

A Non-Stationary Wideband MIMO Channel Model for High-Mobility Intelligent Transportation Systems

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Abstract—The recent development of high-speed trains (HSTs), as a high-mobility intelligent transportation system (ITS), and the growing demands of broadband services for HST users introduce new challenges to wireless communication systems for HSTs. The deployment of mobile relay stations (MRSs) on top of the train carriages is one of the promising solutions for HST wireless systems. For a proper design and evaluation of HST wireless communication systems, we need accurate channel models that can mimic the underlying channel characteristics for different HST scenarios. In this paper, a novel non-stationary geometry-based stochastic model (GBSM) is proposed for wideband multiple-input multiple-output (MIMO) HST channels in rural macro-cell (RMa) scenarios. The corresponding simulation model is then developed with angle parameters calculated by the modified method of equal areas (MMEA). Both channel models can also be used to model non-stationary V2I channels in vehicular communication networks. The system functions and statistical properties of the proposed channel models are investigated based on a theoretical framework that describes non-stationary channels. Numerical and simulation results demonstrate that the proposed channel models have the capability to characterize the non-stationarity of HST channels. The statistical properties of the simulation model, verified by the simulation results, can match those of the proposed theoretical GBSM. An excellent agreement is achieved between the stationary intervals of the proposed simulation model and those of relevant measurement data, demonstrating the utility of the proposed channel models.

Index Terms – High-speed train (HST) channels, vehicle-to-infrastructure (V2I) channels, GBSM, non-stationary MIMO channel models, statistical properties.

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I. INTRODUCTION

Intelligent transportation systems (ITSs) consider all types of communications between vehicles, i.e., vehicle-to-vehicle (V2V), vehicle-to-roadside (V2R) or vehicle-to-infrastructure (V2I), and information and communication technologies for rail, water, and air transport [1], [2]. As a fast and convenient ITS, railways that operate trains with a high speed of more than 300 km/h have attracted more and more attentions recently. With the increase of train speeds, wireless communication systems face various challenges such as fast handover [3], high penetration losses, limited visibility in tunnels, large Doppler, delay, and angular spreads. The widely used Global System for Mobile Communication Railway (GSM-R) can only provide a data rate of up to 200 kbps [4], besides the fact that GSM-R is mainly used for train control rather than providing communications for train passengers. Therefore, GSM-R cannot meet the requirements for future high data rate transmissions. International Union of Railways has recommended that GSM-R has to be replaced by long-term evolution-Railway (LTE-R), which is a broadband railway wireless communication system based on LTE-Advanced (LTE-A) [5]. However, both systems still adopt conventional cellular architecture where mobile stations (MSs) inside trains communicate directly with outdoor base stations (BSs). Such an architecture leads to a spotty coverage and high penetration losses of wireless signals traveling into the carriages of high-speed trains (HSTs) [6]. The received signals at the MS on board will experience fast changing channels resulting in high signaling overhead and high possibility of drop calls and handover failure.

The above problems can be mitigated by deploying other cellular architectures, such as distributed antenna systems (DAS) [7], coordinated multipoint (CoMP) [8], and mobile relay station (MRS) (or Mobile Femtocell) [9]. In this paper, we will only consider using the promising MRS technology, as this has been adopted by IMT-Advanced (IMT-A) [10] and WINNER II [11] systems. This is performed by deploying dedicated MRSs on the surface of the train to extend the coverage of the outdoor BS into train carriages. As a result, the effect of frequent handover will be significantly reduced by performing a group handover with the MRS instead of dealing with the individual handover of each passenger [12]. By considering MRS solution, we will have two channels: an outdoor channel between the BS and MRS and an indoor one between the MRS and MS. Radio channels between the

MRS and MSs in the carriages resemble indoor environments and hence can be modeled using the existing indoor channel models [13]. Here, we will focus on the outdoor channel because of the research challenges due to the high velocity of the MRS. This outdoor channel is very similar to a V2I communication channel.

Demonstrating the feasibility of wireless systems in HST scenarios before implementation is not possible without accurate channel models that are able to mimic key characteristics of HST wireless channels, such as the non-stationarity. Similar to V2V channels [14]–[18], the non-stationarity of the HST channels means that the channel statistics can change rapidly over a short period of time. Several measurement campaigns [19]–[24] for different HST environments (rural macro-cell (RMa), tunnels, viaducts, hilly terrains, and U-shaped) were conducted but they mainly focused on large-scale fading parameters, such as path loss and delay spread, and thus ignored small-scale fading parameters.

Channel models in the literature have also failed to demonstrate different propagation parameters of wireless channels in HST scenarios. Adopting a conventional cellular architecture, the LTE-A system [5] provided a relatively simple single-path channel model that supports two scenarios, i.e., open space and tunnels, but ignores the non-stationarity of HST channels. In [25], the propagation channels between HSTs and fixed BSs were modeled using the ray-tracing method, which incorporates a detailed simulation of the actual physical wave propagation process based on an approximation to Maxwell equations [26]. However, the implementation of ray-tracing models always requires extensive computational resources. In both the RMa scenario in WINNER II [11] and moving networks scenario in IMT-A channel models [10], the train speed can be up to 350 km/h and the MRS technology is employed. Both channel models introduced time evolution concept to explicitly simulate the non-stationarity of channels. However, it has been demonstrated in [27] how the stationary interval, defined as the maximum time duration over which the channel satisfies the wide-sense stationary (WSS) condition, of these two standard channel models is considerably longer than that of real HST channels. For a train speed of 324 km/h, the reported stationary intervals of the standardized models and the measured HST channel were 37.8 ms and 20 ms, respectively [27]. Consequently, the stationary distance of the standardized channel models is equal to 3.4 m, while it is only 1.8 m for the measured HST channel. The statistical characterization of WSS multiple-input multiple-output (MIMO) channels has been investigated extensively in the literature [28]–[30]. In contrast, only few papers [31]–[35] have studied the statistical properties of non-stationary channels.

To fill the above research gaps, it is highly desirable to design accurate channel models that consider the non-stationarity of HST scenarios by taking into account time-varying small-scale fading parameters, like angles of arrival (AoAs) and angles of departure (AoDs). Also, it is essential to establish a theoretical framework that characterizes non-stationary mobile fading channels in terms of their system functions and correlation functions (CFs). The major contributions and novelties of this paper are summarized as follows.

- 1) We study the system functions and CFs of non-stationary channel models and propose a theoretical framework for deriving the corresponding statistical properties.
- 2) By considering the deployment of MRS in HST communication systems, we propose a theoretical geometry-based stochastic model (GBSM) for wideband non-stationary MIMO HST channels in RMa scenarios. The proposed model has time-varying angular parameters and time-varying distance between the transmitter (Tx) and receiver (Rx). Then, we derive and study its time-variant space-time (ST) CF, time-variant space-Doppler (SD) power spectrum density (PSD), and local scattering function (LSF).
- 3) The aforementioned theoretical (reference) model assumes an infinite number of effective scatterers and therefore cannot be used for simulations. Thus, we further develop a corresponding sum-of-sinusoids (SoS) based simulation model for wideband non-stationary MIMO HST channels with reasonable complexity, i.e., a finite number of sinusoids or effective scatterers. The angle parameters of the proposed simulation model are calculated by adopting the modified method of equal areas (MMEA). The relevant statistical properties of the developed simulation model are derived, verified by simulations, and compared with those of the proposed theoretical GBSM. Furthermore, the utility of the proposed simulation model is validated using measurement data.

The rest of this paper is organized as follows. The system functions of non-stationary channel models are presented in Section II. Section III proposes a theoretical non-stationary GBSM for wideband MIMO HST channels in RMa scenarios and studies its statistical properties. In Section IV, the SoS simulation model for wideband MIMO HST channels is proposed and its statistical properties are investigated. Numerical and simulation results are presented and analyzed in Section V. Finally, conclusions are drawn in Section VI.

II. SYSTEM FUNCTIONS AND CFs OF NON-STATIONARY WIDEBAND MIMO CHANNELS

In this section, we will derive the system functions and CFs that describe non-stationary wideband MIMO channels. The received signal experiencing non-stationary wideband mobile channels can be defined as a 3-dimensional (3D) stochastic process in terms of time t , delay τ , and space x , which denotes the location of an antenna element in the antenna array in the Tx/Rx [36]. It can be described by the space-time-variant channel impulse response $h(t, \tau, x)$ [36], [37]. An alternative description of the non-stationary channel in space-time-frequency domain is the space-time-variant transfer function that can be obtained by taking the Fourier transform of $h(t, \tau, x)$ in terms of delay τ , i.e.,

$$L_H(t, f, x) = \int h(t, \tau, x) e^{-j2\pi f\tau} d\tau. \quad (1)$$

Other 3D system functions can be obtained by using Fourier transforms as in [36], [37]. The 6-dimensional (6D) space-time-delay-variant space-time-delay CF can be obtained from

the space-time-variant impulse response as follows:

$$R_h(t, \tau, x; \Delta t, \Delta \tau, \Delta x) = E \{ h(t, \tau, x) \times h^*(t - \Delta t, \tau - \Delta \tau, x - \Delta x) \} \quad (2)$$

where Δt is the time lag (i.e., time difference), $\Delta \tau$ is the delay lag, and Δx is the space lag (i.e., antenna element spacing [36]). Here, $(\cdot)^*$ denotes the complex conjugate operation and $E \{ \cdot \}$ designates the statistical expectation operator. Similarly, we can obtain the space-time-frequency-variant space-time-frequency CF as

$$R_L(t, f, x; \Delta t, \Delta f, \Delta x) = E \{ L_H(t, f, x) \times L_H^*(t - \Delta t, f - \Delta f, x - \Delta x) \} \quad (3)$$

where Δf is the frequency lag. The 6D CFs (2) and (3) are spatial extension of the 4D CFs proposed by Matz [32]. Matz also suggested another channel statistic for non-stationary channels, namely, the LSF $C_H(t, f, \tau, \nu)$, which describes the mean power of the effective scatterers causing delay-Doppler shifts (τ, ν) at time t and frequency f . Here, we extend the 4-dimensional (4D) LSF in [32] to the space and direction domains resulting in the 6D LSF $C_H(t, f, x, \tau, \nu, \Omega)$, which can be obtained as follows:

$$C_H(t, f, x, \tau, \nu, \Omega) = \iiint R_h(t, \tau, x; \Delta t, \Delta \tau, \Delta x) \times e^{-j2\pi(\nu\Delta t + f\Delta\tau + \Omega\Delta x)} d\Delta t d\Delta\tau d\Delta x \quad (4)$$

$$C_H(t, f, x, \tau, \nu, \Omega) = \iiint R_L(t, f, x; \Delta t, \Delta f, \Delta x) \times e^{-j2\pi(\nu\Delta t - \tau\Delta f + \Omega\Delta x)} d\Delta t d\Delta f d\Delta x. \quad (5)$$

Here, Ω is the direction of an antenna element in the antenna array in the Tx/Rx. The above general system functions and CFs of non-stationary channel models can be simplified by applying the following assumptions.

– *Uncorrelated scattering (US)*: US means that different channel taps with different delays are uncorrelated. In [31], Bello showed that US channels are WSS in the frequency domain. Therefore, the 6D space-time-frequency-variant space-time-frequency CF in (3) will no longer depend on frequency f , i.e., it will be reduced to the 5-dimensional (5D) space-time-variant space-time-frequency CF $R_L(t, x; \Delta t, \Delta f, \Delta x)$. It follows that the 6D space-time-delay-variant space-time-delay CF in (2) will be reduced to the 5D space-time-delay-variant space-time CF $R_h(t, \tau, x; \Delta t, \Delta x)$.

– *Antenna stationarity*: Antenna stationarity means that the time, frequency, and antenna statistics, i.e., the correlation between different antenna elements separated by Δx , do not depend on the selected transmit or receive antennas [38]. It follows that the 6D space-time-frequency-variant space-time-frequency CF in (3) will no longer depend on space x , i.e., it will be reduced to the 5D time-frequency-variant space-time-frequency CF $R_L(t, f; \Delta t, \Delta f, \Delta x)$. Also the 6D space-time-delay-variant space-time-delay CF in (2) will be reduced to the 5D time-delay-variant space-time-delay CF $R_h(t, \tau; \Delta t, \Delta \tau, \Delta x)$.

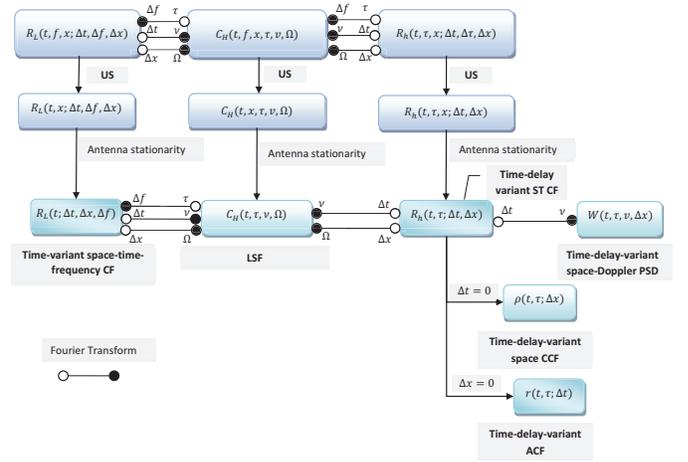


Fig. 1. Relationship of CFs for non-stationary HST channels.

In this paper, we assume that the channel satisfies both the US and antenna stationarity conditions. Antenna stationarity assumption is common for conventional MIMO channels using limited numbers of uniform linear array (ULA) antenna elements. However, this assumption becomes invalid in case of non-ULA antennas [38] and/or large MIMO channels with a large number (tens or even hundreds) of antenna elements [39]. By applying these two assumptions, the CFs will not depend on f , $\Delta \tau$, and x . Therefore, the 6D space-time-delay-variant space-time-delay CF in (2), space-time-frequency-variant space-time-frequency CF in (3), and the LSF in (5) will be reduced to 4-dimensional (4D) time-delay-variant space-time CF $R_h(t, \tau, \Delta t, \Delta x)$, 4D time-variant space-time-frequency CF $R_L(t; \Delta t, \Delta f, \Delta x)$, and 4D LSF $C_H(t, \tau, \nu, \Omega)$, respectively. The time-delay-variant space cross-correlation function (CCF) $\rho(t, \tau; \Delta x)$ and time-delay-variant autocorrelation function (ACF) $r(t, \tau; \Delta t)$ can be obtained from $R_h(t, \tau, \Delta t, \Delta x)$ by imposing $\Delta t=0$ and $\Delta x=0$, respectively. We can also derive the time-delay variant SD PSD $W(t, \tau, \nu, \Delta x)$ by applying the Fourier transform to $R_h(t, \tau, \Delta t, \Delta x)$ in terms of Δt . The relationship between the CFs of non-stationary HST channel models is illustrated in Fig. 1, which serves as a fundamental framework for Sections III and IV. By applying the WSS assumption, the CFs will not depend on t and the 4D CFs will be further reduced to 3D ones as in [36]. Finally, the spatial extension introduced in this section should not be confused with the one presented in [40] where the spatial dimension is related directly to the receiver position.

III. THE NON-STATIONARY WIDEBAND THEORETICAL GBSM

A. Description of the Wideband MIMO Theoretical Model

We adopt the IMT-A cellular network architecture for the HST communication system where MRSs are deployed on the surface of the train. Therefore, the end-to-end communications between the BS and MS will consist of two channels: outdoor channel and indoor one as illustrated in Fig. 2. Here, we

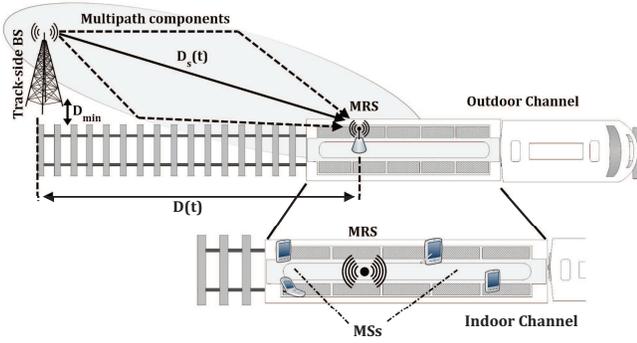


Fig. 2. A HST communication system deploying MRSs.

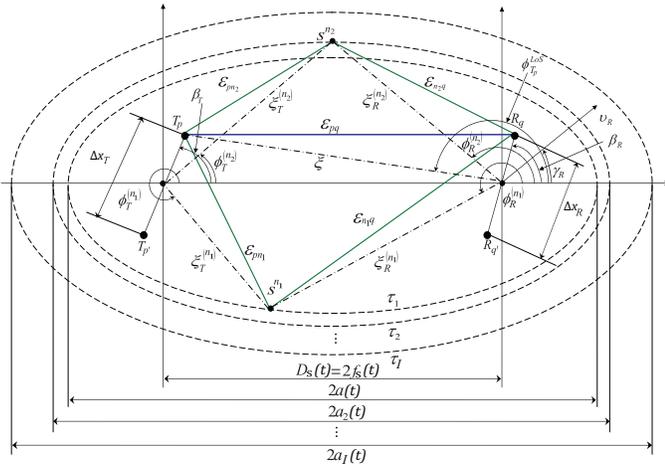


Fig. 3. The GBSM for a wideband MIMO HST channel.

will focus on the outdoor channel between the BS and MRS in RMa scenarios. We consider a MIMO HST system with S transmit and U receive omni-directional antenna elements. The BS is considered to be located on the track-side with the minimum distance between the BS and the track denoted as $D_{\min} = 50$ m [11]. The time-varying distance between the BS and MRS is $D_s(t) = \sqrt{(D_{\min}^2 + D^2(t))}$, where $D(t)$ stands for the projection of $D_s(t)$ on the railway track plane. Fig. 3 illustrates the proposed GBSM, which consists of multiple confocal ellipses with single-bounced rays and the line-of-sight (LoS) component [?]. Geometric elliptical channel models have widely been used to model wideband MIMO channels [41]–[43]. Other GBSMs like one-ring and two-ring models have been mainly used to model narrowband MIMO channels and their extension to wideband channel models [44], [45] is not straightforward. For clarity purposes, we use a 2×2 MIMO channel model in Fig. 3 as an example. The parameters in Fig. 3 are defined in Table I.

Based on the tapped delay line (TDL) structure, the taps are represented by multiple confocal ellipses with the BS and MRS located at the foci. There are N_i effective scatterers on the i th ellipse (i.e., i th tap), where $i=1, 2, \dots, I$ and I is the total number of ellipses or taps. Each effective scatterer is intended to represent the effect of many physical scatterers within the region. The semi-major axis of the i th ellipse

and the n_i th ($n_i = 1, \dots, N_i$) effective scatterer are denoted by $a_i(t)$ and $s^{(n_i)}$, respectively. We denote the time-varying semi-minor axis of the i th ellipse as $b_i(t) = \sqrt{a_i^2(t) - f_s^2(t)}$, where $f_s(t) = D_s(t)/2$ represents a half of the distance between the two foci of ellipses. The tilt angles of the BS and MRS antenna arrays are denoted by β_T and β_R , respectively. The MRS moves with the same speed v_R as the train in the direction determined by the angle of motion γ_R . The AoA of the wave traveling from an effective scatterer $s^{(n_i)}$ to the MRS is denoted by $\phi_R^{(n_i)}(t)$. The AoD of the wave that impinges on the effective scatterer $s^{(n_i)}$ is denoted by $\phi_T^{(n_i)}(t)$, while $\phi_{T_p}^{\text{LoS}}(t)$ denotes the AoA of a LoS path.

Based on the TDL concept, the complex space-time-variant channel impulse response between the p th ($p = 1, \dots, S$) element of the BS, T_p , and the q th ($q = 1, \dots, U$) element of the MRS, R_q , can be expressed as $h(t, \tau, x) = h_{pq}(t, \tau) = \sum_{i=1}^I h_{i,pq}(t) \delta(\tau - \tau_i)$, where $h_{i,pq}(t)$ and τ_i denote the complex space-time-variant tap coefficients and the discrete propagation delay of the i th tap, respectively. Note that the space domain x is implicitly expressed by the subscript pq . From the above GBSM, the complex tap coefficients for the first tap ($i=1$) of the $T_p - R_q$ link is a superposition of the LoS component and single-bounced (SB) components, and can be expressed as $h_{pq}(t, \tau)$ and $h_{i,pq}(t)$ depend only on the antenna spacings of the BS and MRS denoted by Δx_T and Δx_R , respectively.

$$h_{1,pq}(t) = h_{1,pq}^{\text{LoS}}(t) + h_{1,pq}^{\text{SB}}(t) \quad (6)$$

where

$$h_{1,pq}^{\text{LoS}}(t) = \sqrt{\frac{K_{pq}}{K_{pq} + 1}} e^{-j2\pi f_c \tau_{pq}(t)} e^{j2\pi f_{\max} t \cos(\phi_{T_p}^{\text{LoS}}(t) - \gamma_R)} \quad (7a)$$

$$h_{1,pq}^{\text{SB}}(t) = \sqrt{\frac{\Omega_{1,pq}}{K_{pq} + 1}} \lim_{N_1 \rightarrow \infty} \sum_{n_1=1}^{N_1} \frac{1}{\sqrt{N_1}} e^{j(\psi_{n_1} - 2\pi f_c \tau_{pq,n_1}(t))} \times e^{j2\pi f_{\max} t \cos(\phi_R^{(n_1)}(t) - \gamma_R)}. \quad (7b)$$

The complex tap coefficients for other taps ($1 < i \leq I$) of the $T_p - R_q$ link is a sum of SB components only and can be expressed as

$$h_{i,pq}(t) = h_{i,pq}^{\text{SB}}(t) = \sqrt{\Omega_{i,pq}} \lim_{N_i \rightarrow \infty} \sum_{n_i=1}^{N_i} \frac{1}{\sqrt{N_i}} \times e^{j(\psi_{n_i} - 2\pi f_c \tau_{pq,n_i}(t))} e^{j2\pi f_{\max} t \cos(\phi_R^{(n_i)}(t) - \gamma_R)}, 1 < i \leq I. \quad (8)$$

It is worth mentioning that in (7a), (7b), and (8), we have time-varying parameters $\tau_{pq}(t)$, $\phi_{T_p}^{\text{LoS}}(t)$, $\tau_{pq,n_i}(t)$ ($i = 1, \dots, I$), and $\phi_R^{(n_i)}(t)$, which make the underlying GBSM a non-stationary one. If these parameters are not time-varying, then the GBSM can be reduced to a WSS one, as proposed in [?]. In the following, our task is to define or calculate the above time-varying parameters.

In (7a), (7b), and (8), $\Omega_{i,pq}$ designates the mean power for the i th tap, $\tau_{pq}(t) = \varepsilon_{pq}(t)/c$, and $\tau_{pq,n_i}(t) = (\varepsilon_{pn_i}(t) +$

TABLE I
DEFINITION OF PARAMETERS IN FIG. 3.

Parameters	Definition
$D_s(t)$	distance between the BS and MRS
$f_s(t)$	half length of the distance between the two foci of ellipses
$a_i(t), b_i(t)$	semi-major axis and semi-minor axis of the i th ellipse, respectively
v_R, γ_R	MRS speed and angle of motion, respectively
$\Delta x_T, \Delta x_R$	antenna element spacings of the BS and MRS, respectively
β_T, β_R	tilt angles of the BS and MRS antenna arrays in the x-y plane (relative to the x-axis), respectively
$\phi_{T_p}^{\text{LoS}}(t), \phi_R^{(n_i)}(t)$	AoA of the LoS path and AoA of the wave travelling from an effective scatterer $s^{(n_i)}$ to the MRS, respectively
$\phi_T^{(n_i)}(t)$	AoD of the wave that impinges on the effective scatterer $s^{(n_i)}$
$\xi, \xi_T^{(n_i)}(t), \text{ and } \xi_R^{(n_i)}(t)$	distances $d(T_p, \text{MRS}), d(\text{BS}, s^{(n_i)})$, and $d(s^{(n_i)}, \text{MRS})$, respectively
$\varepsilon_{pq}, \varepsilon_{pn_i}, \varepsilon_{niq}$	distances $d(T_p, R_q), d(T_p, s^{(n_i)})$, and $d(s^{(n_i)}, R_q)$, respectively

$\varepsilon_{niq}(t)/c$ are the travel times of the waves through the links $T_p - R_q$ and $T_p - s^{(n_i)} - R_q$, respectively, as shown in Fig. 3. Here, c represents the speed of light and the symbol K_{pq} designates the Ricean factor. The phases ψ_{n_1} and ψ_{n_i} are independent and identically distributed (i.i.d.) random variables with uniform distributions over $[-\pi, \pi)$ and f_{max} is the maximum Doppler shift related to the MRS. From Fig. 3 and based on the law of cosines, we have [43]

$$\varepsilon_{pq}(t) \approx D_s(t) - k_p \Delta x_T \cos \beta_T - k_q \Delta x_R \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R) \quad (9a)$$

$$\varepsilon_{pn_i}(t) \approx \xi_T^{(n_i)}(t) - k_p \Delta x_T \cos(\phi_T^{(n_i)}(t) - \beta_T) \quad (9b)$$

$$\varepsilon_{niq}(t) \approx \xi_R^{(n_i)}(t) - k_q \Delta x_R \cos(\phi_R^{(n_i)}(t) - \beta_R) \quad (9c)$$

where $k_p = (S - 2p + 1)/2$, $k_q = (U - 2q + 1)/2$, and $\xi_R^{(n_i)}(t) = b_i^2(t) / (a_i(t) + f_s(t) \cos \phi_R^{(n_i)}(t))$ with $\xi_T^{(n_i)}(t) = (a_i^2(t) + f_s^2(t) + 2a_i(t)f_s(t) \cos \phi_R^{(n_i)}(t)) / (a_i(t) + f_s(t) \cos \phi_R^{(n_i)}(t))$.

Note that the AoD $\phi_T^{(n_i)}(t)$ and AoA $\phi_R^{(n_i)}(t)$ are interdependent for SB rays. The relationship between the AoD and AoA for multiple confocal ellipses model can be given by [43]

$$\sin \phi_T^{(n_i)}(t) = \frac{b_i^2(t) \sin \phi_R^{(n_i)}(t)}{a_i^2(t) + f_s^2(t) + 2a_i(t)f_s(t) \cos \phi_R^{(n_i)}(t)} \quad (10a)$$

$$\cos \phi_T^{(n_i)}(t) = \frac{2a_i(t)f_s(t) + (a_i^2(t) + f_s^2(t)) \cos \phi_R^{(n_i)}(t)}{a_i^2(t) + f_s^2(t) + 2a_i(t)f_s(t) \cos \phi_R^{(n_i)}(t)} \quad (10b)$$

The time-variant LoS AoA $\phi_{T_p}^{\text{LoS}}(t)$ can be expressed as [5]

$$\phi_{T_p}^{\text{LoS}}(t) = \begin{cases} \phi_{T_p}^{\text{LoS}}(t_0) + \arccos\left(\frac{D_s(t_0) + v_R t \cos \gamma_R}{D_s(t)}\right), & -\pi \leq \gamma_R \leq 0 \\ \phi_{T_p}^{\text{LoS}}(t_0) - \arccos\left(\frac{D_s(t_0) + v_R t \cos \gamma_R}{D_s(t)}\right), & 0 \leq \gamma_R \leq \pi \end{cases} \quad (11)$$

where $\phi_{T_p}^{\text{LoS}}(t_0) = \arcsin\left(\frac{k_p \Delta x_T}{D_s(t_0)} \sin \beta_T\right)$ denotes the initial LoS AoA at time $t = t_0$.

We assume that the numbers of effective scatterers in the theoretical model tend to infinity, i.e., $N_i \rightarrow \infty$. In this case, the discrete angles $\phi_T^{(n_i)}(t)$ and $\phi_R^{(n_i)}(t)$ can be replaced by continuous ones $\phi_T^{(i)}(t)$ and $\phi_R^{(i)}(t)$, respectively. scatterer distributions like the uniform and Gaussian PDFs. Here, we use the von Mises PDF to describe the time-varying angles

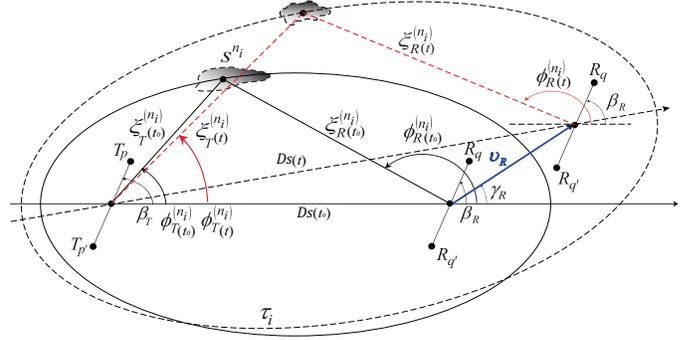


Fig. 4. The time-varying angular parameters in the HST channel model.

$\phi_T^{(n_i)}(t)$ and $\phi_R^{(n_i)}(t)$ as it is a general function and includes some well-known PDFs as special cases, e.g., uniform and Gaussian PDFs [43]. The von Mises PDF is defined as $f(\phi) \triangleq \exp[k \cos(\phi - \mu)] / [2\pi I_0(k)]$, where μ is the mean value of angle $\phi \in [-\pi, \pi)$, $I_0(\cdot)$ is the zeroth-order modified Bessel function of the first kind, and k ($k \geq 0$) is a positive real-valued parameter that controls the spread of ϕ . Applying the von Mises distribution to the time-varying AoAs, we get $f(\phi_R^{(i)}(t)) \triangleq \exp[k_R^{(i)} \cos(\phi_R^{(i)} - \mu_R^{(i)}(t))] / [2\pi I_0(k_R^{(i)})]$, where $\mu_R^{(i)}$ is the mean angular value of the AoA $\phi_R^{(i)}$ and $k_R^{(i)}$ is the relevant von Mises parameter that controls the spread of $\phi_R^{(i)}$. Similarly, we can get $f(\phi_T^{(i)}(t))$ with $\mu_T^{(i)}$ and $k_T^{(i)}$.

In Fig. 4, the MRS is moving with the speed of v_R in the direction defined by the angle of motion γ_R . Correspondingly, the AoAs and the axes of the ellipses will be changed. The distance between the BS and the MRS can be calculated as $D_s(t) = 2f_s(t) = \sqrt{D_s^2(t_0) + (v_R t)^2 + 2D_s(t_0)v_R t \cos \gamma_R}$. Based on the geometric relations and by defining all the angles in Fig. 4, the time-varying function of mean AoA $\mu_R^{(i)}(t)$ can be derived as (12) [46], which is presented at the top of the next page.

B. Statistical Properties of the Theoretical Model

In this subsection, we will derive the statistical properties of the proposed non-stationary HST GBSM based on the theoretical framework described in Section II under the US and antenna stationarity assumptions.

$$\mu_R^{(i)}(t) = \begin{cases} \gamma_R - \arccos\left(\frac{v_R t - \xi_R^{(n_i)}(t_0) \cos(\gamma_R - \mu_R^{(i)}(t_0))}{\sqrt{\xi_R^{2(n_i)}(t_0) + (v_R t)^2 - 2\xi_R^{(n_i)}(t_0)v_R t \cos(\gamma_R - \mu_R^{(i)}(t_0)}}}\right), & -\pi \leq \gamma_R \leq 0 \\ \gamma_R + \arccos\left(\frac{v_R t - \xi_R^{(n_i)}(t_0) \cos(\gamma_R - \mu_R^{(i)}(t_0))}{\sqrt{\xi_R^{2(n_i)}(t_0) + (v_R t)^2 - 2\xi_R^{(n_i)}(t_0)v_R t \cos(\gamma_R - \mu_R^{(i)}(t_0)}}}\right), & 0 \leq \gamma_R \leq \pi. \end{cases} \quad (12)$$

1) *Time-variant ST CF*: The correlation properties of two arbitrary channel impulse responses $h_{pq}(t, \tau)$ and $h_{p'q'}(t, \tau)$ of a wideband MIMO HST channel are determined by the correlation properties of $h_{i,pq}(t)$ and $h_{i,p'q'}(t)$ in each tap, since there is no correlation between the underlying processes in different taps. The normalized time-variant ST CF can be derived as

$$R_h(t, \Delta x_T, \Delta x_R, \Delta t) = \frac{\mathbb{E}\{h_{i,pq}(t) h_{i,p'q'}^*(t - \Delta t)\}}{\sqrt{\Omega_{i,pq} \Omega_{i,p'q'}}} \quad (13)$$

which can be obtained from the time-delay variant space CCF $R_h(t, \tau; \Delta t, \Delta x)$ in Fig. 1 with $\tau = 0$.

– In the case of the LoS component,

$$R_h^{\text{LoS}}(t, \Delta x_T, \Delta x_R, \Delta t) = K' e^{j2\pi [P \cos \beta_T - Q \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R)]} \\ \times e^{j2\pi f_{\max} \cos(\phi_{T_p}^{\text{LoS}}(t - \Delta t) - \gamma_R) \Delta t} \quad (14)$$

where $P = (p' - p) \Delta x_T / \lambda$, $Q = (q' - q) \Delta x_R / \lambda$, and $K' = \sqrt{\frac{K_{pq} K_{p'q'}}{(K_{pq} + 1)(K_{p'q'} + 1)}}$.

– In the case of the SB component,

$$R_h^{\text{SB}_i}(t, \Delta x_T, \Delta x_R, \Delta t) = \frac{1}{2\pi I_0(k_R^{(i)}) U} \\ \times \int_{-\pi}^{\pi} e^{k_R^{(i)} \cos(\phi_R^{(i)} - \mu_R^{(i)}(t))} e^{j2\pi [P \cos(\phi_T^{(i)} - \beta_T) + Q \cos(\phi_R^{(i)} - \beta_R)]} \\ \times e^{j2\pi \xi_{T_R}^{(n_i)}(t, \Delta t)} e^{j2\pi f_{\max} \cos(\phi_R^{(i)} - \gamma_R) \Delta t} d\phi_R^{(i)} \quad (15)$$

where $\xi_{T_R}^{n_i}(t, \Delta t) = \xi_T^{n_i}(t - \Delta t) - \xi_T^{n_i}(t) + \xi_R^{n_i}(t - \Delta t) - \xi_R^{n_i}(t)$.

By imposing $\Delta t = 0$ in (13), we get the normalized time-variant space CCF between two arbitrary channel coefficients as

$$\rho(t, \Delta x_T, \Delta x_R) = \frac{\mathbb{E}\{h_{i,pq}(t) h_{i,p'q'}^*(t)\}}{\sqrt{\Omega_{i,pq} \Omega_{i,p'q'}}} \\ = R_h(t, \Delta x_T, \Delta x_R, 0). \quad (16)$$

– In the case of the LoS component,

$$\rho^{\text{LoS}}(t, \Delta x_T, \Delta x_R) = K' e^{j2\pi [P \cos \beta_T - Q \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R)]}. \quad (17)$$

– In the case of the SB component,

$$\rho^{\text{SB}_i}(t, \Delta x_T, \Delta x_R) = \frac{1}{2\pi I_0(k_R^{(i)}) U} \int_{-\pi}^{\pi} e^{k_R^{(i)} \cos(\phi_R^{(i)} - \mu_R^{(i)}(t))} \\ \times e^{j2\pi [P \cos(\phi_T^{(i)} - \beta_T) + Q \cos(\phi_R^{(i)} - \beta_R)]} d\phi_R^{(i)}. \quad (18)$$

The normalized time-variant space CCF for the first tap ($i=1$) can be expressed as the summation of (17) and (18) with $i=1$, i.e.,

$$\rho_1(t, \Delta x_T, \Delta x_R) = \rho^{\text{LoS}}(t, \Delta x_T, \Delta x_R) + \rho^{\text{SB}_1}(t, \Delta x_T, \Delta x_R). \quad (19)$$

Similarly, the normalized time-variant ACF can be obtained by imposing $\Delta x_T = 0$ and $\Delta x_R = 0$ in (13), i.e.,

$$r(t, \Delta t) = \frac{\mathbb{E}\{h_{i,pq}(t) h_{i,pq}^*(t - \Delta t)\}}{\sqrt{\Omega_{i,pq} \Omega_{i,p'q'}}} = R_h(t, 0, 0, \Delta t). \quad (20)$$

– In the case of the LoS component,

$$r^{\text{LoS}}(t, \Delta t) = \frac{K_{pq}}{1 + K_{pq}} e^{j2\pi f_{\max} \cos(\phi^{\text{LoS}}(t - \Delta t) - \gamma_R) \Delta t}. \quad (21)$$

– In the case of the SB component,

$$r^{\text{SB}_i}(t, \Delta t) = \frac{1}{2\pi I_0(k_R^{(i)}) (1 + K_{pq})} \int_{-\pi}^{\pi} e^{k_R^{(i)} \cos(\phi_R^{(i)} - \mu_R^{(i)}(t))} \\ \times e^{j2\pi \xi_{T_R}^{(n_i)}(t, \Delta t)} e^{j2\pi f_{\max} \cos(\phi_R^{(i)} - \gamma_R) \Delta t} d\phi_R^{(i)}. \quad (22)$$

Therefore, the normalized time-variant ACF for the first tap ($i=1$) can be expressed as the summation of (21) and (22) with $i=1$, i.e.,

$$r_1(t, \Delta t) = r^{\text{LoS}}(t, \Delta t) + r^{\text{SB}_1}(t, \Delta t). \quad (23)$$

2) *Time-variant SD PSD*: The time-variant SD PSD can be obtained from the time-variant ST CF by applying the Fourier transformation in terms of Δt , i.e.,

$$W(t, \nu, \Delta x_T, \Delta x_R) = \int R_h(t, \Delta x_T, \Delta x_R, \Delta t) e^{-j2\pi \nu \Delta t} d\Delta t. \quad (24)$$

– In case of the LoS component,

$$W^{\text{LoS}}(t, \nu, \Delta x_T, \Delta x_R) = K' e^{j2\pi [P \cos \beta_T - Q \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R)]} \\ \times \delta(\nu - (G(t) + v_R)) \quad (25)$$

where $G(t) = f_{\max} \cos(\phi_{T_p}^{\text{LoS}}(t) - \gamma_R)$.

– In case of the SB component,

$$W^{\text{SB}_i}(t, \nu, \Delta x_T, \Delta x_R) = \int R_h^{\text{SB}_i}(t, \Delta x_T, \Delta x_R, \Delta t) \\ \times e^{-j2\pi \nu \Delta t} d\Delta t. \quad (26)$$

This integral will have to be evaluated numerically.

3) *LSF*: It can be obtained from the time-variant space-time-frequency CF $R_L(t; \Delta t, \Delta f, \Delta x)$ using Fourier transform with respect to Δt and Δx and inverse Fourier transform with respect to Δf , i.e.,

$$C_H(t, \tau, \nu, \Omega) = \iint \iint R_L(t; \Delta t, \Delta f, \Delta x) \times e^{-j2\pi(\nu\Delta t - \tau\Delta f + \Omega\Delta x)} d\Delta t d\Delta f d\Delta x. \quad (27)$$

where the time-variant space-time-frequency CF can be obtained from (3) after considering the US and antenna stationarity assumptions, i.e.,

$$R_L(t; \Delta t, \Delta f, \Delta x) = \frac{\mathbb{E}\left\{L_{H_{pq}}(t, f)L_{H_{p'q'}}^*(t - \Delta t, f - \Delta f)\right\}}{\sqrt{\Omega_{i,pq}\Omega_{i,p'q'}}} \quad (28)$$

Here, $L_{H_{pq}}(t, f)$ is the space-time-variant transfer function that can be obtained by (1), i.e.,

$$L_{H_{pq}}(t, f) = \int h_{pq}(t, \tau) e^{-j2\pi f\tau} d\tau. \quad (29)$$

– In the case of the LoS component,

$$R_L^{\text{LoS}}(t; \Delta t, \Delta f, \Delta x) = K' e^{j2\pi[P \cos \beta_T - Q \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R)]} \times e^{j2\pi f_{\max} \cos(\phi_{T_p}^{\text{LoS}}(t) - \gamma_R) \Delta t - \Delta f \tau_1} \quad (30)$$

where

$$C_H^{\text{LoS}}(t, \tau, \nu, \Omega) = \iint \iint R_L^{\text{LoS}}(t; \Delta t, \Delta f, \Delta x) \times e^{-j2\pi(\nu\Delta t - \tau\Delta f + \Omega\Delta x)} d\Delta t d\Delta f d\Delta x. \quad (31)$$

– In the case of the SB component,

$$C_H^{\text{SB}_i}(t, \tau, \nu, \Omega) = \iint \iint R_L^{\text{SB}_i}(t; \Delta t, \Delta f, \Delta x) \times e^{-j2\pi(\nu\Delta t - \tau\Delta f + \Omega\Delta x)} d\Delta t d\Delta f d\Delta x \quad (32)$$

where the time-variant space-time-frequency CF $R_L^{\text{SB}_i}(t; \Delta t, \Delta f, \Delta x)$ can be expressed as (33), which is shown at the top of the next page.

It is important to mention that all the investigated statistical properties in this section, i.e., $R_h(t, \Delta x_T, \Delta x_R, \Delta t)$, $\rho(t, \Delta x_T, \Delta x_R)$, $r(t, \Delta t)$, $W(t, \nu, \Delta x_T, \Delta x_R)$, and $C_H(t, \tau, \nu, \Omega)$, are time-variant due to the non-stationarity of the proposed GBSM. For stationary channel models, the corresponding statistical properties are not dependent on t .

IV. THE SIMULATION MODEL FOR WIDEBAND MIMO HST CHANNELS

A. Description of the Wideband MIMO Simulation Model

The proposed theoretical model assumes an infinite number of effective scatters and hence it cannot be used for simulations. Therefore, we need to develop a HST simulation model, which can be obtained from the theoretical one by utilizing only a finite number of scatterers N . The complex space-time-variant tap coefficient of the first tap of the link T_p-R_q for the simulation model can be expressed as

$$\tilde{h}_{1,pq}(t) = \tilde{h}_{1,pq}^{\text{LoS}}(t) + \tilde{h}_{1,pq}^{\text{SB}}(t) \quad (34)$$

where

$$\tilde{h}_{1,pq}^{\text{LoS}}(t) = \sqrt{\frac{K_{pq}}{K_{pq} + 1}} e^{-j2\pi f_c \tau_{pq}(t)} e^{j[2\pi f_{\max} t \cos(\phi_{T_p}^{\text{LoS}}(t) - \gamma_R)]} \quad (35a)$$

and

$$\tilde{h}_{1,pq}^{\text{SB}}(t) = \sqrt{\frac{\Omega_{1,pq}}{K_{pq} + 1}} \sum_{n_1=1}^{N_1} \frac{1}{\sqrt{N_1}} e^{j(\psi_{n_1} - 2\pi f_c \tau_{pq, n_1}(t))} \times e^{j[2\pi f_{\max} t \cos(\tilde{\phi}_R^{(n_1)}(t) - \gamma_R)]}. \quad (35b)$$

The complex space-time-variant channel coefficient for the rest of the taps ($1 < i \leq I$) can be expressed as

$$\tilde{h}_{i,pq}(t) = \tilde{h}_{i,pq}^{\text{SB}}(t) = \sqrt{\Omega_{i,pq}} \sum_{n_i=1}^{N_i} \frac{1}{\sqrt{N_i}} e^{j(\psi_{n_i} - 2\pi f_c \tau_{pq, n_i}(t))} \times e^{j[2\pi f_{\max} t \cos(\tilde{\phi}_R^{(n_i)}(t) - \gamma_R)]}, 1 < i \leq I. \quad (36)$$

By comparing the simulation and theoretical models and considering the fact that the AoDs are related to the AoAs, we only need to determine the discrete AoA $\left\{\tilde{\phi}_R^{(n_i)}\right\}_{n_i=1}^{N_i}$ for the simulation model. In case of isotropic scattering, i.e., $k_R^{(i)} = 0$, the quantities $\left\{\tilde{\phi}_R^{(n_i)}\right\}_{n_i=1}^{N_i}$ should preferably be computed using the extended method of exact Doppler spread (EMEDS) [42], while MMEA and the L_p -norm method (LPNM) provide high quality solutions when the scattering is non-isotropic [42]. Here, we consider a non-isotropic scattering environment and hence we will use MMEA to calculate $\left\{\tilde{\phi}_R^{(n_i)}\right\}_{n_i=1}^{N_i}$ for the simulation model. By applying the MMEA, the AoAs $\left\{\tilde{\phi}_R^{(n_i)}\right\}_{n_i=1}^{N_i}$ can be determined by finding the solutions of the following equation using numerical root-finding techniques [42]:

$$\frac{n_i - \frac{1}{4}}{N_i} - \int_{\mu_R^{(i)}(t_0) - \pi}^{\tilde{\phi}_R^{(n_i)}} f(\phi_R^{(i)}(t_0)) d\phi_R^{(i)} = 0, \quad n_i = 1, 2, \dots, N_i. \quad (37)$$

Reasonable values of N_i are in the range from 40 to 50 [42].

B. Statistical Properties of the Simulation Model

Based on our wideband MIMO HST theoretical model and its statistical properties, the corresponding statistical properties for the simulation model can be derived by using discrete angle parameters.

1) *Time-variant ST CF*: The normalized time-variant ST CF can be calculated by

$$\tilde{R}_h(t, \Delta x_T, \Delta x_R, \Delta t) = \frac{\mathbb{E}\left\{\tilde{h}_{i,pq}(t)\tilde{h}_{i,p'q'}^*(t - \Delta t)\right\}}{\sqrt{\Omega_{i,pq}\Omega_{i,p'q'}}}. \quad (38)$$

– In the case of the LoS component,

$$\tilde{R}_h^{\text{LoS}}(t, \Delta x_T, \Delta x_R, \Delta t) = K' e^{j2\pi[P \cos \beta_T - Q \cos(\phi_{T_p}^{\text{LoS}}(t) - \beta_R)]} \times e^{j2\pi f_{\max} \cos(\tilde{\phi}_R^{\text{LoS}}(t) - \gamma_R) \Delta t}. \quad (39)$$

$$R_L^{SBi}(t; \Delta t, \Delta f, \Delta x) = \frac{1}{2\pi I_0 \left(k_R^{(i)} \right) U} \int_{-\pi}^{\pi} e^{k_R^{(i)} \cos(\phi_R^{(i)} - \mu_R^{(i)}(t))} e^{j2\pi f_{\max} \cos(\phi_R^{(i)} - \gamma_R) \Delta t} \\ \times e^{j2\pi [P \cos(\phi_T^{(i)} - \beta_T) + Q \cos(\phi_R^{(i)} - \beta_R)]} e^{-j2\pi \Delta f \tau_i} d\phi_R^{(i)}. \quad (33)$$

– In the case of the SB component,

$$\tilde{R}_h^{SBi}(t, \Delta x_T, \Delta x_R, \Delta t) = \frac{1}{N_i U} \\ \times \sum_{n_i=1}^{N_i} e^{j2\pi [P \cos(\tilde{\phi}_T^{(n_i)}(t) - \beta_T) + Q \cos(\tilde{\phi}_R^{(n_i)}(t) - \beta_R)]} \\ \times e^{j2\pi \xi_{TR}^{(n_i)}(t, \Delta t)} e^{j2\pi f_{\max} \cos(\tilde{\phi}_R^{(n_i)}(t) - \gamma_R) \Delta t}. \quad (40)$$

Similar to the procedure applied to the theoretical model, the normalized time-variant space CCF and the time-variant ACF of the simulation model can be expressed as

$$\tilde{\rho}(t, \Delta x_T, \Delta x_R) = \frac{\mathbb{E} \left\{ \tilde{h}_{i,pq}(t) \tilde{h}_{i,p'q'}^*(t) \right\}}{\sqrt{\Omega_{i,pq} \Omega_{i,p'q'}}} \\ = \tilde{R}_h(t, \Delta x_T, \Delta x_R, 0) \quad (41)$$

$$\tilde{r}(t, \Delta t) = \frac{\mathbb{E} \left\{ \tilde{h}_{i,pq}(t) \tilde{h}_{i,pq}^*(t - \Delta t) \right\}}{\sqrt{\Omega_{i,pq} \Omega_{i,p'q'}}} = \tilde{R}_h(t, 0, 0, \Delta t) \quad (42)$$

respectively.

2) *Time-variant SD PSD*: The time-variant SD PSD of the simulation model $\tilde{W}(t, \nu, \Delta x_T, \Delta x_R)$ can be obtained from the ST CF by applying the Fourier transform in terms of Δt . Therefore, it can be expressed similar to (24) by replacing $R_h(t, \Delta x_T, \Delta x_R, \Delta t)$ by $\tilde{R}_h(t, \Delta x_T, \Delta x_R, \Delta t)$.

– In case of the LoS component, $\tilde{W}^{\text{LoS}}(t, \nu, \Delta x_T, \Delta x_R)$ can be obtained by replacing $\phi_{T_p}^{\text{LoS}}$ by $\tilde{\phi}_{T_p}^{\text{LoS}}$ in (25).

– In case of the SB component, time-variant SD PSD $\tilde{W}^{\text{SBi}}(t, \nu, \Delta x_T, \Delta x_R)$ can be obtained from (26) by substituting $R_h^{\text{SBi}}(t, \Delta x_T, \Delta x_R, \Delta t)$ by $\tilde{R}_h^{\text{SBi}}(t, \Delta x_T, \Delta x_R, \Delta t)$.

3) *LSF*: Analogous to the theoretical model, the LSF of the simulation model $\tilde{C}_H(t, \tau, \nu, \Omega)$ can be obtained from the time-frequency-space CF $\tilde{R}_L(t; \Delta t, \Delta f, \Delta x)$. Therefore, the derived equations can be obtained from (27)–(32) by replacing the theoretical model functions and the continuous model parameters, e.g., $\phi_R^{(i)}$ with the corresponding simulation model functions and discrete model parameters, e.g., $\tilde{\phi}_R^{(n_i)}$.

V. RESULTS AND ANALYSIS

In this section, the statistical properties of the proposed theoretical model and simulation model are evaluated and analyzed. Then, the proposed simulation channel model is further validated by measurements. The parameters for our analysis are listed here or specified otherwise: the LoS Ricean factor $K_{pq} = K_{p'q'} = 6$, taps delays for the first and second taps are $\tau_1 = 0$ and $\tau_2 = 35$ ns, respectively, as for the RMa scenario in [10], $v_R = 360$ km/h, $f_c = 4$ GHz, and thus $f_{\max} = 1.34$ KHz, $D_s(t_0) = 1000$ m, $D_{\min} = 50$ m as in

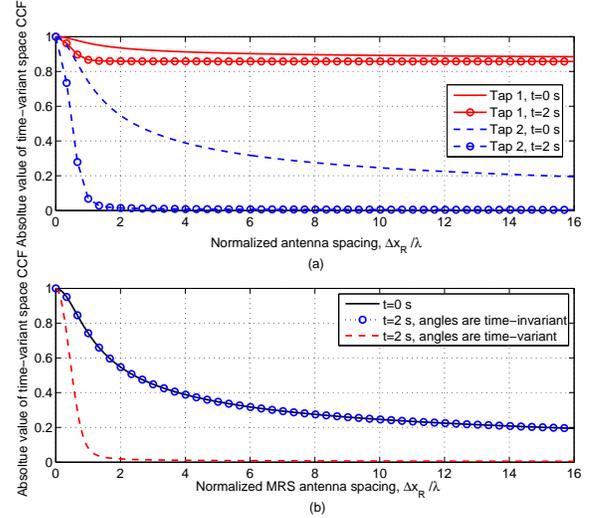


Fig. 5. (a) The absolute values of the time-variant space CCF of different taps of the proposed HST channel model at different time instants. (b) The absolute values of the time-variant space CCF of the second tap with/without time-varying angular parameters.

[5], $a_1(t_0) = \frac{D_s(t_0)}{2} + 5$ m, $a_2(t_0) = \frac{D_s(t_0)}{2} + 10.25$ m, $\xi_R^{(n_i)}(t_0) = 600$ m, $\gamma_R = 30^\circ$, $\mu_R^{(i)}(t_0) = 45^\circ$, $k_R^{(i)} = 6$ and we use a linear antenna array with $M_R = M_T = 2$ and $\beta_R = \beta_T = 60^\circ$.

A. Time-variant ST CFs

By adopting a BS antenna element spacing $\Delta x_T = \lambda$, the absolute values of the time-variant space CCF of non-stationary HST MIMO channel model are illustrated in Fig. 5(a) and Fig. 5(b). By using (19) and imposing $i = 2$ in (18), Fig. 5(a) shows the absolute values of the time-variant space CCF of the first and second taps of the theoretical model at two different time instants, i.e., $t = 0$ s and 2 s. From the figure, we can easily notice the higher correlation in the first tap in comparison with the second one because of the dominant LoS component. To highlight the impact of the time-varying parameters on channel statistical properties, Fig. 5(b) shows the absolute values of the time-variant space CCF of the second tap with time-variant and time-invariant angular parameters. It shows that time-varying angles are the only time-varying parameters that affect the time-variant space CCF. The same conclusion can be drawn from (18). Fig. 6 shows a comparison between the time-variant space CCFs of the theoretical model (18), simulation model (41), and simulation results with $N=50$ for BS antenna spacing $\Delta x_T = \lambda$ at different time instants $t = 0$ s and 2 s. It shows that the simulation model provides a fairly good approximation

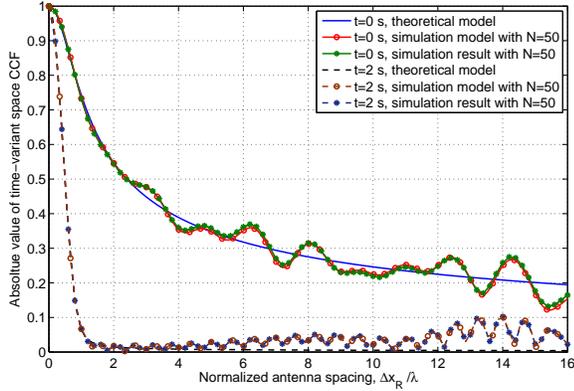


Fig. 6. Comparison between the time-variant space CCFs of the second tap of the theoretical model and simulation model for different time instants.

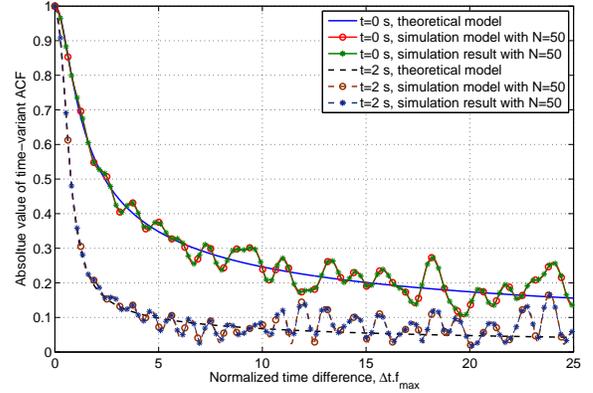


Fig. 8. Comparison between the time-variant ACFs of the second tap of the theoretical model and simulation model for different time instants.

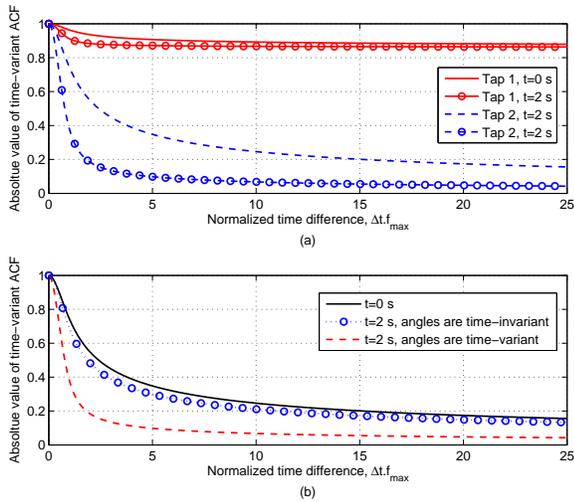


Fig. 7. (a) The absolute values of the time-variant ACF of different taps of the proposed HST channel model at different time instants. (b) The absolute values of the time-variant ACF with/without time-varying angular parameters.

to the theoretical one especially at small antenna spacings. The simulation results fit the simulation model very well, demonstrating the correctness of both theoretical derivations and simulations.

By using (23) and imposing $i = 2$ in (18), Fig. 7(a) shows the absolute values of the time-variant ACF of different taps of the proposed theoretical HST channel model at different time instants. A higher correlation in the first tap in comparison with the second can be easily noticed. Again, this is due to the dominant LoS component. Fig. 7(b) shows the absolute values of the time-variant ACF of the second tap with/without time-varying angular parameters. We can see that even with time-invariant angles, the absolute value of the time-variant ACF still changes with time because of the time-varying dimensions of the ellipses. The same conclusion can be drawn from (22). From this figure, we can also calculate *coherence time*, which quantifies the duration within which the channel is approximately constant and can be defined as the smallest value of Δt that fulfills the condition $|r(t, \Delta t)| = \frac{1}{2}|r(0, \Delta t)|$.

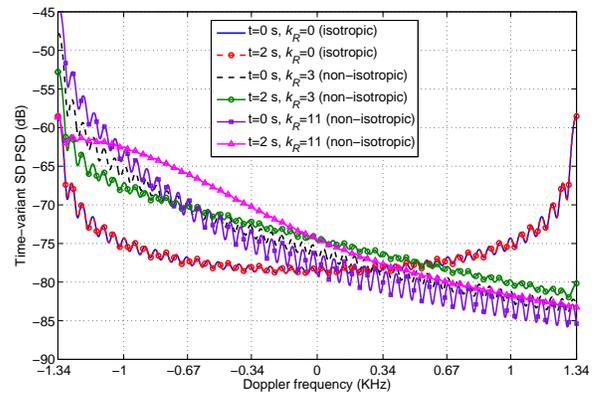


Fig. 9. Time-variant SD PSDs of the theoretical model for different scenarios ($v_R = 360$ km/h, $f_{\max} = 1.34$ KHz): isotropic: $k_R = 0$ & non-isotropic: $k_R = 3$ & 11.

The coherence time for time-variant and time-invariant angular parameters is equal to 1 ms and 4 ms, respectively. It is important to mention that the smaller the coherence time, the larger the Doppler spread. Fig. 8 shows a comparison between the time-variant ACFs of the second tap of the theoretical model (22), simulation model (42), and simulation results for different time instants. Again, the simulation model provides a fairly good approximation to the theoretical one especially in small values of time separation. The simulation results and (42) of the simulation model match very well, illustrating the correctness of the derivation of (42) and simulations.

B. Time-variant SD PSDs

Fig. 9 compares the time-variant SD PSDs of the theoretical model (24) for isotropic (i.e., $k_R = 0$) and non-isotropic (i.e., $k_R > 0$) scenarios at different time instants with $\Delta x_T = \Delta x_R = \lambda$. We can easily notice that the SD PSD is U-shaped for isotropic case only. To understand the impact of the angular parameters on SD PSD given in (26) for the theoretical model and the corresponding simulation model, Fig. 10 shows normalized SD PSDs of both models for different angular parameters, i.e., the angle of motion γ_R and the initial mean

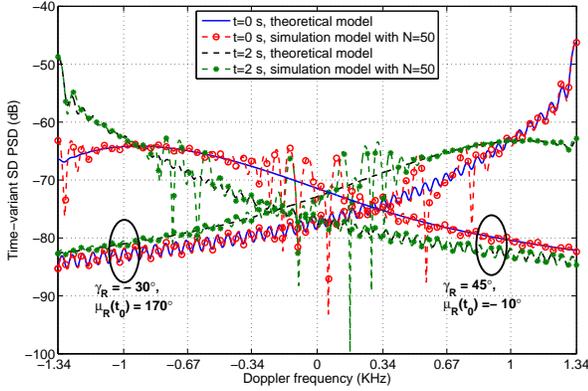


Fig. 10. Time-variant SD PSDs of the theoretical and simulation models for different angular parameters ($v_R = 360$ km/h, $f_{\max} = 1.34$ KHz, $k_R = 11$).

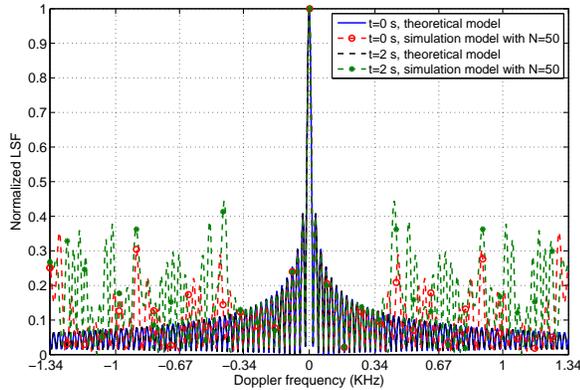


Fig. 11. Comparison between the LSFs of the second tap of the theoretical model and the simulation model for different time instants.

AoA $\mu_R(t_0)$. From this figure, it can be concluded that angular parameters of channel models affect considerably the trends of the time-variant SD PSDs.

C. LSFs

Fig. 11 shows a comparison between the LSFs of the theoretical model and simulation model with $N=50$ for different time instants. It can be noticed how the power of the effective scatterers varies with time t and the power of the components with zero Doppler frequency is higher than the rest of the components. Simulation model shows good approximation to the theoretical one at different time instants. different time instants due to the non-stationarity of the HST channel. They also demonstrate that simulation model provides a good approximation to the statistical properties of the theoretical one.

D. Stationary Interval

To verify our proposed channel models, we use HST measurement data presented in [27] where the authors compared the stationary interval of a measured HST channel with that of standard channel models such as IMT-A and WINNER II.

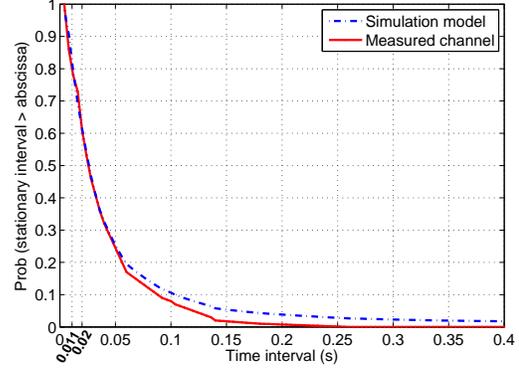


Fig. 12. The empirical CCDFs of stationary intervals for the proposed HST simulation model and the measured channel in [27].

The stationary interval can be calculated using averaged power delay profiles (APDPs) that can be expressed as [27]

$$\overline{P}_h(t_k, \tau) = \frac{1}{N_{PD P}} \sum_k^{k+N_{PD P}-1} |\tilde{h}_{pq}(t_k, \tau)|^2 \quad (43)$$

where $N_{PD P}$ is the number of power delay profiles to be averaged, t_k is the time of the k -th drop (snapshot), and $\tilde{h}_{pq}(t_k, \tau) = \sum_{i=1}^I \tilde{h}_{i,pq}(t_k) \delta(\tau - \tau_i)$. The correlation coefficient between two APDPs can be calculated as

$$c(t_k, \Delta t) = \frac{\int \overline{P}_h(t_k, \tau) \overline{P}_h(t_k + \Delta t, \tau) d\tau}{\max\{\int \overline{P}_h(t_k, \tau)^2 d\tau, \int \overline{P}_h(t_k + \Delta t, \tau)^2 d\tau\}} \quad (44)$$

The stationary interval can be then calculated as

$$T_s(t_k) = \max\{\Delta t | c(t_k, \Delta t) \geq c_{\text{thresh}}\}, \quad (45)$$

where c_{thresh} is a given threshold of the correlation coefficient. Fig. 12 shows the empirical complementary cumulative distribution functions (CCDFs) of stationary intervals for our proposed HST simulation model and the measured HST channel using the following simulation parameters obtained from [27]: $f_c = 930$ MHz, $v_R = 324$ km/h, $N_{PD P} = 15$, $c_{\text{thresh}} = 0.8$. It is worth mentioning that since the measured HST channel is a narrowband one, in (43) we used $\tilde{h}_{pq}(t_k, \tau) = \tilde{h}_{1,pq}(t_k) \delta(\tau - \tau_1)$ where $\tilde{h}_{1,pq}(t_k)$ is given in (34). The excellent agreement between the proposed HST simulation model and the measurement data demonstrates the utility of our HST channel models. From Fig. 12, the stationary interval is equal to 11 ms for 80% and 20 ms for 60% which is considerably shorter than the ones reported for standardized channel models, i.e., 37.8 ms for 60% as we previously mentioned in the introduction.

VI. CONCLUSIONS

In this paper, we have proposed a non-stationary theoretical wideband MIMO HST GBSM for the outdoor channel of HST communication systems adopting MRS technology. The proposed model contains time-varying model parameters, i.e., angular parameters and distance between the Tx and Rx. Using the MMEA, a corresponding SoS simulation model

has been developed. Both models can be further used to model non-stationary V2I channels. The statistical properties of both models have been investigated based on a proposed framework that describes non-stationary channels. Numerical analyses have shown that these statistical properties experience different behaviours at different time instants, demonstrating the capability of the proposed models to mimic the non-stationarity of HST channels. The dominance of the LoS component has resulted in higher correlation in the first tap of the proposed channel models in comparison with the second one. It has also been demonstrated that the time-varying angles will affect the time-variant space CCFs and time-variant ACFs while time-varying dimensions of the ellipses will only have an influence on the time variant ACFs. Moreover, the trends of the time-variant SD PSDs are considerably affected by the angular parameters of the channel models. For all statistical properties, the simulation model provides good approximation to the theoretical one. Finally, it has been shown that the stationary interval of our simulation model matches well that of the measured data, which validates the utility of the proposed model. Our future work will further verify the proposed models by fitting more statistical properties to those of relevant measurement data, which have not yet been available in the existing literature to the best of our knowledge.

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