Star-QAM Signaling Constellations for Spatial Modulation

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Abstract—The performance of spatial modulation (SM)-assisted 6 multiple-input-multiple-output (MIMO) communication systems 7 is highly dependent on the specific amplitude/phase modulation 8 (APM) signal constellation adopted. In this paper, we conceive 9 new star-quadrature amplitude modulation (star-QAM)-aided SM 10 schemes. Our goal is to minimize the system's average bit error 11 probability (ABEP). More specifically, a new class of star-QAM 12 constellations is introduced for SM, which is capable of flexi-13 bly adapting ring ratios of the amplitude levels. Then, under a 14 specific MIMO configuration and a predetermined transmission 15 rate, a simple and efficient ring-ratio optimization algorithm is 16 proposed to minimize the ABEP. Moreover, to improve further 17 the performance of our star-QAM-aided SM scheme, a diagonal 18 precoding technique is proposed, and a low-complexity minimum-19 distance-based approach is conceived for extracting the precod-20 ing parameters. Our numerical results show that the proposed 21 star-QAM-aided SM arrangement provides beneficial system per-22 formance improvements compared with the identical-throughput 23 maximum-minimum distance (MMD) QAM and phase-shift key-24 ing (PSK) benchmarkers. Moreover, our precoding scheme is 25 capable of further improving the attainable system performance 26 at a modest feedback requirement.

27 *Index Terms*—Constellation optimization, multiple-input—28 multiple-output (MIMO), spatial modulation (SM), star-29 quadrature amplitude modulation (star-QAM).

I. Introduction

31 S PATIAL MODULATION (SM), which maps the informa-32 S tion bits to two information-carrying entities, namely the an-33 tenna indexes and the combined amplitude/phase modulation 34 (APM) constellation, constitutes a promising low-complexity 35 multiple-input-multiple-output (MIMO) transmission tech-36 nique [1]–[8]. In a conventional single-input-single-output 37 (SISO) system, the Gray-coded maximum-minimum distance

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(MMD) quadrature amplitude modulation (QAM) constellation 38 minimizes the bit error rate (BER) [9], [10]. However, the 39 advantage of MMD-QAM may be eroded in SM-MIMO sys- 40 tems [11]. This is due to the fact that the BER performance of 41 SM-MIMO systems is jointly determined by the spatial signal 42 (i.e., antenna indexes), by the classic APM constellation, and 43 by their interaction [11]–[18].

Recently, the effects of APM schemes on the performance 45 of SM have been investigated in [11], [14], and [18]. More 46 specifically, in [11], the performance of SM systems relying 47 both on conventional QAM and PSK modulation was studied, 48 demonstrating that, in some MIMO setups, the PSK-modulated 49 SM scheme may outperform the identical-throughput MMD- 50 QAM-aided SM scheme. In [18], the dispersion matrices and 51 the signal constellations were jointly optimized for a near- 52 capacity irregular precoded space-time shift keying (STSK) 53 system, which includes SM as a special case and strikes a 54 flexible rate-diversity tradeoff. It was also shown in [14] that 55 the star-QAM-aided STSK scheme outperforms its MMD-56 based square-QAM-aided counterpart. This observation may 57 be also valid for SM systems [11]. The aforementioned results 58 indicated that the performance of SM is highly dependent on 59 the specific APM adopted; hence, a suitable APM scheme has 60 to be designed for this hybrid modulation scheme.

On the other hand, star-QAM constitutes a special case of 62 circular amplitude- and phase-shift keying, which is capable of 63 outperforming the classic square-QAM constellation in peak- 64 power-limited systems [19]. Hence, it has been adopted in most 65 of the recent satellite communication standards, such as in 66 the Digital Video Broadcast System (DVB) S2, DVB-SH, and 67 the Internet Protocol over Satellite and Advanced Broadcasting 68 System via Satellite [19]. The star-QAM constellation is com- 69 posed of multiple concentric circles, and it was shown to be 70 beneficial in the context of STSK systems. Hence, star-QAM 71 may be an attractive APM candidate for SM-MIMO. However, 72 the constellations' optimization has not been carried out for 73 star-QAM-aided SM.

Moreover, to increase the robustness of the SM-MIMO sys-75 tem, limited-feedback-aided link adaptation schemes have been 76 proposed in [20]–[26]. For example, in [20], an opportunistic 77 power-allocation (PA) scheme was conceived for achieving a 78 beneficial transmit diversity gain in SM-MIMO systems. In 79 [21], a beamforming codebook was designed for optimizing the 80 coding gain of SM-MIMO based on the knowledge of the chan-81 nel envelope's spatial correlation. Recently, an adaptive closed-82 loop-aided method was invoked for providing both diversity 83 and coding gains in the context of space-shift keying (SSK)[22], 84

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85 which is a special case of SM. However, the scheme proposed 86 for SSK may not be directly applicable to the conventional 87 SM scheme. Moreover, ASM-MIMO architectures relying on 88 different combinations of modulation schemes were proposed 89 in [24], which aimed for maximizing the channel capacity at a 90 predefined target BER, rather than for minimizing the BER. In 91 contrast, in [25] and [26], a transmit precoding (TPC) technique 92 was used for improving the modulated signal design for SM. 93 However, this technique may only be suitable for a new class of 94 SM relying on a single-receiver antenna. For the conventional 95 SM, we proposed a near-instantaneously adaptive-modulation-96 aided scheme for minimizing the BER [7], which was termed 97 adaptive SM (ASM). Then, we further generalized this paper in 98 [12] and [15], where the implementation complexity of ASM 99 was considerably reduced. However, ASM typically transmits 100 a different number of bits in the different-quality time slots, 101 which may be inconvenient in fixed-rate applications and po-102 tentially leads to error propagation in the case of ASM-mode 103 signaling errors.

104 Against this background, the novel contributions of this 105 paper are threefold.

- We introduced the class of star-QAM constellations [27], which is capable of flexibly adapting the ring ratios, hence subsuming classic PSK as a special case. Alternatively, if the ring ratio is appropriately selected, the proposed star-QAM is capable of achieving almost the same Euclidean distance (ED) as the MMD-based QAM.
- Given a specific MIMO configuration and a predetermined 112 transmission rate, a low-complexity yet efficient optimiza-113 114 tion algorithm is proposed to minimize the average bit error probability (ABEP) of SM-MIMO systems, where 115 the effects of both the antenna index, as well as of the APM 116 signal and their interaction, are jointly considered. Only 117 118 the optimal ring ratios of star-QAM constellation have to be found by the optimization algorithm. 119
 - We introduce a new TPC scheme for star-QAM-aided SM-MIMO systems, which further improves the performance. To retain the benefits of SM, such as its low-complexity single-stream detector and its single RF chain, we design its TPC matrix P to be diagonal. We demonstrate that this precoded scheme and the ASM schemes of [12] and [15] are capable of exploiting the same degrees of freedom as that offered by the classic SM-MIMO for maximizing the free distance (FD). However, our TPC scheme assigns the same number of bits to each time slot; hence, it is capable of avoiding the potential error propagation effects of ASM encountered in the case of ASM-mode signaling errors. Our simulation results show that the proposed TPC scheme considerably improves the system's performance compared with the conventional star-QAM-aided SM, the PA-aided SM, and ASM arrangements.

The remainder of this paper is organized as follows. In 137 Section II, we conceive a signaling constellation optimization 138 method for star-QAM-aided SM and elaborate both on the 139 choice of our optimization criterion and on the corresponding 140 optimization algorithm. In Section III, we propose a new TPC 141 scheme for enhancing the performance of the star-QAM-aided

SM. Our numerical analysis is carried out in Section IV. Finally, 142 our conclusions are presented in Section V. 143

II. SIGNALING CONSTELLATION OPTIMIZATION

A. Performance Metric and Star-QAM Constellation 145

Consider a flat-fading MIMO channel associated with N_t 146 transmit antennas (TAs) and N_r receive antennas. The $(N_t \times$ 147 1)-element transmit symbol vector \mathbf{x} is assumed to satisfy 148 $E[\mathbf{x}\mathbf{x}^H] = \mathbf{I}_{N_t}$, where \mathbf{I}_{N_t} denotes an $(N_t \times N_t)$ -element 149 identity matrix. Then, the transmitted SM symbol $\mathbf{x} \in \mathbb{C}^{N_t \times 1}$ 150 is given as $\mathbf{x} = s_l^n \mathbf{e}_n$ [21], where s_l^n is the complex-valued 151 symbol of the APM scheme employed at the nth TA. For 152 example, L-PSK/QAM is associated with $m_{\mathrm{APM}} = log_2(L)$ 153 input bits, whereas $\mathbf{e}_n(1 \leq n \leq N_t)$ is selected from the N_t - 154 dimensional standard basis vectors (i.e., $\mathbf{e}_1 = [1,0,\ldots,0]^T$), 155 according to $\log_2(N_t)$ input bits. The corresponding received 156 signal is given by

$$\mathbf{y} = \mathbf{H}\mathbf{x} + \mathbf{n} = \mathbf{h}_n s_l^n + \mathbf{n} \tag{1}$$

where ${\bf H}$ is an $(N_r \times N_t)$ -element channel matrix, ${\bf h}_n$ is the 158 nth column of ${\bf H}$, and the elements of the N_r -dimensional noise 159 vector ${\bf n}$ are Gaussian random variables obeying ${\cal CN}(0,\,N_0)$. 160 In [11], an improved union bound partitions the ABEP 161 expression of SM-MIMO systems into three terms: the $P_{\rm spatial}$ 162 term related to the TA index, the $P_{\rm signal}$ term related to the APM 163 signals, and the joint term $P_{\rm joint}$, which depends on both the TA 164 index and on the APM signals. This bound is formulated as

$$P_{\rm SM}(\rho) \le P_{\rm spatial}(\rho) + P_{\rm signal}(\rho) + P_{\rm joint}(\rho).$$
 (2)

This improved union bound is more accurate than the 166 conventional union-bound-based methods, hence facilitating a 167 deeper understanding of the joint impact of spatial and APM 168 signals, as illustrated in [11]. We focus our attention on the sys- 169 tem's performance for transmission over i.i.d. Rayleigh fading 170 channels, which may be readily extended to the Nakagami-m 171 fading model of [11]. Let us assume that ρ is the average SNR, 172 whereas x_l and $x_{\hat{l}}$ represent two different APM constellation 173 points, with their modulus values being given as β_l and $\beta_{\hat{l}}$, 174 respectively. Then, we have

$$P_{\text{signal}}(\rho) = \frac{\log_2(L)}{\log_2(N_t \cdot L)} P_{\text{APM}}(\rho)$$
 (3)

$$P_{\text{spatial}}(\rho) = \frac{\log_2(N_t)N_t}{2L\log_2(N_t \cdot L)} \sum_{l=1}^{L} \mathcal{F}\left(\rho\beta_l^2\right) \tag{4}$$

$$P_{\text{joint}}(\rho) = A \sum_{l=1}^{L} \sum_{\hat{i} \neq l-1}^{L} \left[B + CD_H \left(x_l \to x_{\hat{l}} \right) \right)$$

$$\times \mathcal{F}\left(\frac{\rho}{2}\left(\beta_l^2 + \beta_{\hat{l}}^2\right)\right].$$
 (5)

Here, $P_{\text{APM}}(\rho)$ represents the error probability of conventional 176 L-APM, which depends on the ED of the constellation points 177 of APM, whereas $D_H(x_l \to x_{\hat{l}})$ is the Hamming distance 178 between signals x_l and $x_{\hat{l}}$. Here, $A = 1/L \log(N_t \cdot L)$, $B = 179 N_t \log(N_t)/2$, and $C = (N_t - 1)$ are constants for a fixed 180

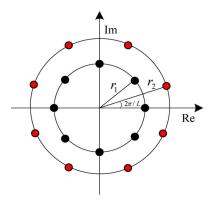


Fig. 1. Complex signal constellation of 16-star-QAM. The symbols are evenly distributed on two rings and the phase differences between the neighboring symbols on the same ring are equal.

181 MIMO setup. Moreover, the function $\mathcal{F}(\varepsilon)$ in (4) and (5) is the 182 pairwise error probability function [11], which is given by

$$\mathcal{F}(\varepsilon) = \gamma(\varepsilon)^{N_r} \sum_{n=0}^{N_r-1} {N_r - 1 + n \choose n} \left[1 - \gamma(\varepsilon)\right]^n \quad (6)$$

183 where we have $\gamma(\varepsilon) \stackrel{\Delta}{=} (1/2)(1-\sqrt{(\varepsilon/2+\varepsilon)})$. Note that the 184 ABEP bound of (2) was proposed for the general family of 185 APM schemes, which contains not only the conventional PSK 186 but also the generic rectangular nonsquare-QAM schemes and 187 the square-QAM schemes. Moreover, since P_{signal} is available 188 in closed form for conventional APM modulation schemes, the 189 bound of (2) is more accurate than the conventional results 190 of [21].

As indicated in (3)–(5), $P_{\rm signal}$ mainly depends on the mini-192 mum ED $d_{\rm min}$ of the APM constellation points, whereas $P_{\rm joint}$ 193 and $P_{\rm spatial}$ mainly depend on the modulus values β_l ($l=194,\ldots,L$) of the APM constellation points.

Note that the modulus values β_l are represented by the 196 Frobenius norms of the APM constellation points. These re-197 sults suggested that, for jointly minimizing $P_{\rm signal}$, $P_{\rm joint}$, and 198 $P_{\rm spatial}$, we can focus our attention on the design of $d_{\rm min}$ and 199 on the β_l parameters of APM.

To make the choice of the APM parameters d_{\min} and β_l as 201 flexible as possible, we consider a class of star-QAM constel-202 lations, which subsumes the classic PSK as a special case but 203 may also be configured for maximizing the minimum ED of 204 the constellation by appropriately adjusting the ring ratios of 205 the amplitude levels. For simplicity, we consider the example 206 of a twin-ring 16-star-QAM constellation having a ring ratio 207 of $\alpha = r_2/r_1$, as shown in Fig. 1. The symbols are evenly 208 distributed on the two rings, and the phase differences between 209 the neighboring symbols on the same ring are equal. Unlike the 210 conventional twin-ring star-QAM constellation [19], [28], the 211 constellation points on the outer circle of our proposed star-212 OAM constellation are rotated by $2\pi/L$ degrees compared 213 with the corresponding constellation points on the inner circle 214 [27]. Hence, again, the conventional PSK constitutes an integral 215 part of our star-QAM scheme, which is associated with $\alpha = 1$. 216 Table I summarizes the minimum EDs d_{\min} between the con-217 stellation points for different APM schemes. It is found that 218 this star-QAM scheme is capable of achieving almost the same

TABLE I
MINIMUM ED BETWEEN THE CONSTELLATION
POINTS FOR DIFFERENT APM SCHEMES

Modulation order	2	4 (MMD)	8 ([9])	16 (MMD)	32 ([9])
PSK	2	$\sqrt{2}$	0.7654	0.3902	0.1960
QAM		$\sqrt{2}$	0.8165	0.6325	0.4082
Proposed star-QAM	2	$\sqrt{2}$	0.9134	0.5737	0.3952

minimum ED as the MMD-based QAM. Note that, although 219 this twin-ring star-QAM constellation has been indeed applied 220 for noncoherent detection [27], it has not been considered 221 whether this constellation can be directly applied to SM for 222 achieving performance improvements.

The aforementioned twin-ring philosophy of Fig. 1 may be 224 readily extended to multiple-ring star-QAM. The reasons for 225 considering twin-ring star-QAM in our paper are the following. 226

- It is an attractive APM modulation candidate for SM, 227 exhibiting a high performance at low detection complexity 228 compared with conventional QAM schemes, as detailed in 229 [13]–[15].
- It can be flexibly designed for different d_{\min} and $\beta_l(l=231\ 1,\ldots,L)$ combinations, which is achieved by simply ad-232 justing a single parameter α , whereas β_l can assume two 233 values because only two rings are considered.
- The ABEP of star-QAM, which is related to the $P_{\rm spatial}$ 235 term of (3), has been documented in [28] and [29].

B. Optimization Criteria and Optimization Algorithm 237

Observe in Fig. 1 that there are numerous options for the 238 parameter α of the star-QAM constellation, for a given MIMO 239 setup, specified by the total number of bits per symbol $m_{\rm all}$, 240 the $(N_r \times N_t)$ configuration of transceiver, and the number of 241 modulation level L. The goal of star-QAM-aided signaling 242 AQ2 constellation optimization is to find the specific ring ratio α , 243 which minimizes the ABEP of the SM-MIMO of (2). Note that, 244 although the term $P_{\rm SM}(\rho)$ in (2) cannot be directly represented 245 by parameter α , it varies as a function of α , which may 246 be formulated as $P_{\rm SM}(\rho,\alpha)$. Following the aforementioned 247 approach, we formulated this optimization problem as

$$\begin{cases} \alpha^* = \min_{\alpha} P_{\text{SM}}(\rho, \alpha) \\ \text{s.t.} \quad \alpha > 1 \end{cases}$$
 (7)

which may be a convex one for a fixed SNR value ρ , as 249 indicated in Fig. 4. However, deriving the closed-form solu- 250 tion of (7) remains an open challenge since the expression of 251 $P_{\rm SM}(\rho,\alpha)$ depends both on the specific APM constellation and 252 on the particular MIMO setup [19], and since the expressions 253 of $P_{\rm signal}, P_{\rm joint}$ and $P_{\rm spatial}$ in (3)–(5) are complex. Hence, a 254 numerical search is adopted.

Our optimization algorithm conceived for finding the ring 256 ratio is summarized as follows.

Step 1: Initialize the values of N_r , N_t , $m_{\rm all}$, L, and the SNR 258 value ρ . Set the iteration step size to $\Delta \alpha = 0.1$ and the 259 number of iterations to n=1. The choice of $\Delta \alpha$ is flexible, 260 and a lower value of $\Delta \alpha$ may lead to a better performance. 261 We then set the search area of α to $1 \le \alpha \le U_\alpha$ and the 262 performance metric to $P_{\rm iter}(n) = 0$.

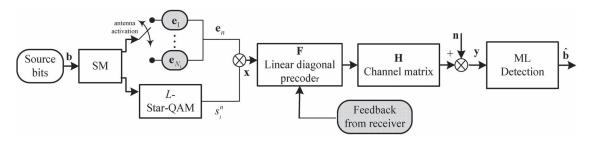


Fig. 2. System model of the diagonal-precoding-assisted star-QAM-aided SM scheme.

264 Step 2: While $\alpha \leq U_{\alpha}$, let $\Delta \hat{\alpha} = \min\{\Delta \hat{\alpha}, U_{\alpha} - \alpha\}$, and calculate the probabilities of $P_{\text{signal}}, P_{\text{joint}}$, and P_{spatial} by using (3)–(5) associated with α . Then, let $P_{\text{iter}}(n) = P_{\text{SM}}(\rho)$ using (2), and set $\alpha = \alpha + \Delta \hat{\alpha}$ and n = n + 1.

268 Step 3: Find the index $n^* = \min_n \{P_{\text{iter}}(n)\}$ to achieve the optimal ring ratio of $\alpha^* = 1 + (n^* - 1)\Delta\hat{\alpha}$.

In the aforementioned optimization algorithm, we have to 271 choose an appropriate U_{α} to promptly find the optimal α^* . 272 More explicitly, an excessively low value of U_{α} may lead 273 to missing the optimal solution, whereas an excessively high 274 value of U_{α} imposes excessive computational complexity on 275 the optimization process. Hence, we will show in Section III 276 that $U_{\alpha}=3$ is a beneficial choice for promptly approaching 277 the optimal results. Moreover, the optimum ring ratio α^* is a 278 function of the SNR. However, we will show that the optimum 279 ratio approaches its asymptotic optimum as the SNR increases.

280 III. PROPOSED DIAGONAL PRECODING FOR 281 STAR-QUADRATURE AMPLITUDE MODULATION-AIDED 282 SPATIAL MODUALTION

Since the performance of the optimum maximum-likelihood 283 284 (ML) receiver depends on the FD of the received signal con-285 stellation [30], we propose a new TPC based on maximizing 286 the FD for the family of star-QAM-aided SM-MIMO systems, 287 when limited channel state information is available at the 288 transmitter. Since the FD is increased by the TPC algorithm, 289 the proposed scheme is expected to provide a beneficial system 290 performance improvement. To retain all the single-RF-related 291 benefits of SM, we design the TPC matrix P to be diagonal. 292 The system model of the diagonal-TPC-assisted star-QAM-293 aided SM scheme is shown in Fig. 2. To identify the specific 294 TPC parameters, which are capable of maximizing the FD, 295 we propose a low-complexity TPC design algorithm. We will 296 demonstrate that as few as two elements of the diagonal TPC 297 matrix have to be fed back to the transmitter, regardless of N_t .

298 A. TPC Design Criterion

To construct a TPC for star-QAM-aided SM-MIMO systems, 300 we can rewrite the system model of (1) as

$$y = HPx + n \tag{8}$$

301 where ${\bf P}$ denotes the diagonal TPC matrix, which can be 302 represented as

$$\mathbf{P} = \operatorname{diag}\{p_1, \dots, p_n, \dots, p_{N_t}\}\tag{9}$$

where p_n controls the channel gain associated with x_n . Here, 303 we let $\sum_{n=1}^{N_t} |p_n|^2 = N_t$ for normalizing the transmit power. 304 Note that the introduction of TPC in SM does not affect the 305 advantages of SM, such as the avoidance of the interantenna 306 interference and the reliance on a single RF chain, because the 307 precoded transmit vector $\mathbf{P}\mathbf{x}$ includes only a single nonzero 308 component; hence, only a single TA is activated in each time 309 slot, as indicated in (8).

Numerous techniques may be invoked for constructing the 311 TPC **P** [21], [25]. In this paper, similar to the precoding 312 methods conceived for the orthogonalized spatial multiplexing 313 of [31], we decompose **P** as

$$\mathbf{P} = \bar{\mathbf{P}}\mathbf{\Theta} = \operatorname{diag}\left\{\bar{p}_1 e^{j\theta_1}, \dots, \bar{p}_n e^{j\theta_n}, \dots, \bar{p}_{N_t} e^{j\theta_{N_t}}\right\}$$
(10)

where $\bar{\mathbf{P}} = \mathrm{diag}\{\bar{p}_1,\ldots,\bar{p}_n,\ldots,\bar{p}_{N_t}\}$ represents the PA ma- 315 trix, whereas $\boldsymbol{\Theta} = \mathrm{diag}\{e^{j\theta_1},\ldots,e^{j\theta_n},\ldots,e^{j\theta_{N_t}}\}$ is the phase 316 rotation matrix. The FD between the constellation points at the 317 receiver is defined as

$$d_{\min}(\mathbf{H}, \mathbf{P}) = \min_{\substack{\mathbf{x}_i, \mathbf{x}_j \in \mathbb{X}, \\ \mathbf{x}_i \neq \mathbf{x}_j}} \|\mathbf{H} \mathbf{P}(\mathbf{x}_i - \mathbf{x}_j)\|_F$$
$$= \min_{\mathbf{e}_{ij} \in \mathbb{E}} \|\mathbf{H} \bar{\mathbf{P}} \mathbf{\Theta} \mathbf{e}_{ij}\|_F$$
(11)

where \mathbb{X} is the set of all legitimate transmit symbols, $\mathbf{e}_{ij} = 319$ $\mathbf{x}_i - \mathbf{x}_j$, $i \neq j$ denotes the error vector, and \mathbb{E} is a set of error 320 vectors. Then, we design the TPC \mathbf{P} by maximizing the FD 321 with the aid of the following criterion:

$$\begin{cases}
\mathbf{P}_{\text{opt}} = \arg\max d_{\min}(\mathbf{H}, \mathbf{P}) \\
\text{s.t.} \quad \sum_{n=1}^{N_t} |p_n|^2 = N_t; \quad p_n \in C; \\
\theta_n \in (0, 2\pi]; \quad n = 1, \dots, N_t.
\end{cases}$$
(12)

Note that, since the attainable performance of the optimum 323 single-stream ML receiver depends on the FD of the received 324 signal constellation [30], the maximization of the FD directly 325 reduces the probability of error. Let $\mathbf{x}_i = s_l^i \mathbf{e}_i$ and $\mathbf{x}_j = s_k^j \mathbf{e}_j$ 326 denote two different transmit symbols, whereas s_l^i and s_k^j 327 denote the constellation points l and k represented by the ith 328 and jth antennas, respectively. Then, the FD of (11) can be 329 represented as (13), where $\phi = \angle((s_l^i)^* s_k^j) = -(s_l^i (s_k^j)^*)$. In 330

¹Because the conventional PSK-and-QAM-aided SM scheme's performance is worse than that of the proposed star-QAM-aided SM, we only invoked the TPC algorithm for the star-QAM-aided SM for the sake of achieving further performance improvements. However, it is worth noting that the proposed TPC algorithm is also suitable for SM in conjunction with both conventional PSK and QAM schemes.

331 the ASM scheme of [7], only the APM modulation orders to 332 be used by the transmitter are adapted, i.e., only the elements 333 $|s_l^i|$, $|s_k^j|$, and ϕ of (13), shown at the bottom of the page, are 334 dynamically adapted to the channel conditions, and the legit-335 imate values of these elements are selected from the discrete 336 set depending on the modulation order set utilized. By contrast, 337 our proposed scheme adjusts all the TPC elements $|p_i|$, $|p_j|$, 338 θ_i , and θ_i of (13) for maximizing the FD $d_{\min}(\mathbf{H}, \mathbf{P})$, whose 339 legitimate values are drawn from the real-valued number field. 340 Based on these observations and on (13), the proposed scheme 341 and the ASM scheme may exploit the same degrees of freedom 342 as that offered by the SM-MIMO in terms of maximizing the 343 FD. However, unlike the ASM scheme of [7] and [15], our 344 proposed scheme assigns the same number of bits to each time 345 slot; hence, the potential error propagation effects experienced 346 in ASM are avoided.

347 B. Low-Complexity TPC Design Algorithm

To identify the specific TPC matrix P, which is capable of 349 maximizing the FD, we have to determine all the N_t parameters 350 $p_n(n=1,\ldots,N_t)$. Since it may become excessively complex 351 to jointly optimize these N_t parameters in the complex-valued 352 field, we propose a low-complexity precoder design algorithm. 353 Similar to the one-bit reallocation algorithm designed for ASM 354 in [15], only the specific TA pair associated with the FD is con-355 sidered, and the TPC parameters are selected for appropriately 356 weighting the SM symbols because the FD of this particular 357 TA pair predominantly determines the achievable performance. 358 The calculation of the TPC matrix is summarized in Fig. 3. To be specific, given the channel matrix H, the indexes of 360 the TA pair (g, k) associated with the FD $d_{\min}(\mathbf{H})$ can be 361 found with the aid of the flowchart shown in Fig. 3. To offer 362 an increased FD, the precoding parameters of this TA pair can 363 be dynamically adapted. Note that, if the value of g is the same 364 as k, it is plausible that the TA g has the smallest channel gain. 365 In this case, the phase rotation elements of (10) do not have to 366 be considered because this would not increase the FD of (13). 367 To increase the FD, we only consider the PA matrix of (10) 368 and may deduct some power from the TA u having the highest 369 channel gain, which may hence be reassigned it to the TA g. 370 As a result, p_u and p_g have to be optimized. On the other hand, 371 if the value of g and k is not the same, parameters p_a and p_k 372 have to be calculated. Overall, there are only two parameters, 373 namely, p_q and p_k , $(p_u$ for g = k) that have to be searched 374 for. Finding the optimal values of p_g and p_k as a function of

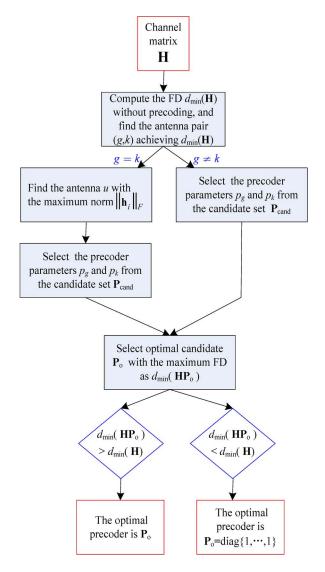


Fig. 3. Calculation of the diagonal precoding matrix for star-QAM-aided SM-MIMO.

both ${\bf H}$ and of the optimal transmit parameters involves an 375 exhaustive search over the vast design space of $\bar p_g$, $\bar p_k$, θ_g , and 376 θ_k of (10), which is overly complex. To reduce the complexity, 377 according to (12), the power of the TA pair (g,k) satisfies the 378 constraint $\bar p_k^2 + \bar p_g^2 = 2$; hence, only the element $\bar p_k$ has to be 379 searched for in the power matrix $\bar {\bf P}$ of (10). Moreover, since 380 the phase rotation of the symbol is only carried by two TAs 381 and their phase difference is correlated, we can simplify the 382 computations by fixing $\theta_k = 1$ and then finding the optimal 383

$$d_{\min}(\mathbf{H}, \mathbf{P}) = \min_{s_l^j, s_k^j \in S} \left\| \mathbf{H} \mathbf{P} \left(s_l^i \mathbf{e}_i - s_k^j \mathbf{e}_j \right) \right\|_F$$

$$= \min_{s_l^j, s_k^j \in S} \left\| \left(\mathbf{h}_i p_i s_l^i - \mathbf{h}_j p_j s_k^j \right) \right\|_F$$

$$= \min_{s_l^j, s_k^j \in S} \sqrt{\left| s_l^i \right|^2 |p_i|^2 \mathbf{h}_i^H \mathbf{h}_i + \left| s_k^j \right|^2 |p_j|^2 \mathbf{h}_j^H \mathbf{h}_j - 2|p_i||p_j| \left| s_l^i \right| \left| s_k^j \right| \operatorname{Re} \left\{ \mathbf{h}_i^H \mathbf{h}_j e^{j(\phi - \theta_i + \theta_j)} \right\}}$$
(13)

384 θ_g . This implies that only the phase parameter θ_g has to be 385 optimized for the phase matrix Θ . In Fig. 3, a numerical search 386 is used for varying \bar{p}_g and θ_g in small steps. Note that we 387 have $0 \leq \bar{p}_g \leq \sqrt{2}$ and $0 \leq \theta_g \leq 2\pi$ according to (12). For our 388 numerical search, we have assumed

$$\begin{cases}
\bar{p}_g = \sqrt{2}/V_1 * v_1, & v_1 = 0, \dots, V_1 \\
\theta_g = 2\pi/V_2 * v_2, & v_2 = 0, \dots, V_2
\end{cases}$$
(14)

389 where V_1 and V_2 represent the number of quantization steps and 390 can be flexibly selected according to the prevalent performance 391 requirements. As a result, the corresponding diagonal TPC 392 matrix candidates are

$$\mathbf{P}_{\text{cand}} = \operatorname{diag} \left\{ 1, \dots, \bar{p}_g e^{j\theta_g}, \dots, \sqrt{2 - \bar{p}_g^2}, \dots, 1 \right\}$$

$$\uparrow g \text{th} \qquad \uparrow k \text{th.} \tag{15}$$

393 Upon denoting the quantized TPC matrix ${\bf P}$ as ${\bf P}_{\rm cand}$, the 394 optimization problem of (12) is reformulated as

$$\mathbf{P}_{\text{opt}} = \underset{\{\mathbf{P} \in \mathbf{P}_{\text{eand}}, \mathbf{P}_{\text{I}}\}}{\arg \max} d_{\min}(\mathbf{H}, \mathbf{P}). \tag{16}$$

395 where we have $\mathbf{P_I} = \mathbf{I}_{N_t}$. In (16), the FD of the TPC matrices 396 $\mathbf{P}_{\mathrm{cand}}$ generated will be compared with that of the conventional 397 scheme associated with $\mathbf{P_I}$, and then we select the one having 398 the largest FD as our final result. The receiver determines the 399 optimal diagonal TPC matrix based on (16) and feeds back the 400 TA indexes and their TPC parameters to the transmitter. Since 401 only the specific TA pair, which predominantly determines 402 the achievable performance, is considered, the proposed low-403 complexity algorithm can be readily extended to a high number 404 of TAs.

405 IV. SIMULATION RESULTS

Here, we characterize the performance of both the proposed 406 407 star-QAM-aided SM scheme and of the corresponding TPC 408 scheme, and compare it with that of the conventional OAM-409 modulated SM schemes, with the PSK-modulated SM schemes 410 and with the ASM schemes [15] for transmission over inde-411 pendent Rayleigh block-flat MIMO channels. It is assumed that 412 the receiver is capable of perfect phase and gain tracking, i.e., 413 of perfect channel estimation. In practice, pilot symbols are 414 used for estimating the MIMO channel; hence, the estimated 415 channel matrix will inevitably be imperfect. To alleviate the 416 effects of channel estimation errors, the joint channel estimation 417 and data detection algorithm of [32] may be considered in the 418 proposed schemes, where the channel estimator and the data 419 detector iteratively exchange their information. We consider 420 two practical MIMO systems here, namely, (2×2) and (4×2) 421 4) MIMO systems. Moreover, in the TPC design algorithm, we 422 select $V_1 = V_2 = 5$ for simplicity.²

423 Fig. 4 shows the optimal ring ratios of star-QAM-aided 424 SM relying on (4×4) elements for a different number of 425 modulation levels L, where the optimal ring ratio α^* is seen 426 to be a function of the SNR. The bound of (2) is well suited

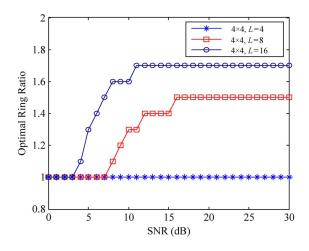


Fig. 4. Optimal ring ratios of star-QAM-aided SM with (4×4) MIMO for different numbers of modulation levels L.

for numerically optimizing the ring ratio, particularly in the 427 high-SNR region. Observe in Fig. 4 that the optimal ratios 428 approach their asymptotic values, as the SNR increases. This 429 is expected since the bound of (2) is also asymptotically tight 430 and the probability of an error event in slow fading associated 431 with ML detection is dominated by the minimum-distance error 432 event at high values of the SNR. Moreover, the optimal ring 433 ratios are different for different MIMO parameters.

Since the transmitter operates at a fixed ring ratio, we have 435 opted for the asymptotic ring-ratio value for the evaluation 436 of the BER. For example, we have chosen the optimal ring 437 ratio $\alpha^*=1.7$ for the 16-star-QAM-aided (4 × 4) SM-MIMO, 438 according to the results in Fig. 4. This result may be readily 439 extended to other star-QAM-aided SM scenarios, such as the (4 440 × 4)-element star-QAM-aided SM schemes using L=4, 8 in 441 Fig. 4.

In Figs. 5 and 6, we compare various SM-MIMO systems 443 relying on diverse MIMO parameters and modulation orders. 444 First, in Figs. 5 and 6, we depict the BER performance 445 of the conventional QAM-modulated SM schemes, of the 446 PSK-modulated SM arrangements, and of the proposed star- 447 QAM-aided SM scheme. Note that the optimized star-QAM 448 constellation is designed offline for different SM-MIMO sys- 449 tems. Hence, the resultant system does not need any feedback. 450 To be specific, we may create a parameter lookup table for 451 the star-QAM SM schemes associated with the MIMO setups 452 considered; hence, the complexity of the optimal ring-ratio 453 search process detailed in Section II is negligible. For com- 454 pleteness, we also included the theoretical upper bound [30] 455 for the family of conventional SM schemes. We found that 456 the conventional QAM-modulated SM scheme outperforms its 457 identical-throughput PSK counterpart for a (4 × 4)-element 458 MIMO channel in Fig. 5, whereas the PSK scheme is preferred 459 for a (2×2) -element MIMO channel in Fig. 6. This indicates 460 that the best choice of the APM scheme depends on the specific 461 SM parameters, such as the MIMO setup and throughput. 462 Moreover, as shown in Fig. 5, the optimized star-QAM-aided 463 SM scheme provides an SNR gain of about 3 dB at BER = 464 10⁻⁵ over the conventional 16-PSK-modulated SM scheme and 465 an SNR gain of about 1.1 dB over the identical-throughput 466

 $^{^2}$ Note that the values of V_1 and V_2 can be different. Moreover, the selection of V_1 and V_2 is flexible, and higher values of V_1 and V_2 may lead to better performance at the cost of a higher TPC design complexity.

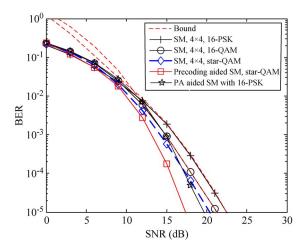


Fig. 5. BER performance of various SM-MIMO schemes operating in a (4 \times 4) MIMO channel at a total throughput of 6 b/s. Since the transmitter operates with a fixed ring ratio, we have chosen the asymptotic ring-ratio value for the evaluation of star-OAM-aided schemes. Here, α is chosen as $\alpha = 1.7$.

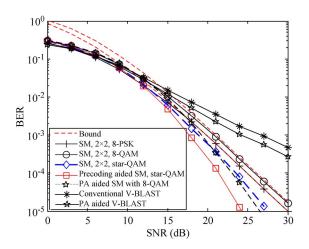


Fig. 6. BER performance of various SM schemes operating in (2×2) MIMO channel at a total throughput of 4 b/s. Here, α is chosen as $\alpha = 1.5$.

467 Gray-coded MMD 16-QAM SM scheme. This advantage of the 468 optimized star-QAM scheme recorded for SM-MIMO is also 469 visible in Fig. 6.

Moreover, in Figs. 5 and 6, we also compare the 471 achievable BER performance of the limited-feedback-aided 472 ASM schemes. To be specific, two diagonal-precoding-aided 473 schemes, namely, the precoding-assisted star-QAM-based SM 474 schemes and the PA-aided SM schemes of [33] are compared. 475 For simplicity, the PA algorithm is only applied to the non-476 ASM schemes exhibiting an inferior performance in Figs. 5 477 and 6, namely, to the conventional (4×4) -element SM using 478 16-PSK and (2×2) -element SM employing 8-QAM. Note that 479 the (4 \times 4)-element SM associated with 16-QAM and (2 \times 480 2)-element SM employing 8-PSK can also use the PA regime 481 to attain a BER improvement. Due to space limitations, these 482 results are not presented here. As shown in Figs. 5 and 6, the 483 proposed TPC schemes provide a gain of 2.5-3 dB at the BER 484 of 10^{-5} over the PA-aided SM schemes. This is because PA-485 aided SM may be viewed as a special case of the proposed 486 precoding-aided SM created by only considering the PA matrix 487 in (10). To be specific, compared with the PA-aided SM of

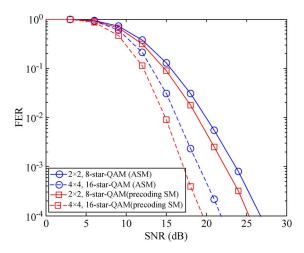


Fig. 7. FER performance of the proposed precoding star-QAM-aided SM and the ASM schemes at total throughputs of 4 and 6 b/s.

[33], our precoding-based SM regime jointly adapts the power 488 and the phases of the transmit signals and hence improves the 489 achievable BER performance.

Furthermore, in Fig. 6, we compare the QPSK-modulated 491 V-BLAST scheme and its PA-aided counterpart associated 492 with a zero-forcing-based successive interference cancelation 493 (ZF-SIC) detector [18] as the benchmarkers because their 494 detection complexity is similar to that of the single-stream 495 ML-based SM schemes. Observe in Fig. 6 for $m_{\rm all}=4$ b/s that 496 our TPC-aided SM scheme outperforms the PA-aided VBLAST 497 arrangement relying on a ZF-SIC detector. Indeed, if a powerful 498 ML detector is employed for the VBLAST system, we can 499 achieve a better BER performance. However, designing PA 500 algorithms for ML-based VBLAST systems is a challenge, and 501 their detection complexity is high, as indicated in [34].

Fig. 7 shows the frame error rate (FER) of both the proposed 503 precoded star-QAM-aided SM scheme and of the ASM scheme 504 [15]. The transmission frame size is $L_F = 60$ b. 3 Note that, 505 although the proposed scheme and the ASM scheme exploit 506 the same degrees of freedom offered by the SM-MIMO for 507 improving the performance, our proposed scheme is capable 508 of avoiding the error propagation effects often experienced in 509 ASM, owing to ASM-mode signaling errors. Moreover, the 510 selection of TPC parameters is more flexible than that of ASM 511 because the modulation orders of ASM are selected from a 512 discrete set, whereas the TPC parameters are chosen from the 513 complex-valued field. As expected, the performance gain of 514 the proposed scheme over ASM is seen to be about 2 dB at 515 FER = 10^{-3} in Fig. 7.

V. CONCLUSION 517

In this paper, we have investigated the problem of designing 518 APM constellations that minimize the SM system's ABEP. 519 We considered a class of star-QAM constellations, which is 520

³Here, we assume that the channel matrix remains constant within each transmit frame and consider the FER performance of these schemes. Note that the ASM schemes often suffer from error-propagation effects, as indicated in Section I. Hence, using the FER comparison of the ASM and TPC-aided SM schemes may be more suitable than the BER metric.

521 capable of flexibly adapting the ring ratios. We formulated 522 the constellation design problem as an optimization problem 523 and conceived an efficient iterative constellation-optimization 524 method. Moreover, a diagonal TPC technique was proposed 525 for the optimized star-QAM-aided SM to attain an improved 526 performance. The simulation results confirm that our proposed 527 optimized star-QAM-aided SM scheme outperforms the con-528 ventional PSK/QAM schemes. Moreover, our TPC method also 529 exhibits an attractive BER/FER performance. For achieving an 530 improved performance for a high number of bits per symbol, 531 our further work will be focused on the integration of GSM and 532 channel coding into the proposed TPC schemes.

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Star-QAM Signaling Constellations for Spatial Modulation

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Abstract—The performance of spatial modulation (SM)-assisted 6 multiple-input-multiple-output (MIMO) communication systems 7 is highly dependent on the specific amplitude/phase modulation 8 (APM) signal constellation adopted. In this paper, we conceive 9 new star-quadrature amplitude modulation (star-QAM)-aided SM 10 schemes. Our goal is to minimize the system's average bit error 11 probability (ABEP). More specifically, a new class of star-QAM 12 constellations is introduced for SM, which is capable of flexi-13 bly adapting ring ratios of the amplitude levels. Then, under a 14 specific MIMO configuration and a predetermined transmission 15 rate, a simple and efficient ring-ratio optimization algorithm is 16 proposed to minimize the ABEP. Moreover, to improve further 17 the performance of our star-QAM-aided SM scheme, a diagonal 18 precoding technique is proposed, and a low-complexity minimum-19 distance-based approach is conceived for extracting the precod-20 ing parameters. Our numerical results show that the proposed 21 star-QAM-aided SM arrangement provides beneficial system per-22 formance improvements compared with the identical-throughput 23 maximum-minimum distance (MMD) QAM and phase-shift key-24 ing (PSK) benchmarkers. Moreover, our precoding scheme is 25 capable of further improving the attainable system performance 26 at a modest feedback requirement.

27 *Index Terms*—Constellation optimization, multiple-input—28 multiple-output (MIMO), spatial modulation (SM), star-29 quadrature amplitude modulation (star-QAM).

I. Introduction

31 S PATIAL MODULATION (SM), which maps the informa-32 S tion bits to two information-carrying entities, namely the an-33 tenna indexes and the combined amplitude/phase modulation 34 (APM) constellation, constitutes a promising low-complexity 35 multiple-input-multiple-output (MIMO) transmission tech-36 nique [1]–[8]. In a conventional single-input-single-output 37 (SISO) system, the Gray-coded maximum-minimum distance

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(MMD) quadrature amplitude modulation (QAM) constellation 38 minimizes the bit error rate (BER) [9], [10]. However, the 39 advantage of MMD-QAM may be eroded in SM-MIMO sys- 40 tems [11]. This is due to the fact that the BER performance of 41 SM-MIMO systems is jointly determined by the spatial signal 42 (i.e., antenna indexes), by the classic APM constellation, and 43 by their interaction [11]–[18].

Recently, the effects of APM schemes on the performance 45 of SM have been investigated in [11], [14], and [18]. More 46 specifically, in [11], the performance of SM systems relying 47 both on conventional QAM and PSK modulation was studied, 48 demonstrating that, in some MIMO setups, the PSK-modulated 49 SM scheme may outperform the identical-throughput MMD- 50 QAM-aided SM scheme. In [18], the dispersion matrices and 51 the signal constellations were jointly optimized for a near- 52 capacity irregular precoded space-time shift keying (STSK) 53 system, which includes SM as a special case and strikes a 54 flexible rate-diversity tradeoff. It was also shown in [14] that 55 the star-QAM-aided STSK scheme outperforms its MMD-56 based square-QAM-aided counterpart. This observation may 57 be also valid for SM systems [11]. The aforementioned results 58 indicated that the performance of SM is highly dependent on 59 the specific APM adopted; hence, a suitable APM scheme has 60 to be designed for this hybrid modulation scheme.

On the other hand, star-QAM constitutes a special case of 62 circular amplitude- and phase-shift keying, which is capable of 63 outperforming the classic square-QAM constellation in peak- 64 power-limited systems [19]. Hence, it has been adopted in most 65 of the recent satellite communication standards, such as in 66 the Digital Video Broadcast System (DVB) S2, DVB-SH, and 67 the Internet Protocol over Satellite and Advanced Broadcasting 68 System via Satellite [19]. The star-QAM constellation is com- 69 posed of multiple concentric circles, and it was shown to be 70 beneficial in the context of STSK systems. Hence, star-QAM 71 may be an attractive APM candidate for SM-MIMO. However, 72 the constellations' optimization has not been carried out for 73 star-QAM-aided SM.

Moreover, to increase the robustness of the SM-MIMO sys-75 tem, limited-feedback-aided link adaptation schemes have been 76 proposed in [20]–[26]. For example, in [20], an opportunistic 77 power-allocation (PA) scheme was conceived for achieving a 78 beneficial transmit diversity gain in SM-MIMO systems. In 79 [21], a beamforming codebook was designed for optimizing the 80 coding gain of SM-MIMO based on the knowledge of the chan-81 nel envelope's spatial correlation. Recently, an adaptive closed-82 loop-aided method was invoked for providing both diversity 83 and coding gains in the context of space-shift keying (SSK)[22], 84

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85 which is a special case of SM. However, the scheme proposed 86 for SSK may not be directly applicable to the conventional 87 SM scheme. Moreover, ASM-MIMO architectures relying on 88 different combinations of modulation schemes were proposed 89 in [24], which aimed for maximizing the channel capacity at a 90 predefined target BER, rather than for minimizing the BER. In 91 contrast, in [25] and [26], a transmit precoding (TPC) technique 92 was used for improving the modulated signal design for SM. 93 However, this technique may only be suitable for a new class of 94 SM relying on a single-receiver antenna. For the conventional 95 SM, we proposed a near-instantaneously adaptive-modulation-96 aided scheme for minimizing the BER [7], which was termed 97 adaptive SM (ASM). Then, we further generalized this paper in 98 [12] and [15], where the implementation complexity of ASM 99 was considerably reduced. However, ASM typically transmits 100 a different number of bits in the different-quality time slots, 101 which may be inconvenient in fixed-rate applications and po-102 tentially leads to error propagation in the case of ASM-mode 103 signaling errors.

104 Against this background, the novel contributions of this 105 paper are threefold.

- We introduced the class of star-QAM constellations [27], which is capable of flexibly adapting the ring ratios, hence subsuming classic PSK as a special case. Alternatively, if the ring ratio is appropriately selected, the proposed star-QAM is capable of achieving almost the same Euclidean distance (ED) as the MMD-based QAM.
- Given a specific MIMO configuration and a predetermined 112 transmission rate, a low-complexity yet efficient optimiza-113 114 tion algorithm is proposed to minimize the average bit error probability (ABEP) of SM-MIMO systems, where 115 the effects of both the antenna index, as well as of the APM 116 signal and their interaction, are jointly considered. Only 117 118 the optimal ring ratios of star-QAM constellation have to be found by the optimization algorithm. 119
 - We introduce a new TPC scheme for star-QAM-aided SM-MIMO systems, which further improves the performance. To retain the benefits of SM, such as its low-complexity single-stream detector and its single RF chain, we design its TPC matrix P to be diagonal. We demonstrate that this precoded scheme and the ASM schemes of [12] and [15] are capable of exploiting the same degrees of freedom as that offered by the classic SM-MIMO for maximizing the free distance (FD). However, our TPC scheme assigns the same number of bits to each time slot; hence, it is capable of avoiding the potential error propagation effects of ASM encountered in the case of ASM-mode signaling errors. Our simulation results show that the proposed TPC scheme considerably improves the system's performance compared with the conventional star-QAM-aided SM, the PA-aided SM, and ASM arrangements.

The remainder of this paper is organized as follows. In 137 Section II, we conceive a signaling constellation optimization 138 method for star-QAM-aided SM and elaborate both on the 139 choice of our optimization criterion and on the corresponding 140 optimization algorithm. In Section III, we propose a new TPC 141 scheme for enhancing the performance of the star-QAM-aided

SM. Our numerical analysis is carried out in Section IV. Finally, 142 our conclusions are presented in Section V. 143

II. SIGNALING CONSTELLATION OPTIMIZATION

A. Performance Metric and Star-QAM Constellation 145

Consider a flat-fading MIMO channel associated with N_t 146 transmit antennas (TAs) and N_r receive antennas. The $(N_t \times$ 147 1)-element transmit symbol vector \mathbf{x} is assumed to satisfy 148 $E[\mathbf{x}\mathbf{x}^H] = \mathbf{I}_{N_t}$, where \mathbf{I}_{N_t} denotes an $(N_t \times N_t)$ -element 149 identity matrix. Then, the transmitted SM symbol $\mathbf{x} \in \mathbb{C}^{N_t \times 1}$ 150 is given as $\mathbf{x} = s_l^n \mathbf{e}_n$ [21], where s_l^n is the complex-valued 151 symbol of the APM scheme employed at the nth TA. For 152 example, L-PSK/QAM is associated with $m_{\mathrm{APM}} = log_2(L)$ 153 input bits, whereas $\mathbf{e}_n(1 \leq n \leq N_t)$ is selected from the N_t - 154 dimensional standard basis vectors (i.e., $\mathbf{e}_1 = [1,0,\ldots,0]^T$), 155 according to $\log_2(N_t)$ input bits. The corresponding received 156 signal is given by

$$\mathbf{y} = \mathbf{H}\mathbf{x} + \mathbf{n} = \mathbf{h}_n s_l^n + \mathbf{n} \tag{1}$$

where ${\bf H}$ is an $(N_r \times N_t)$ -element channel matrix, ${\bf h}_n$ is the 158 nth column of ${\bf H}$, and the elements of the N_r -dimensional noise 159 vector ${\bf n}$ are Gaussian random variables obeying ${\cal CN}(0,\,N_0)$. 160 In [11], an improved union bound partitions the ABEP 161 expression of SM-MIMO systems into three terms: the $P_{\rm spatial}$ 162 term related to the TA index, the $P_{\rm signal}$ term related to the APM 163 signals, and the joint term $P_{\rm joint}$, which depends on both the TA 164 index and on the APM signals. This bound is formulated as

$$P_{\rm SM}(\rho) \le P_{\rm spatial}(\rho) + P_{\rm signal}(\rho) + P_{\rm joint}(\rho).$$
 (2)

This improved union bound is more accurate than the 166 conventional union-bound-based methods, hence facilitating a 167 deeper understanding of the joint impact of spatial and APM 168 signals, as illustrated in [11]. We focus our attention on the sys- 169 tem's performance for transmission over i.i.d. Rayleigh fading 170 channels, which may be readily extended to the Nakagami-m 171 fading model of [11]. Let us assume that ρ is the average SNR, 172 whereas x_l and $x_{\hat{l}}$ represent two different APM constellation 173 points, with their modulus values being given as β_l and $\beta_{\hat{l}}$, 174 respectively. Then, we have

$$P_{\text{signal}}(\rho) = \frac{\log_2(L)}{\log_2(N_t \cdot L)} P_{\text{APM}}(\rho)$$
 (3)

$$P_{\text{spatial}}(\rho) = \frac{\log_2(N_t)N_t}{2L\log_2(N_t \cdot L)} \sum_{l=1}^{L} \mathcal{F}\left(\rho\beta_l^2\right) \tag{4}$$

$$P_{\text{joint}}(\rho) = A \sum_{l=1}^{L} \sum_{\hat{i} \neq l-1}^{L} \left[B + CD_H \left(x_l \to x_{\hat{l}} \right) \right)$$

$$\times \mathcal{F}\left(\frac{\rho}{2}\left(\beta_l^2 + \beta_{\hat{l}}^2\right)\right].$$
 (5)

Here, $P_{\text{APM}}(\rho)$ represents the error probability of conventional 176 L-APM, which depends on the ED of the constellation points 177 of APM, whereas $D_H(x_l \to x_{\hat{l}})$ is the Hamming distance 178 between signals x_l and $x_{\hat{l}}$. Here, $A = 1/L \log(N_t \cdot L)$, $B = 179 N_t \log(N_t)/2$, and $C = (N_t - 1)$ are constants for a fixed 180

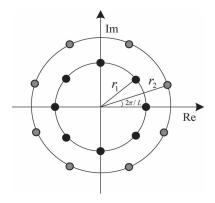


Fig. 1. Complex signal constellation of 16-star-QAM. The symbols are evenly distributed on two rings and the phase differences between the neighboring symbols on the same ring are equal.

181 MIMO setup. Moreover, the function $\mathcal{F}(\varepsilon)$ in (4) and (5) is the 182 pairwise error probability function [11], which is given by

$$\mathcal{F}(\varepsilon) = \gamma(\varepsilon)^{N_r} \sum_{n=0}^{N_r - 1} {N_r - 1 + n \choose n} \left[1 - \gamma(\varepsilon)\right]^n \quad (6)$$

183 where we have $\gamma(\varepsilon) \stackrel{\Delta}{=} (1/2)(1-\sqrt{(\varepsilon/2+\varepsilon)})$. Note that the 184 ABEP bound of (2) was proposed for the general family of 185 APM schemes, which contains not only the conventional PSK 186 but also the generic rectangular nonsquare-QAM schemes and 187 the square-QAM schemes. Moreover, since P_{signal} is available 188 in closed form for conventional APM modulation schemes, the 189 bound of (2) is more accurate than the conventional results 190 of [21].

As indicated in (3)–(5), $P_{\rm signal}$ mainly depends on the mini-192 mum ED $d_{\rm min}$ of the APM constellation points, whereas $P_{\rm joint}$ 193 and $P_{\rm spatial}$ mainly depend on the modulus values β_l ($l=194,\ldots,L$) of the APM constellation points.

Note that the modulus values β_l are represented by the 196 Frobenius norms of the APM constellation points. These re-197 sults suggested that, for jointly minimizing $P_{\rm signal}$, $P_{\rm joint}$, and 198 $P_{\rm spatial}$, we can focus our attention on the design of $d_{\rm min}$ and 199 on the β_l parameters of APM.

To make the choice of the APM parameters d_{\min} and β_l as 201 flexible as possible, we consider a class of star-QAM constel-202 lations, which subsumes the classic PSK as a special case but 203 may also be configured for maximizing the minimum ED of 204 the constellation by appropriately adjusting the ring ratios of 205 the amplitude levels. For simplicity, we consider the example 206 of a twin-ring 16-star-QAM constellation having a ring ratio 207 of $\alpha = r_2/r_1$, as shown in Fig. 1. The symbols are evenly 208 distributed on the two rings, and the phase differences between 209 the neighboring symbols on the same ring are equal. Unlike the 210 conventional twin-ring star-QAM constellation [19], [28], the 211 constellation points on the outer circle of our proposed star-212 OAM constellation are rotated by $2\pi/L$ degrees compared 213 with the corresponding constellation points on the inner circle 214 [27]. Hence, again, the conventional PSK constitutes an integral 215 part of our star-QAM scheme, which is associated with $\alpha = 1$. 216 Table I summarizes the minimum EDs d_{\min} between the con-217 stellation points for different APM schemes. It is found that 218 this star-QAM scheme is capable of achieving almost the same

TABLE I
MINIMUM ED BETWEEN THE CONSTELLATION
POINTS FOR DIFFERENT APM SCHEMES

Modulation order	2	4 (MMD)	8 ([9])	16 (MMD)	32 ([9])
PSK	2	$\sqrt{2}$	0.7654	0.3902	0.1960
QAM		$\sqrt{2}$	0.8165	0.6325	0.4082
Proposed star-QAM	2	$\sqrt{2}$	0.9134	0.5737	0.3952

minimum ED as the MMD-based QAM. Note that, although 219 this twin-ring star-QAM constellation has been indeed applied 220 for noncoherent detection [27], it has not been considered 221 whether this constellation can be directly applied to SM for 222 achieving performance improvements.

The aforementioned twin-ring philosophy of Fig. 1 may be 224 readily extended to multiple-ring star-QAM. The reasons for 225 considering twin-ring star-QAM in our paper are the following. 226

- It is an attractive APM modulation candidate for SM, 227 exhibiting a high performance at low detection complexity 228 compared with conventional QAM schemes, as detailed in 229 [13]–[15].
- It can be flexibly designed for different d_{\min} and $\beta_l(l=231\ 1,\ldots,L)$ combinations, which is achieved by simply ad-232 justing a single parameter α , whereas β_l can assume two 233 values because only two rings are considered.
- The ABEP of star-QAM, which is related to the $P_{\rm spatial}$ 235 term of (3), has been documented in [28] and [29].

B. Optimization Criteria and Optimization Algorithm

Observe in Fig. 1 that there are numerous options for the 238 parameter α of the star-QAM constellation, for a given MIMO 239 setup, specified by the total number of bits per symbol $m_{\rm all}$, 240 the $(N_r \times N_t)$ configuration of transceiver, and the number of 241 modulation level L. The goal of star-QAM-aided signaling 242 AQ2 constellation optimization is to find the specific ring ratio α , 243 which minimizes the ABEP of the SM-MIMO of (2). Note that, 244 although the term $P_{\rm SM}(\rho)$ in (2) cannot be directly represented 245 by parameter α , it varies as a function of α , which may 246 be formulated as $P_{\rm SM}(\rho,\alpha)$. Following the aforementioned 247 approach, we formulated this optimization problem as

$$\begin{cases} \alpha^* = \min_{\alpha} P_{\text{SM}}(\rho, \alpha) \\ \text{s.t.} \quad \alpha > 1 \end{cases}$$
 (7)

which may be a convex one for a fixed SNR value ρ , as 249 indicated in Fig. 4. However, deriving the closed-form solu- 250 tion of (7) remains an open challenge since the expression of 251 $P_{\rm SM}(\rho,\alpha)$ depends both on the specific APM constellation and 252 on the particular MIMO setup [19], and since the expressions 253 of $P_{\rm signal}, P_{\rm joint}$ and $P_{\rm spatial}$ in (3)–(5) are complex. Hence, a 254 numerical search is adopted.

Our optimization algorithm conceived for finding the ring 256 ratio is summarized as follows.

Step 1: Initialize the values of N_r , N_t , $m_{\rm all}$, L, and the SNR 258 value ρ . Set the iteration step size to $\Delta \alpha = 0.1$ and the 259 number of iterations to n=1. The choice of $\Delta \alpha$ is flexible, 260 and a lower value of $\Delta \alpha$ may lead to a better performance. 261 We then set the search area of α to $1 \le \alpha \le U_\alpha$ and the 262 performance metric to $P_{\rm iter}(n) = 0$.

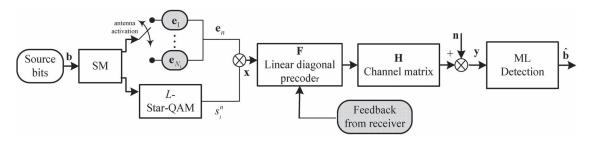


Fig. 2. System model of the diagonal-precoding-assisted star-QAM-aided SM scheme.

264 Step 2: While $\alpha \leq U_{\alpha}$, let $\Delta \hat{\alpha} = \min\{\Delta \hat{\alpha}, U_{\alpha} - \alpha\}$, and calculate the probabilities of $P_{\text{signal}}, P_{\text{joint}}$, and P_{spatial} by using (3)–(5) associated with α . Then, let $P_{\text{iter}}(n) = P_{\text{SM}}(\rho)$ using (2), and set $\alpha = \alpha + \Delta \hat{\alpha}$ and n = n + 1.

268 Step 3 : Find the index $n^* = \min_n \{P_{\text{iter}}(n)\}$ to achieve the optimal ring ratio of $\alpha^* = 1 + (n^* - 1)\Delta\hat{\alpha}$.

In the aforementioned optimization algorithm, we have to 271 choose an appropriate U_{α} to promptly find the optimal α^* . 272 More explicitly, an excessively low value of U_{α} may lead 273 to missing the optimal solution, whereas an excessively high 274 value of U_{α} imposes excessive computational complexity on 275 the optimization process. Hence, we will show in Section III 276 that $U_{\alpha}=3$ is a beneficial choice for promptly approaching 277 the optimal results. Moreover, the optimum ring ratio α^* is a 278 function of the SNR. However, we will show that the optimum 279 ratio approaches its asymptotic optimum as the SNR increases.

280 III. PROPOSED DIAGONAL PRECODING FOR 281 STAR-QUADRATURE AMPLITUDE MODULATION-AIDED 282 SPATIAL MODUALTION

Since the performance of the optimum maximum-likelihood 283 284 (ML) receiver depends on the FD of the received signal con-285 stellation [30], we propose a new TPC based on maximizing 286 the FD for the family of star-QAM-aided SM-MIMO systems, 287 when limited channel state information is available at the 288 transmitter. Since the FD is increased by the TPC algorithm, 289 the proposed scheme is expected to provide a beneficial system 290 performance improvement. To retain all the single-RF-related 291 benefits of SM, we design the TPC matrix P to be diagonal. 292 The system model of the diagonal-TPC-assisted star-QAM-293 aided SM scheme is shown in Fig. 2. To identify the specific 294 TPC parameters, which are capable of maximizing the FD, 295 we propose a low-complexity TPC design algorithm. We will 296 demonstrate that as few as two elements of the diagonal TPC 297 matrix have to be fed back to the transmitter, regardless of N_t .

298 A. TPC Design Criterion

To construct a TPC for star-QAM-aided SM-MIMO systems, 300 we can rewrite the system model of (1) as

$$y = HPx + n \tag{8}$$

301 where ${\bf P}$ denotes the diagonal TPC matrix, which can be 302 represented as

$$\mathbf{P} = \operatorname{diag}\{p_1, \dots, p_n, \dots, p_{N_t}\}\tag{9}$$

where p_n controls the channel gain associated with x_n . Here, 303 we let $\sum_{n=1}^{N_t} |p_n|^2 = N_t$ for normalizing the transmit power. 304 Note that the introduction of TPC in SM does not affect the 305 advantages of SM, such as the avoidance of the interantenna 306 interference and the reliance on a single RF chain, because the 307 precoded transmit vector $\mathbf{P}\mathbf{x}$ includes only a single nonzero 308 component; hence, only a single TA is activated in each time 309 slot, as indicated in (8).

Numerous techniques may be invoked for constructing the 311 TPC **P** [21], [25]. In this paper, similar to the precoding 312 methods conceived for the orthogonalized spatial multiplexing 313 of [31], we decompose **P** as

$$\mathbf{P} = \bar{\mathbf{P}}\mathbf{\Theta} = \operatorname{diag}\left\{\bar{p}_1 e^{j\theta_1}, \dots, \bar{p}_n e^{j\theta_n}, \dots, \bar{p}_{N_t} e^{j\theta_{N_t}}\right\}$$
(10)

where $\bar{\mathbf{P}} = \mathrm{diag}\{\bar{p}_1,\ldots,\bar{p}_n,\ldots,\bar{p}_{N_t}\}$ represents the PA ma- 315 trix, whereas $\boldsymbol{\Theta} = \mathrm{diag}\{e^{j\theta_1},\ldots,e^{j\theta_n},\ldots,e^{j\theta_{N_t}}\}$ is the phase 316 rotation matrix. The FD between the constellation points at the 317 receiver is defined as

$$d_{\min}(\mathbf{H}, \mathbf{P}) = \min_{\substack{\mathbf{x}_i, \mathbf{x}_j \in \mathbb{X}, \\ \mathbf{x}_i \neq \mathbf{x}_j}} \|\mathbf{H} \mathbf{P}(\mathbf{x}_i - \mathbf{x}_j)\|_F$$
$$= \min_{\mathbf{e}_{ij} \in \mathbb{E}} \|\mathbf{H} \bar{\mathbf{P}} \mathbf{\Theta} \mathbf{e}_{ij}\|_F$$
(11)

where \mathbb{X} is the set of all legitimate transmit symbols, $\mathbf{e}_{ij} = 319$ $\mathbf{x}_i - \mathbf{x}_j$, $i \neq j$ denotes the error vector, and \mathbb{E} is a set of error 320 vectors. Then, we design the TPC \mathbf{P} by maximizing the FD 321 with the aid of the following criterion:

$$\begin{cases}
\mathbf{P}_{\text{opt}} = \arg\max d_{\min}(\mathbf{H}, \mathbf{P}) \\
\text{s.t.} \quad \sum_{n=1}^{N_t} |p_n|^2 = N_t; \quad p_n \in C; \\
\theta_n \in (0, 2\pi]; \quad n = 1, \dots, N_t.
\end{cases}$$
(12)

Note that, since the attainable performance of the optimum 323 single-stream ML receiver depends on the FD of the received 324 signal constellation [30], the maximization of the FD directly 325 reduces the probability of error. Let $\mathbf{x}_i = s_l^i \mathbf{e}_i$ and $\mathbf{x}_j = s_k^j \mathbf{e}_j$ 326 denote two different transmit symbols, whereas s_l^i and s_k^j 327 denote the constellation points l and k represented by the ith 328 and jth antennas, respectively. Then, the FD of (11) can be 329 represented as (13), where $\phi = \angle((s_l^i)^* s_k^j) = -(s_l^i (s_k^j)^*)$. In 330

¹Because the conventional PSK-and-QAM-aided SM scheme's performance is worse than that of the proposed star-QAM-aided SM, we only invoked the TPC algorithm for the star-QAM-aided SM for the sake of achieving further performance improvements. However, it is worth noting that the proposed TPC algorithm is also suitable for SM in conjunction with both conventional PSK and QAM schemes.

331 the ASM scheme of [7], only the APM modulation orders to 332 be used by the transmitter are adapted, i.e., only the elements 333 $|s_l^i|$, $|s_k^j|$, and ϕ of (13), shown at the bottom of the page, are 334 dynamically adapted to the channel conditions, and the legit-335 imate values of these elements are selected from the discrete 336 set depending on the modulation order set utilized. By contrast, 337 our proposed scheme adjusts all the TPC elements $|p_i|$, $|p_j|$, 338 θ_i , and θ_i of (13) for maximizing the FD $d_{\min}(\mathbf{H}, \mathbf{P})$, whose 339 legitimate values are drawn from the real-valued number field. 340 Based on these observations and on (13), the proposed scheme 341 and the ASM scheme may exploit the same degrees of freedom 342 as that offered by the SM-MIMO in terms of maximizing the 343 FD. However, unlike the ASM scheme of [7] and [15], our 344 proposed scheme assigns the same number of bits to each time 345 slot; hence, the potential error propagation effects experienced 346 in ASM are avoided.

347 B. Low-Complexity TPC Design Algorithm

To identify the specific TPC matrix P, which is capable of 349 maximizing the FD, we have to determine all the N_t parameters 350 $p_n(n=1,\ldots,N_t)$. Since it may become excessively complex 351 to jointly optimize these N_t parameters in the complex-valued 352 field, we propose a low-complexity precoder design algorithm. 353 Similar to the one-bit reallocation algorithm designed for ASM 354 in [15], only the specific TA pair associated with the FD is con-355 sidered, and the TPC parameters are selected for appropriately 356 weighting the SM symbols because the FD of this particular 357 TA pair predominantly determines the achievable performance. 358 The calculation of the TPC matrix is summarized in Fig. 3. To be specific, given the channel matrix H, the indexes of 360 the TA pair (g, k) associated with the FD $d_{\min}(\mathbf{H})$ can be 361 found with the aid of the flowchart shown in Fig. 3. To offer 362 an increased FD, the precoding parameters of this TA pair can 363 be dynamically adapted. Note that, if the value of g is the same 364 as k, it is plausible that the TA g has the smallest channel gain. 365 In this case, the phase rotation elements of (10) do not have to 366 be considered because this would not increase the FD of (13). 367 To increase the FD, we only consider the PA matrix of (10) 368 and may deduct some power from the TA u having the highest 369 channel gain, which may hence be reassigned it to the TA g. 370 As a result, p_u and p_g have to be optimized. On the other hand, 371 if the value of g and k is not the same, parameters p_a and p_k 372 have to be calculated. Overall, there are only two parameters, 373 namely, p_q and p_k , $(p_u$ for g = k) that have to be searched 374 for. Finding the optimal values of p_g and p_k as a function of

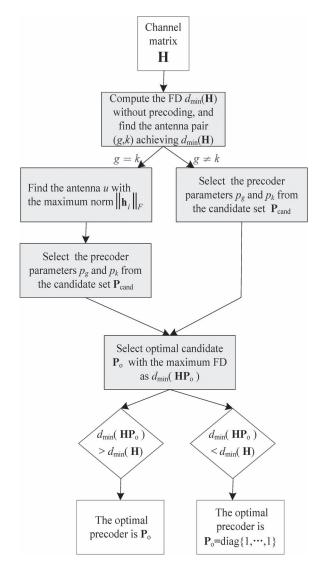


Fig. 3. Calculation of the diagonal precoding matrix for star-QAM-aided SM-MIMO.

both ${\bf H}$ and of the optimal transmit parameters involves an 375 exhaustive search over the vast design space of $\bar p_g$, $\bar p_k$, θ_g , and 376 θ_k of (10), which is overly complex. To reduce the complexity, 377 according to (12), the power of the TA pair (g,k) satisfies the 378 constraint $\bar p_k^2 + \bar p_g^2 = 2$; hence, only the element $\bar p_k$ has to be 379 searched for in the power matrix $\bar {\bf P}$ of (10). Moreover, since 380 the phase rotation of the symbol is only carried by two TAs 381 and their phase difference is correlated, we can simplify the 382 computations by fixing $\theta_k = 1$ and then finding the optimal 383

$$d_{\min}(\mathbf{H}, \mathbf{P}) = \min_{s_l^j, s_k^j \in S} \left\| \mathbf{H} \mathbf{P} \left(s_l^i \mathbf{e}_i - s_k^j \mathbf{e}_j \right) \right\|_F$$

$$= \min_{s_l^j, s_k^j \in S} \left\| \left(\mathbf{h}_i p_i s_l^i - \mathbf{h}_j p_j s_k^j \right) \right\|_F$$

$$= \min_{s_l^j, s_k^j \in S} \sqrt{\left| s_l^i \right|^2 |p_i|^2 \mathbf{h}_i^H \mathbf{h}_i + \left| s_k^j \right|^2 |p_j|^2 \mathbf{h}_j^H \mathbf{h}_j - 2|p_i||p_j| \left| s_l^i \right| \left| s_k^j \right| \operatorname{Re} \left\{ \mathbf{h}_i^H \mathbf{h}_j e^{j(\phi - \theta_i + \theta_j)} \right\}}$$
(13)

384 θ_g . This implies that only the phase parameter θ_g has to be 385 optimized for the phase matrix Θ . In Fig. 3, a numerical search 386 is used for varying \bar{p}_g and θ_g in small steps. Note that we 387 have $0 \leq \bar{p}_g \leq \sqrt{2}$ and $0 \leq \theta_g \leq 2\pi$ according to (12). For our 388 numerical search, we have assumed

$$\begin{cases}
\bar{p}_g = \sqrt{2}/V_1 * v_1, & v_1 = 0, \dots, V_1 \\
\theta_g = 2\pi/V_2 * v_2, & v_2 = 0, \dots, V_2
\end{cases}$$
(14)

389 where V_1 and V_2 represent the number of quantization steps and 390 can be flexibly selected according to the prevalent performance 391 requirements. As a result, the corresponding diagonal TPC 392 matrix candidates are

$$\mathbf{P}_{\text{cand}} = \operatorname{diag} \left\{ 1, \dots, \bar{p}_g e^{j\theta_g}, \dots, \sqrt{2 - \bar{p}_g^2}, \dots, 1 \right\}$$

$$\uparrow g \text{th} \qquad \uparrow k \text{th.} \tag{15}$$

393 Upon denoting the quantized TPC matrix ${\bf P}$ as ${\bf P}_{\rm cand}$, the 394 optimization problem of (12) is reformulated as

$$\mathbf{P}_{\text{opt}} = \underset{\{\mathbf{P} \in \mathbf{P}_{\text{end}}, \mathbf{P}_{\mathbf{I}}\}}{\arg \max} d_{\min}(\mathbf{H}, \mathbf{P}). \tag{16}$$

395 where we have $\mathbf{P_I} = \mathbf{I}_{N_t}$. In (16), the FD of the TPC matrices 396 $\mathbf{P}_{\mathrm{cand}}$ generated will be compared with that of the conventional 397 scheme associated with $\mathbf{P_I}$, and then we select the one having 398 the largest FD as our final result. The receiver determines the 399 optimal diagonal TPC matrix based on (16) and feeds back the 400 TA indexes and their TPC parameters to the transmitter. Since 401 only the specific TA pair, which predominantly determines 402 the achievable performance, is considered, the proposed low-403 complexity algorithm can be readily extended to a high number 404 of TAs.

405 IV. SIMULATION RESULTS

Here, we characterize the performance of both the proposed 406 407 star-QAM-aided SM scheme and of the corresponding TPC 408 scheme, and compare it with that of the conventional OAM-409 modulated SM schemes, with the PSK-modulated SM schemes 410 and with the ASM schemes [15] for transmission over inde-411 pendent Rayleigh block-flat MIMO channels. It is assumed that 412 the receiver is capable of perfect phase and gain tracking, i.e., 413 of perfect channel estimation. In practice, pilot symbols are 414 used for estimating the MIMO channel; hence, the estimated 415 channel matrix will inevitably be imperfect. To alleviate the 416 effects of channel estimation errors, the joint channel estimation 417 and data detection algorithm of [32] may be considered in the 418 proposed schemes, where the channel estimator and the data 419 detector iteratively exchange their information. We consider 420 two practical MIMO systems here, namely, (2×2) and (4×2) 421 4) MIMO systems. Moreover, in the TPC design algorithm, we 422 select $V_1 = V_2 = 5$ for simplicity.²

423 Fig. 4 shows the optimal ring ratios of star-QAM-aided 424 SM relying on (4 \times 4) elements for a different number of 425 modulation levels L, where the optimal ring ratio α^* is seen 426 to be a function of the SNR. The bound of (2) is well suited

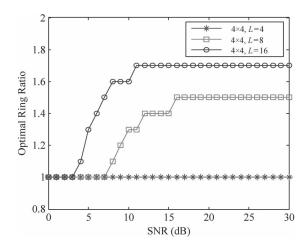


Fig. 4. Optimal ring ratios of star-QAM-aided SM with (4 \times 4) MIMO for different numbers of modulation levels L.

for numerically optimizing the ring ratio, particularly in the 427 high-SNR region. Observe in Fig. 4 that the optimal ratios 428 approach their asymptotic values, as the SNR increases. This 429 is expected since the bound of (2) is also asymptotically tight 430 and the probability of an error event in slow fading associated 431 with ML detection is dominated by the minimum-distance error 432 event at high values of the SNR. Moreover, the optimal ring 433 ratios are different for different MIMO parameters.

Since the transmitter operates at a fixed ring ratio, we have 435 opted for the asymptotic ring-ratio value for the evaluation 436 of the BER. For example, we have chosen the optimal ring 437 ratio $\alpha^* = 1.7$ for the 16-star-QAM-aided (4 × 4) SM-MIMO, 438 according to the results in Fig. 4. This result may be readily 439 extended to other star-QAM-aided SM scenarios, such as the (4 440 × 4)-element star-QAM-aided SM schemes using L=4, 8 in 441 Fig. 4.

In Figs. 5 and 6, we compare various SM-MIMO systems 443 relying on diverse MIMO parameters and modulation orders. 444 First, in Figs. 5 and 6, we depict the BER performance 445 of the conventional QAM-modulated SM schemes, of the 446 PSK-modulated SM arrangements, and of the proposed star- 447 QAM-aided SM scheme. Note that the optimized star-QAM 448 constellation is designed offline for different SM-MIMO sys- 449 tems. Hence, the resultant system does not need any feedback. 450 To be specific, we may create a parameter lookup table for 451 the star-QAM SM schemes associated with the MIMO setups 452 considered; hence, the complexity of the optimal ring-ratio 453 search process detailed in Section II is negligible. For com- 454 pleteness, we also included the theoretical upper bound [30] 455 for the family of conventional SM schemes. We found that 456 the conventional QAM-modulated SM scheme outperforms its 457 identical-throughput PSK counterpart for a (4 × 4)-element 458 MIMO channel in Fig. 5, whereas the PSK scheme is preferred 459 for a (2×2) -element MIMO channel in Fig. 6. This indicates 460 that the best choice of the APM scheme depends on the specific 461 SM parameters, such as the MIMO setup and throughput. 462 Moreover, as shown in Fig. 5, the optimized star-QAM-aided 463 SM scheme provides an SNR gain of about 3 dB at BER = 464 10⁻⁵ over the conventional 16-PSK-modulated SM scheme and 465 an SNR gain of about 1.1 dB over the identical-throughput 466

 $^{^2}$ Note that the values of V_1 and V_2 can be different. Moreover, the selection of V_1 and V_2 is flexible, and higher values of V_1 and V_2 may lead to better performance at the cost of a higher TPC design complexity.

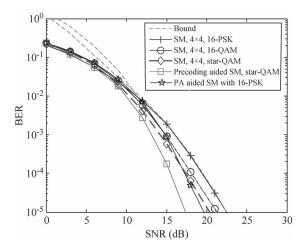


Fig. 5. BER performance of various SM-MIMO schemes operating in a (4 \times 4) MIMO channel at a total throughput of 6 b/s. Since the transmitter operates with a fixed ring ratio, we have chosen the asymptotic ring-ratio value for the evaluation of star-OAM-aided schemes. Here, α is chosen as $\alpha = 1.7$.

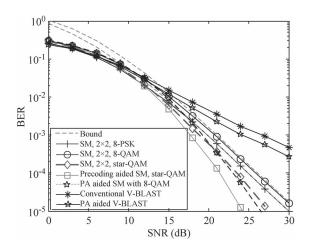


Fig. 6. BER performance of various SM schemes operating in (2×2) MIMO channel at a total throughput of 4 b/s. Here, α is chosen as $\alpha = 1.5$.

467 Gray-coded MMD 16-QAM SM scheme. This advantage of the 468 optimized star-QAM scheme recorded for SM-MIMO is also 469 visible in Fig. 6.

Moreover, in Figs. 5 and 6, we also compare the 471 achievable BER performance of the limited-feedback-aided 472 ASM schemes. To be specific, two diagonal-precoding-aided 473 schemes, namely, the precoding-assisted star-QAM-based SM 474 schemes and the PA-aided SM schemes of [33] are compared. 475 For simplicity, the PA algorithm is only applied to the non-476 ASM schemes exhibiting an inferior performance in Figs. 5 477 and 6, namely, to the conventional (4×4) -element SM using 478 16-PSK and (2×2) -element SM employing 8-QAM. Note that 479 the (4 \times 4)-element SM associated with 16-QAM and (2 \times 480 2)-element SM employing 8-PSK can also use the PA regime 481 to attain a BER improvement. Due to space limitations, these 482 results are not presented here. As shown in Figs. 5 and 6, the 483 proposed TPC schemes provide a gain of 2.5-3 dB at the BER 484 of 10^{-5} over the PA-aided SM schemes. This is because PA-485 aided SM may be viewed as a special case of the proposed 486 precoding-aided SM created by only considering the PA matrix 487 in (10). To be specific, compared with the PA-aided SM of

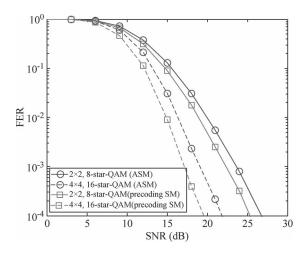


Fig. 7. FER performance of the proposed precoding star-QAM-aided SM and the ASM schemes at total throughputs of 4 and 6 b/s.

[33], our precoding-based SM regime jointly adapts the power 488 and the phases of the transmit signals and hence improves the 489 achievable BER performance.

Furthermore, in Fig. 6, we compare the QPSK-modulated 491 V-BLAST scheme and its PA-aided counterpart associated 492 with a zero-forcing-based successive interference cancelation 493 (ZF-SIC) detector [18] as the benchmarkers because their 494 detection complexity is similar to that of the single-stream 495 ML-based SM schemes. Observe in Fig. 6 for $m_{\rm all}=4$ b/s that 496 our TPC-aided SM scheme outperforms the PA-aided VBLAST 497 arrangement relying on a ZF-SIC detector. Indeed, if a powerful 498 ML detector is employed for the VBLAST system, we can 499 achieve a better BER performance. However, designing PA 500 algorithms for ML-based VBLAST systems is a challenge, and 501 their detection complexity is high, as indicated in [34].

Fig. 7 shows the frame error rate (FER) of both the proposed 503 precoded star-QAM-aided SM scheme and of the ASM scheme 504 [15]. The transmission frame size is $L_F = 60 \text{ b.}^3$ Note that, 505 although the proposed scheme and the ASM scheme exploit 506 the same degrees of freedom offered by the SM-MIMO for 507 improving the performance, our proposed scheme is capable 508 of avoiding the error propagation effects often experienced in 509 ASM, owing to ASM-mode signaling errors. Moreover, the 510 selection of TPC parameters is more flexible than that of ASM 511 because the modulation orders of ASM are selected from a 512 discrete set, whereas the TPC parameters are chosen from the 513 complex-valued field. As expected, the performance gain of 514 the proposed scheme over ASM is seen to be about 2 dB at 515 FER = 10^{-3} in Fig. 7.

V. CONCLUSION 517

In this paper, we have investigated the problem of designing 518 APM constellations that minimize the SM system's ABEP. 519 We considered a class of star-QAM constellations, which is 520

³Here, we assume that the channel matrix remains constant within each transmit frame and consider the FER performance of these schemes. Note that the ASM schemes often suffer from error-propagation effects, as indicated in Section I. Hence, using the FER comparison of the ASM and TPC-aided SM schemes may be more suitable than the BER metric.

521 capable of flexibly adapting the ring ratios. We formulated 522 the constellation design problem as an optimization problem 523 and conceived an efficient iterative constellation-optimization 524 method. Moreover, a diagonal TPC technique was proposed 525 for the optimized star-QAM-aided SM to attain an improved 526 performance. The simulation results confirm that our proposed 527 optimized star-QAM-aided SM scheme outperforms the con-528 ventional PSK/QAM schemes. Moreover, our TPC method also 529 exhibits an attractive BER/FER performance. For achieving an 530 improved performance for a high number of bits per symbol, 531 our further work will be focused on the integration of GSM and 532 channel coding into the proposed TPC schemes.

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