# ESTIMATING WAFER PROCESSING CYCLE TIME USING AN IMPROVED G/G/M QUEUE 

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#### Abstract

Wafer processing cycle times have been successfully calculated using the basic G/G/m queue by relying on historical data to determine the required variability component. The basic equation was found to work well for a highly utilized factory but provided less accurate results at low factory utilization points. Implementation of an improved $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue as suggested by existing research has resulted in improved correlation with factory performance even during times of lower factory utilization. An overview of the original implementation is presented, followed by the equation for the improved $G / \mathrm{G} / \mathrm{m}$ queue, its implementation, and subsequent validation results.


## 1 INTRODUCTION

Queuing theory has been widely dismissed as an insufficient means to estimate production cycle time in semiconductor manufacturing due to the inherent complexity of the re-entrant and lengthy process flow associated with silicon wafer processing and the inherent difficulty of determining the variability component required by the equations that have been developed. Previous work by Schelasin (2011) has shown that by taking advantage of historical data the Kingman equation can be solved to backward calculate variability representative of known factory states. This variability can then be utilized to forward calculate estimated cycle time variations that would result from changes in equipment utilization due to loading, process or equipment parameter changes.

Initial results showed encouraging correlation with actual factory cycle time performance and were effectively used to assist in making tactical as well as strategic factory management decisions for several weeks. However, when factory utilization decreased cycle time estimates were found to be less accurate than they were during the original period of higher factory utilization. Additional review of already existing research revealed that improvements to the G/G/m queue were suggested by Ward Witt (1993) to address this problem. This paper provides a review of the original work done using the more basic equation for the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue, presents the improved equation proposed by Ward Whitt, its implementation, and how its use has improved cycle time estimates when compared to actual factory performance.

## 2 ORIGINAL WORK DONE USING THE BASIC G/G/M QUEUE

### 2.1 Original Equation

The original work used the basic equation for the G/G/m queue as found in Hopp and Spearman (2003). Using Kendall's notation the Kingman equation is also known as the G/G/m queuing system. The fundamental equation for the wait time in queue for this system is defined as:

$$
\begin{equation*}
\mathrm{CT}_{q}(G / G / m)=\left(\frac{c_{a}^{2}+c_{e}^{2}}{2}\right)\left(\frac{u^{\sqrt{2(m+1)}-1}}{m(1-u)}\right) t_{e} \tag{1}
\end{equation*}
$$

where
$\mathrm{CT}_{\mathrm{q}}=$ time waiting in queue;
$c_{a}=$ coefficient of variation of inter-arrival times into the queue;
$c_{e}=$ coefficient of variation of effective process times at each machine;
$m=$ number of machines in the equipment set;
$u=$ utilization of the equipment set; and
$t_{e}=$ effective process time.

### 2.2 Original Implementation

In practical applications machine count $m$ and effective process time $t_{e}$ (consisting of raw process time RPT, Load and Unload time L/UL, and Move time between operations) are known. Utilization $u$ can be calculated using these values as part of standard static capacity modeling algorithms. In today's highly automated factories variability coefficient $c_{e}$ can be easily calculated from historical data. Variability coefficient $c_{a}$ remains as the only unknown element in Equation (1) that is difficult to determine. Li et al. (2005) suggest using the Kingman or VUT equation to backward calculate variability V from historical data. The implementation of this approach follows the steps depicted in the overview flow chart in Figure 1.


Figure 1: Queuing theory cycle time implementation - Overview.

## Schelasin

This methodology is employed to backward calculate each toolset's specific variability component using toolset specific historical machine count, historical toolset utilization, operation specific historical queue times, and operation specific effective process times. Operation specific cycle times are subsequently forward calculated for each production flow operation using the backward calculated toolset specific variability, scenario specific toolset machine counts and utilization, and operation specific effective process times. These operation specific cycle time estimates are then added together for each technology flow to produce overall technology cycle time estimates for the entire process flows through the factory.

In order to account for different equipment types and tool configurations that run the same process, toolset machine counts are adjusted within the static capacity model using an equivalency factor that is based on the model throughput standard for that toolset.

### 2.3 Original Validation Results

Cycle time estimates for major technologies running in the factory were calculated using the initial equation for the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue. Comparison of results over the course of several weeks showed very encouraging correlation to actual factory performance as shown in the first half of the charts in Figure 2.

High Volume Short Process Product


Low Volume Long Process Product


Figure 2: Cycle time validation chart - Initial results.
As can also be seen in Figure 2 cycle time results started to drift in week 10 and did not correlate very well for the second half of the charts starting in week 15. It was found that cycle time estimates became less accurate as factory utilization decreased.

## 3 THE IMPROVED G/G/M QUEUE

As suggested by Ward Whitt (1993) the fundamental high-traffic G/G/m equation performs well in cases of high machine utilization but results in decreased accuracy when machine utilization is lower. Whitt proposes improvements to the G/G/m queue by adding correction factors based on known closed-form solutions. He applies his own modifications of the accurate approximations for the $\mathrm{M} / \mathrm{D} / \mathrm{m}$ and $\mathrm{D} / \mathrm{M} / \mathrm{m}$ systems developed by Cosmetatos (1975) to obtain a better approximation. The result leads to much improved queue time values for utilizations below seventy percent especially for low machine counts. Both of these circumstances were affecting the factory being modeled when cycle time estimates based on the more fundamental queuing theory equation started to no longer validate as well against actual factory performance as they did initially. The improved equation for the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue as suggested by Whitt was used to replace the more basic equation originally implemented and is made up of the components shown in Equations (2) through (9) below:

$$
\begin{equation*}
C T_{q}\left(\mathrm{u}, c_{a}{ }^{2}, c_{e}{ }^{2}, m\right) \approx \Phi\left(\mathrm{u}, c_{a}{ }^{2}, c_{e}{ }^{2}, m\right) C T_{q}(G / G / m) \tag{2}
\end{equation*}
$$

where
$\Phi\left(\mathrm{u}, c_{a}{ }^{2}, c_{e}{ }^{2}, m\right)=\left\{\begin{array}{l}\left(\frac{4\left(c_{a}{ }^{2}-c_{e}{ }^{2}\right)}{4 c_{a}{ }^{2}-3 c_{e}{ }^{2}}\right) \Phi_{1}(m, u)+\left(\frac{c_{e}{ }^{2}}{4 c_{a}{ }^{2}-3 c_{e}{ }^{2}}\right) \psi\left(\frac{c_{a}{ }^{2}+c_{e}{ }^{2}}{2}, m, u\right), c_{a}{ }^{2} \geq c_{e}{ }^{2} \\ \left(\frac{c_{a}{ }^{2}-c_{e}{ }^{2}}{2 c_{a}{ }^{2}+2 c_{e}{ }^{2}}\right) \Phi_{3}(m, u)+\left(\frac{c_{e}{ }^{2}+3 c_{a}{ }^{2}}{2 c_{a}{ }^{2}+2 c_{e}{ }^{2}}\right) \psi\left(\frac{c_{a}{ }^{2}+c_{e}{ }^{2}}{2}, m, u\right), c_{a}{ }^{2} \leq c_{e}{ }^{2}\end{array}\right.$
where

$$
\begin{equation*}
\Phi_{1}(m, u)=1+\gamma(m, u) \tag{4}
\end{equation*}
$$

and

$$
\Psi\left(\frac{c_{a}^{2}+c_{e}^{2}}{2}, m, u\right)=\left\{\begin{array}{lr}
1, & \frac{\left(c_{a}^{2}+c_{e}^{2}\right)}{2} \geq 1  \tag{5}\\
\Phi_{4}(m, u)^{\left[2\left(1-\frac{c_{a}^{2}+c_{e}^{2}}{2}\right)\right],} & 0 \leq \frac{\left(c_{a}^{2}+c_{e}^{2}\right)}{2} \leq 1
\end{array}\right\}
$$

where

$$
\begin{equation*}
\gamma(m, u)=\min \left\{0.24, \frac{(1-u)(m-1)\left[(4+5 m)^{0.5}-2\right]}{16 m u}\right\} \tag{6}
\end{equation*}
$$

and

$$
\begin{equation*}
\Phi_{4}(m, u)=\min \left\{1,\left(\Phi_{1}(m, u)+\Phi_{3}(m, u)\right) / 2\right\} \tag{7}
\end{equation*}
$$

where

$$
\begin{equation*}
\Phi_{3}(m, u)=\Phi_{2}(m, u) e^{[-2(1-u) / 3 u]} \tag{8}
\end{equation*}
$$

where

$$
\begin{equation*}
\Phi_{2}(m, u)=1-4 \gamma(m, u) . \tag{9}
\end{equation*}
$$

## 4 IMPLEMENTATION OF THE IMPROVED G/G/M QUEUE

As was done in the original implementation, in order to effectively use the improved equation as part of the process to predict $C T_{q}$ for hypothetical scenarios assuming a similar factory state but with different machine count $m$ and utilization $u$, the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue needs to be backward calculated for variability since only $C T_{q}, t_{e}, c_{e}{ }^{2}, m$, and $u$ are known from historical data for actual scenarios. Therefore Equation (3) needs to be solved for $c_{a}{ }^{2}$. Based on experience with the factory being modeled, several approximations can be made to simplify this process.

Historical data for the factory being modeled indicate that $c_{a}{ }^{2}$ is greater than or equal to $c_{e}{ }^{2}$. This reduces Equation (3) to:

$$
\begin{equation*}
C T_{q}\left(\mathrm{u}, c_{a}{ }^{2}, c_{e}{ }^{2}, m\right) \approx\left(\frac{4\left(c_{a}{ }^{2}-c_{e}{ }^{2}\right)}{4 c_{a}{ }^{2}-3 c_{e}{ }^{2}}\right) \Phi_{1}(m, u)+\left(\frac{c_{e}{ }^{2}}{4 c_{a}^{2}-3 c_{e}{ }^{2}}\right) \psi\left(\frac{c_{a}{ }^{2}+c_{e}{ }^{2}}{2}, m, u\right) . \tag{10}
\end{equation*}
$$

Equation (10) can be further simplified based on historical data. For the majority case in the factory being modeled, the variability term $\left(c_{a}{ }^{2}+c_{e}{ }^{2}\right) / 2$ is greater than or equal to one. This allows simplification of Equation (5). After appropriate substitutions of Equations (1) through (9) into Equation (10) the final equation for the improved wait time in queue becomes:

$$
\begin{gather*}
C T_{q} \approx\left[\left(\frac{4\left(c_{a}^{2}-c_{e}^{2}\right)}{4 c_{a}^{2}-3 c_{e}^{2}}\right)\left(1+\min \left\{0.24, \frac{(1-u)(m-1)\left[(4+5 m)^{0.5}-2\right]}{16 m u}\right\}\right)\right. \\
\left.+\left(\frac{c_{e}^{2}}{4 c_{a}^{2}-3 c_{e}^{2}}\right)\right]\left(\frac{c_{a}^{2}+c_{e}^{2}}{2}\right)\left(\frac{u^{(\sqrt{2(m+1)}-1)}}{m(1-u)}\right) t_{e} \tag{11}
\end{gather*}
$$

Since for the factory being modeled $c_{e}{ }^{2}$ is much smaller than $c_{a}{ }^{2}$ additional approximations are made to solve Equation (11) for $c_{a}{ }^{2}$. The resulting Equation (12) provides backward calculated values for $c_{a}{ }^{2}$ that have been found to work well for both low as well as high factory utilization points.

$$
\begin{equation*}
c_{a}^{2} \approx\left(\frac{2 C T_{q}}{t_{e}\left(\frac{\left.u^{(\sqrt{2(m+1)}-1}\right)}{m(1-u)}\right)\left(1+\min \left\{0.24, \frac{(1-u)(m-1)\left[(4+5 m)^{0.5}-2\right]}{16 m u}\right\}\right.}\right)-c_{e}^{2} . \tag{12}
\end{equation*}
$$

Equation (12) can now be used to backward calculate $c_{a}{ }^{2}$ based on known values for $\mathrm{CT}_{\mathrm{q}}, t_{e}, c_{e}{ }^{2}, m$, and $u$. Using the backward calculated $c_{a}{ }^{2}$ and known values for $t_{e}$ and $c_{e}{ }^{2}$ allows calculation of $\mathrm{CT}_{\mathrm{q}}$ for scenarios with different values of $m$ and/or $u$, thereby providing a method to estimate the impact on cycle time due to tool count as well as volume and/or mix changes for future factory scenarios. While cycle time estimates will reflect the assumption that the future factory state modeled will be similar to that which produced the back-calculated factory variability, this method has been sufficiently accurate to greatly assist in the decision making processes used in factory capacity management.

## 5 VALIDATION RESULTS FOR THE IMPROVED G/G/M QUEUE

The charts in Figure 3 show how cycle time estimates compare with actual factory performance both before and after the change to the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ equation used. Data is presented for two of the more prevalent technology flows in the factory.

High Volume Short Process Product


Low Volume Long Process Product


Figure 3: Cycle time validation chart - Initial results and improved G/G/m queue results.
As shown previously initial cycle time estimates using the simpler equation for the $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue correlated well through week 14 but then drifted away from actual cycle time performance as factory utilization dropped. Cycle time estimates improved significantly once the improved equation for the $\mathrm{G} / \mathrm{G} / \mathrm{m}$
queue as presented in this paper was implemented starting in week 30 indicated by the vertical blue line in each graph.

The largest relative improvement in accuracy was noted in the cycle time estimates for the low volume long process product. This product was running on a newer technology and as a result was running on a number of technology unique toolsets that had a low machine count as well as low utilization.

Figure 4 shows the average percent delta to actual cycle times. As can be seen from this graph the accuracy of the calculated cycle time estimates when compared to actual factory performance not only returned to its original level, but actually improved considerably. The dashed line in Figure 4 starting in week 1 shows how after the initial implementation using the simpler $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue equations estimated cycle times were on average within just over $6 \%$ of actual cycle times. The dotted line starting in week 15 shows how the delta to actuals increased at lower factory utilization to almost $11 \%$. The equations for the improved G/G/m queue were implemented in week 30 as indicated by the vertical blue line. With the implementation of the improved $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue equations accuracy improved markedly to being on average within just over $3 \%$ of actual cycle times. As factory utilization increased starting around week 60 cycle time estimate accuracy continued to be better than before and even further improved.


Figure 4: Percent delta between estimated and actual cycle times.

## 6 CONCLUSION

The original implementation of the basic $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue algorithms to calculate wafer processing cycle time provided good results when compared to actual factory performance but only as long as factory utilization was high. An improved $\mathrm{G} / \mathrm{G} / \mathrm{m}$ queue equation as suggested by existing research which includes approximations based on closed-form solutions has been successfully used to improve on the accuracy of cycle time wafer processing estimates during time periods of both low as well as high factory utilization.

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