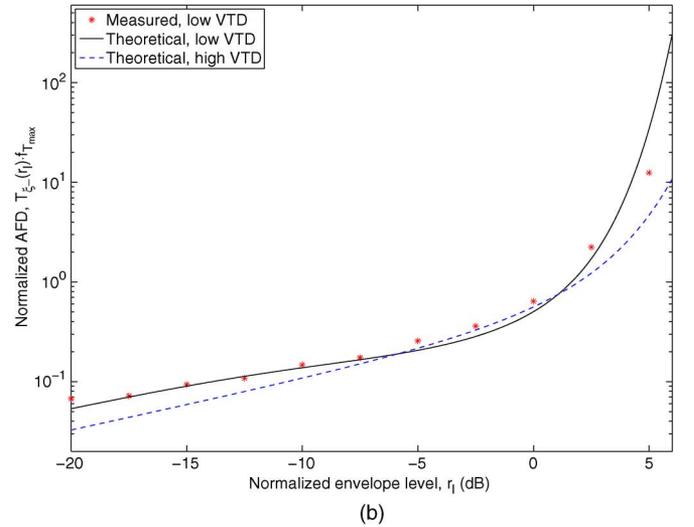


Fig. 5. LCRs of the SB TR model, DB TR model, and SB EL model in V2V channels with the Tx and Rx moving in the same direction ($\gamma_T = \gamma'_T = \gamma_R = \gamma'_R = 0$) for different nonisotropic scenarios. Scenario a (S_a): $k_T^{TR} = k_R^{TR} = k_R^{EL} = 3$, $\mu_T^{TR} = 45^\circ$, and $\mu_R^{TR} = \mu_R^{EL} = 145^\circ$. Scenario b (S_b): $k_T^{TR} = k_R^{TR} = k_R^{EL} = 6$, $\mu_T^{TR} = 45^\circ$, and $\mu_R^{TR} = \mu_R^{EL} = 145^\circ$. Scenario c (S_c): $k_T^{TR} = k_R^{TR} = k_R^{EL} = 3$, $\mu_T^{TR} = 120^\circ$, $\mu_R^{TR} = 45^\circ$, and $\mu_R^{EL} = 0^\circ$.

the Tx and Rx was approximately $D = 300$ m, and the directions of movement of the Tx and Rx were $\gamma_T = \gamma_R = 0$ (SD). Both Tx and Rx were equipped with one omnidirectional antenna, i.e., SISO case. Based on the measured scenarios in [26], we chose the following environment-related parameters for Fig. 6(a) and (b): $\mu_T^{TR} = 33.2^\circ$, $k_T^{TR} = 18.2$, $\mu_R^{TR} = 148.6^\circ$, $k_R^{TR} = 13.3$, $\mu_R^{ER} = 148.6^\circ$, and $k_R^{ER} = 8.6$. Considering the constraints of the Ricean factor and power-related parameters for a propagation scenario with low VTD as mentioned in Section II, we assume that the Ricean factor is comparatively large and single-bounced rays of the EL model bear more power than SB and double-bounced rays of the TR model. Based on the minimum of the mean squared error between the theoretical LCR/AFD and the measured LCR/AFD reported in [26], we can obtain the following parameters: $K = 4.26$, $\eta_{DB} = 0.08$, $\eta_{SB_1} = 0.12$, $\eta_{SB_2} = 0.18$, and $\eta_{SB_3} = 0.62$. The excellent agreement between the theoretical results and measured data confirms the utility of the proposed model. The theoretical LCR and AFD for high VTD shown in Fig. 6(a) and (b) were obtained via the assumption that the Ricean factor is comparatively small and double-bounced rays bear more energy than single-bounced rays, i.e., $K = 0.56$, $\eta_{DB} = 0.58$, $\eta_{SB_1} = 0.1$, $\eta_{SB_2} = 0.18$, and $\eta_{SB_3} = 0.14$. Unfortunately, to the best of the authors' knowledge, no measurement results are



(a)



(b)

Fig. 6. (a) LCRs and (b) AFDs of the developed V2V channel model with a low or high VTD when the Tx and Rx move in the same direction.

available for studying the impact of high VTD (e.g., traffic jam) on the LCR and AFD. Comparing the theoretical LCRs and AFDs in Fig. 6(a) and (b), respectively, we observe that the VTD significantly affects the LCR and AFD for V2V channels. However, we note that the LCR and AFD around $r_l = 0$ dB are nearly independent of the VTD. This attractive property suggests that the LCR can be used to provide a velocity estimate that is robust to the VTD. Moreover, Fig. 6(a) shows that the fades are shallower when the VTD is lower. We see in Fig. 6(b) that the AFD tends to be larger with lower VTD. This is because with a high VTD, the received power comes mainly from the moving cars around the TX and Rx from all directions, whereas with a low VTD, the received power concentrates on several directions, e.g., the directions of LoS components and/or large stationary scatterers on the roadside environment. The above observations coincide with our intuition that the LCR increases with the increase in the VTD while the AFD increases with the decrease in the VTD. This demonstrates the correctness of the method by taking into account the impact of the VTD in our model, i.e., using a TR model to describe the moving scatterers

around the Tx and Rx and to utilize an EL model to depict the stationary scatterers located on the roadside.

V. CONCLUSION

In this paper, a new generic RS-GBSM that can be used to practically study the impact of the VTD on channel statistics has been proposed for a 2-D nonisotropic scattering narrow-band SISO V2V Ricean fading channel. Based on the proposed model, the LCR and AFD have been derived and further investigated in more detail. Analysis and simulation results have shown that some important parameters, e.g., the scattering assumption, shape of the scattering region, mean angle, angle spread, and directions of movement of the Tx and Rx, can significantly affect the LCR and AFD of V2V channels. More importantly, we have investigated the impact of VTD on LCR and AFD and found that a lower VTD results in a smaller LCR (i.e., the shallower fades) and correspondingly a larger AFD. In addition, we have found that the LCR and AFD around $r_l = 0$ dB are roughly independent of the VTD, indicating that the velocity estimate obtained from the LCR is robust against the VTD. Finally, it has been shown that the theoretical results of the LCR and AFD match the measured data, which validates the utility of the analysis and channel model proposed in this paper in the practical design of V2V communications in ITSs.

APPENDIX A DERIVATION OF (8B)

The starting point for the derivation of (8b) is given by the time ACF of the complex channel fading envelope $h^{\text{DB}}(t)$. Substituting (2c) into the expression of $\rho_{h^{\text{DIF}}}(\tau)$, considering the von Mises PDFs for TR scatterers and using equality $\int_{-\pi}^{\pi} e^{a \sin c + b \cos c} dc = 2\pi I_0(\sqrt{a^2 + b^2})$ [29], we can obtain the closed-form expression of $\rho_{h^{\text{DB}}}(\tau)$ as

$$\rho_{h^{\text{DB}}}(\tau) = \frac{\eta_{\text{DB}}}{K+1} \frac{1}{I_0(k_T^{\text{TR}}) I_0(k_R^{\text{TR}})} \times I_0 \left\{ \sqrt{(A_T^{\text{DB}})^2 + (B_T^{\text{DB}})^2} \right\} I_0 \left\{ \sqrt{(A_R^{\text{DB}})^2 + (B_R^{\text{DB}})^2} \right\} \quad (13)$$

where $A_T^{\text{DB}} = k_T^{\text{TR}} \cos \mu_T^{\text{TR}} + j2\pi\tau f_{T_{\text{max}}} \cos \gamma_T$, $B_T^{\text{DB}} = k_T^{\text{TR}} \sin \mu_T^{\text{TR}} + j2\pi\tau f_{T_{\text{max}}} \sin \gamma_T$, $A_R^{\text{DB}} = k_R^{\text{TR}} \cos \mu_R^{\text{TR}} + j2\pi\tau f_{R_{\text{max}}} \cos \gamma_R$, and $B_R^{\text{DB}} = k_R^{\text{TR}} \sin \mu_R^{\text{TR}} + j2\pi\tau f_{R_{\text{max}}} \sin \gamma_R$. Substituting (13) into the expression of b_m with $m = 2$ and applying trigonometric transformations, product rule for differentiation, and equalities $dI_V(z)/dz = [I_{V-1}(z) + I_{V+1}(z)]/2$ and $zI_{V-1}(z) - zI_{V+1}(z) = (V+1)I_V(z)$ [29], where $I_V(\cdot)$ is the V th-order modified Bessel function of the first kind, we can get the closed-form expression of the parameter b_2^{DB} given in (8b) after extensive manipulations.

APPENDIX B DERIVATION OF (10B)

Note that (10b) includes two formulas regarding parameters b_2^{SB1} and b_2^{SB2} . In this appendix, we only derive parameter b_2^{SB1}

since the derivation of parameter b_2^{SB2} is exactly the same. Different from the derivation of the parameter b_2^{DB} given in Appendix A, we derive parameter b_2^{SB1} directly from its general expression in (9a) with $m = 2$ in (14), shown at the top of the next page. For the above equation, the first term X_1 can be readily obtained as the following closed-form expression based on equality $\int_{-\pi}^{\pi} e^{a \sin c + b \cos c} dc = 2\pi I_0(\sqrt{a^2 + b^2})$ [29]:

$$X_1 = b_0^{\text{SB1}} 4\pi^2 \left(\frac{f_{T_{\text{max}}}^2}{2} + f_{R_{\text{max}}}^2 \cos^2 \gamma_R + \frac{f_{R_{\text{max}}}^2 \Delta_T^2 \sin^2 \gamma_R}{2} + f_{T_{\text{max}}} f_{R_{\text{max}}} \Delta_T \sin \gamma_T \sin \gamma_R \right). \quad (15)$$

The second term X_2 is given as follows:

$$X_2 = \frac{b_0^{\text{SB1}} 4\pi f_{T_{\text{max}}} f_{R_{\text{max}}} \cos \gamma_R}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB1}} - \mu_T^{\text{TR}})} \times \frac{1}{2} \left[e^{j(\phi_T^{\text{SB1}} - \gamma_T)} + e^{-j(\phi_T^{\text{SB1}} - \gamma_T)} \right] d\phi_T^{\text{SB1}} \\ = \frac{b_0^{\text{SB1}} 2\pi f_{T_{\text{max}}} f_{R_{\text{max}}} \cos \gamma_R}{I_0(k_T^{\text{TR}})} \times \left[e^{j(\pi/2 + \mu_T^{\text{TR}} - \gamma_T)} \int_{-\pi/2 + \mu_T^{\text{TR}}}^{3\pi/2 + \mu_T^{\text{TR}}} e^{-j\beta_T + k_T^{\text{TR}} \sin \beta_T} d\beta_T + e^{j(\pi/2 - \mu_T^{\text{TR}} + \gamma_T)} \int_{-\pi/2 - \mu_T^{\text{TR}}}^{3\pi/2 - \mu_T^{\text{TR}}} e^{-j\theta_T + k_T^{\text{TR}} \sin \theta_T} d\theta_T \right] \quad (16)$$

where in the third equality we have used equalities $\phi_T^{\text{SB1}} = \pi/2 - \beta_T + \mu_T^{\text{TR}}$ and $\phi_T^{\text{SB1}} = -\pi/2 + \theta_T + \mu_T^{\text{TR}}$ so that $d\phi_T^{\text{SB1}} = -d\beta_T$ and $d\phi_T^{\text{SB1}} = d\theta_T$ hold, respectively. To solve the definite integrals in the right-hand side of (16), we need to modify the following equality: $\int_{-\pi}^{\pi} e^{-jV\theta + jz \sin \theta} d\theta = 2\pi J_V(z)$ [29], where $J_V(\cdot)$ is the V th-order Bessel function of the first kind. Considering the periodic property of the exponential function in the left-hand side of the above equation (here, its period is 2π) and $J_V(-jz) = (-j)^V I_V(z)$, we can extend the aforementioned equality into a more general expression as $\int_{\alpha_l}^{\alpha_u} e^{-jV\theta + jz \sin \theta} d\theta = 2\pi (-j)^V I_V(z)$, where $|\alpha_u - \alpha_l| = 2\pi$. It follows that (16) becomes the following closed-form expression:

$$X_2 = b_0^{\text{SB1}} 8\pi^2 f_{T_{\text{max}}} f_{R_{\text{max}}} \cos \gamma_R \cos(\gamma_T - \mu_T^{\text{TR}}) \frac{I_1(k_T^{\text{TR}})}{I_0(k_T^{\text{TR}})}. \quad (17)$$

Using the same procedure shown above, the closed-form expressions of other terms X_3 , X_4 , X_5 , and X_6 can be obtained similarly. The substitution of X_1, X_2, \dots, X_6 into (14) gives the final result of b_2^{SB1} , as shown in (10b).

$$\begin{aligned}
b_2^{\text{SB}_1} &= \frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})} \\
&\times \left(\frac{f_{T_{\max}}^2}{2} + \frac{f_{R_{\max}}^2 \Delta_T^2 \sin^2 \gamma_R}{2} + f_{R_{\max}}^2 \cos^2 \gamma_R + f_{T_{\max}} f_{R_{\max}} \Delta_T \sin \gamma_T \times \sin \gamma_R \right) d\phi_T^{\text{SB}_1} \\
&- \left[\frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})} 2f_{T_{\max}} f_{R_{\max}} \cos \gamma_R \cos(\phi_T^{\text{SB}_1} - \gamma_T) d\phi_T^{\text{SB}_1} + \frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \right. \\
&\quad \times \left. \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{2\text{SB}_1} - \mu_T^{\text{TR}})} f_{R_{\max}}^2 \Delta_T \sin(2\gamma_R) \sin \phi_T^{\text{SB}_1} d\phi_T^{\text{SB}_1} \right] \\
&+ \left[\frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})} f_{T_{\max}}^2 \frac{\cos(2(\phi_T^{\text{SB}_1} - \gamma_T))}{2} d\phi_T^{\text{SB}_1} \right. \\
&\quad - \frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})} \frac{f_{R_{\max}}^2 \Delta_T^2 \sin^2 \gamma_R \cos(2\phi_T^{\text{SB}_1})}{2} d\phi_T^{\text{SB}_1} \\
&\quad \left. + \frac{b_0^{\text{SB}_1} 2\pi}{I_0(k_T^{\text{TR}})} \int_{-\pi}^{\pi} e^{k_T^{\text{TR}} \cos(\phi_T^{\text{SB}_1} - \mu_T^{\text{TR}})} f_{T_{\max}} f_{R_{\max}} \Delta_T \sin \gamma_R \sin(\gamma_T - 2\phi_T^{\text{SB}_1}) d\phi_T^{\text{SB}_1} \right] \\
&= X_1 - [X_2 + X_3] + [X_4 - X_5 + X_6]. \tag{14}
\end{aligned}$$

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