

Liftings and stresses for planar periodic frameworks

Ciprian S. Borcea and Ileana Streinu

Abstract

We formulate and prove a periodic analog of Maxwell’s theorem relating stressed planar frameworks and their liftings to polyhedral surfaces with spherical topology. We use our lifting theorem to prove deformation and rigidity-theoretic properties for planar periodic pseudo-triangulations, generalizing features known for their finite counterparts. These properties are then applied to questions originating in mathematical crystallography and materials science, concerning planar periodic auxetic structures and ultrarigid periodic frameworks.

Keywords: periodic framework Maxwell’s theorem periodic stress liftings periodic pseudo-triangulation expansive motion auxetics ultrarigidity

1 Introduction

A remarkable correspondence between planar stressed graphs, their duals and polyhedral surfaces with a spherical topology has been established in 1870 by James Clerk Maxwell:

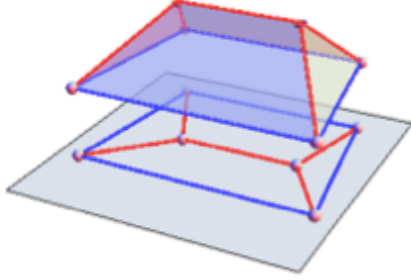


Figure 1: A finite planar stressed graph and a Maxwell lifting.

Maxwell’s Theorem [36] *A planar geometric graph (G, p) supports a non-trivial stress on its edges if and only if it has a dual reciprocal diagram and, at the same time, if and only if it has a non-trivial lifting to 3D as a polyhedral terrain.*

The necessary definitions are recalled below in Section 2. A closely related instance of this theorem is the classical duality between Voronoi diagrams and Delaunay tessellations, where the 3D lifting is onto a paraboloid. Maxwell’s diagrams, further popularized in Cremona’s book [16], were widely used for engineering calculations throughout the 19th and 20th centuries. The theorem has many other applications, for example in problems of robustness for geometric algorithms, rigidity theory, polyhedral combinatorics and computational geometry [15, 30, 43, 44, 12, 48]. Most relevant to our undertaking is its role in establishing the existence of planar expansive motions used in the solution to the Carpenter’s Rule problem [12], and in proving the expansive properties of pointed pseudo-triangulation mechanisms that are central to the algorithm for convexifying simple planar polygons of [47, 48].

Our results. In this paper we prove the following *periodic* analog of Maxwell’s theorem. Figure 2 illustrates the concepts, whose precise definitions will be given in Section 3.

Main Theorem *Let (G, Γ, p, π) be a planar non-crossing periodic framework. A stress induced by a periodic lifting is a periodic stress and conversely, any periodic stress is induced by a periodic lifting, determined up to an arbitrary additive constant.*

Non-crossing periodic graphs can be seen as graphs embedded on the flat torus. However, as it will become clear from this paper, to reason on a fixed torus would be too restrictive a perspective. The most important foundational element that makes the new result possible is our recent *deformation theory of periodic frameworks* [3], which allows the periodicity lattice to deform. The corresponding notion of *periodic stress* is precisely the notion of stress that is needed for the Main Theorem. This stress is more constrained than the direct generalization of the classical *self-stress* used for finite frameworks, which is based solely on equilibrium at all vertices. In order to maintain the proper distinction, we refer to the latter type of stress as an *equilibrium stress*.

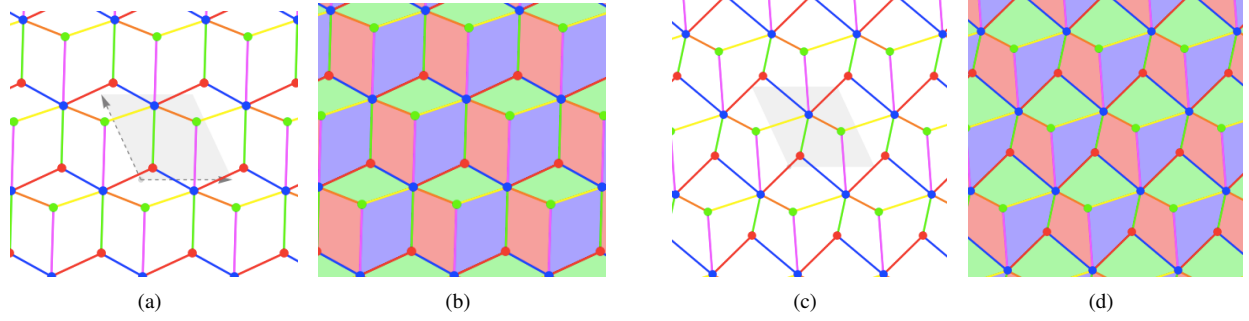


Figure 2: The connection between periodic stresses and liftings proven in this paper. (a) A stressed periodic framework. Vertex and edge orbits are identically colored, and a fundamental polygon of the periodicity lattice is highlighted in grey. (b) Coloring the faces helps visualize the 3D lifting of the framework as a periodic arrangement of “cubes”. (c) The same periodic graph, in a placement with no non-trivial periodic stresses. (d) The face coloring visually confirms that this is *not* the projection of a polyhedral surface: the faces do not look “flat” in 3D.

Our theorem was motivated by questions arising in mathematical crystallography and computational materials science. We demonstrate its usefulness with two applications: constructions of ultrarigid frameworks and auxetic mechanisms.

Ultrarigidity of periodic frameworks. Leaving some technical details aside, our proof of the correspondence between periodic liftings and periodic stresses will proceed by showing how to obtain a transparent, algebraic matching of all the concepts involved after a sufficient *relaxation of periodicity*. Relaxations of periodicity are a central concern in displacive phase transitions [20, 6] and successive relaxations give rise to difficult and important problems for estimating the *asymptotic behavior* of a periodic framework.

By definition, a periodic framework is *ultrarigid* if it is and remains infinitesimally periodically rigid under arbitrary relaxations of periodicity to subgroups of finite index (see Figure 3). This concept was introduced in [5], and illustrated with a few examples of crystalline materials exhibiting this property. Ultrarigidity provides a rigorous tool for studying the asymptotic rigidity of a periodic framework when successive relaxations of periodicity are applied. The proof techniques developed in this paper will allow us to construct infinite families of ultrarigid examples.

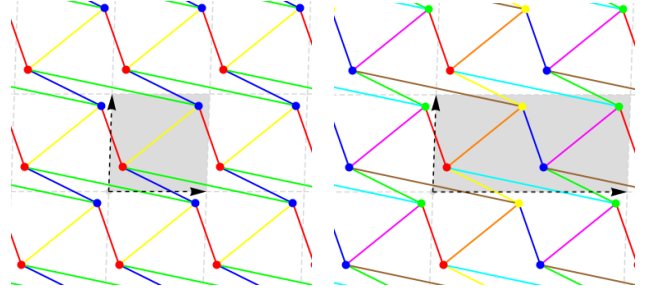


Figure 3: A periodic framework and a 2×1 relaxation of its periodicity lattice.

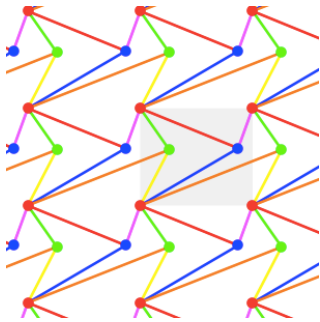


Figure 4: A periodic pointed pseudo-triangulation.

For some related considerations and observations on rigidity and relaxation, we mention [41, 13]. The basic theory of periodic frameworks from the point of view of rigidity and flexibility can be found in [3, 4, 6]. For wider or complementary aspects of periodic framework theory we suggest [50, 11] and references therein.

Periodic pseudo-triangulations. We use the Main Theorem to study a new class of planar non-crossing periodic frameworks called *periodic pointed pseudo-triangulations* or shortly *periodic pseudo-triangulations*. They represent a natural analog of the finite *pointed* pseudo-triangulation frameworks defined and studied in [47, 48] and possess *mutatis mutandis* many outstanding characteristics related to rigidity and deformations [47, 48, 45, 46]. Here we focus on the *expansive* one-degree-of-freedom mechanisms they provide and on the property of turning into ultrarigid periodic frameworks after the insertion of a single (adequate) edge-orbit.

Deformations of periodic frameworks: auxetic and expansive behavior. The significance of the idea of expansive motion is well recognized in the finite setting [12, 48, 46]: when the distance between any pair of vertices cannot decrease, self-collision of the framework is avoided. In the periodic setting, expansive

mechanisms have not been explicitly considered before, although a related, yet weaker notion of *auxetic behavior* has recently attracted a lot of attention in materials science [21, 33, 39]. Since the existing literature on auxetics is based on elasticity theory, we include a brief and necessarily selective overview of the relations existing between the purely geometric theory pursued in this paper and the larger context of periodic structures explored in crystallography, solid state physics and materials science [34, 50, 22].

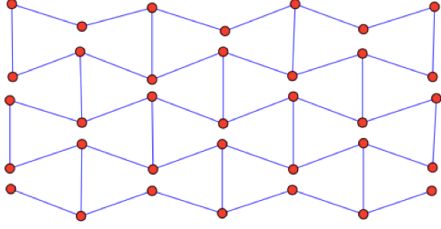


Figure 5: This so-called ‘reentrant’ structure of hexagons is often used to illustrate auxetic behavior.

along an axis, most materials are expected to expand along this axis and to contract along directions perpendicular to it. Auxetic behavior refers to the rather counter-intuitive lateral widening upon application of a longitudinal tensile strain. A purely geometric expression of this behavior is not anticipated in all situations. However, for periodic frameworks, we have recently proposed the general geometric notion of *auxetic path* in the deformation space of the periodic framework [8]. Relying on this formulation, we prove that an expansive deformation path is necessarily an auxetic path. Periodic pseudo-triangulations thus exhibit auxetic behavior and offer an infinite supply of planar examples of “auxetic frameworks”. By contrast, only a limited collection of sporadic and artisanal auxetic periodic examples (Figure 5) has appeared in the literature. One may already notice that the reentrant framework from Figure 5 looks “almost” like a pointed pseudo-triangulation, except that it is not maximal. It needs one more edge-orbit for all its faces to become pseudo-triangles, as illustrated in Figure 16 of Section 6.

Interest in crystal morphology and structure motivated mathematical studies of symmetry, lattice sphere packings and crystallographic groups [14, 34]. With the advent of X-ray diffraction, materials science gained access to atomic-scale configurations and bonding networks. An explicit mention of a *periodic framework deformation* appears in Pauling’s 1930 paper [40]. Nevertheless, such geometric investigations addressed only specific crystalline materials and remained mostly concerned with a number of instances of one-parameter deformations related to particular displacive phase transitions, as in [18, 20].

The notion of *auxetic behavior* is formulated using the concept of negative Poisson’s ratio [22, 23, 21], which relies on physical properties of the material: when two forces pull in opposite directions

Organization of the paper. In Section 2 we define the basic concepts needed to study the correspondence between liftings and stresses in (finite or infinite) frameworks. Section 3 specializes these concepts to *periodic* liftings and stresses. Section 4 concludes the proof of the Main Theorem by providing the necessary link with periodic rigidity and flexibility. The Main theorem is applied in Section 5 to prove the expansive properties of periodic pseudo-triangulations. The connection with auxetic behavior and the ultrarigid character of periodic frameworks obtained from pseudo-triangulations are presented in the final Sections 6 and 7.

2 Liftings and stresses

To formulate and prove our Main Theorem, we start with those concepts and properties that do not depend (yet) on periodicity, which is introduced in the next section.

Graphs and frameworks. We consider finite or countably infinite graphs which are simple (i.e. without loops or multiple edges), unoriented and of finite degree (or valency) at each vertex. Such a graph is given as a pair $G = (V, E)$, with V the set of vertices and E the set of (unoriented) edges. We use lower case symbols u, v, \dots for vertices in V . An edge $e = \{u, v\} = \{v, u\} \in E$ has two *endpoints* $u, v \in V, u \neq v$ and can be given two orientations (u, v) and (v, u) . Two edges $e_1, e_2 \in E$ are *adjacent* if they have a common endpoint: $|e_1 \cap e_2| = 1$. The set of edges *incident* to a vertex v consists of all edges $e \in E$ having v as one of their endpoints. The degree (or valency) of a vertex is the number of edges incident to it.

A *placement* of G in \mathbb{R}^d is given by a mapping $p : V \mapsto \mathbb{R}^d$ of the vertices to points in \mathbb{R}^d , such that the two endpoints of each edge $e = \{u, v\} \in E$ are mapped to distinct points in \mathbb{R}^d : $p(u) \neq p(v)$. An edge $\{u, v\}$ is seen geometrically as an *edge-segment* $[p(u), p(v)]$, and an oriented edge (u, v) determines an *edge-vector* $p(v) - p(u) \in \mathbb{R}^d$. We work under

the assumption that **all placements are locally finite maps**, that is, the preimage of any bounded set is finite. This is certainly true for the periodic placements defined in the next section.

A *framework* or *geometric graph* (G, p) is a graph G together with a placement p , restricted in this paper to \mathbb{R}^2 or \mathbb{R}^3 . We use the term *planar placement* for \mathbb{R}^2 , when the distinction is necessary.

Planar non-crossing frameworks. A planar placement is *non-crossing* if any pair of edges induces disjoint closed segments, with the possible exception of the common endpoint, in the case when the edges are adjacent. A graph G is *planar*¹ if it admits a non-crossing placement (G, p) . We consider only connected graphs, therefore a non-crossing placement (G, p) induces a connected subset of the plane, made of the points $p(v), v \in V$ and the edge segments $[p(u), p(v)]$ with $\{u, v\} \in E$. A *face* U is a connected component of the complement of the placement (G, p) . **We assume throughout the paper that the boundary of each face is a simple finite polygon.** A face is described combinatorially by the cyclic collection of its boundary vertices or edges, and each edge is on the boundary of exactly two distinct faces.

For a planar non-crossing framework it is convenient to use now the same symbol G to denote the entire collection $G = (V, E, F)$ of vertices V , edges E and faces F . For notational simplicity, we allow the capital letters U, V, \dots to stand for open face domains, closed faces, or the corresponding boundary cycles (as needed in various contexts).

When referring to a *planar graph* G (with no reference to a particular placement) we assume that the choice of face cycles F is also given, i.e. $G = (V, E, F)$. We note that even when the underlying graph $G = (V, E, F)$ of a framework (G, p) is a planar graph, the particular placement p of the framework may have crossings: we still refer to the realization of a face, although it may be a self-intersecting polygon.

To a planar graph $G = (V, E, F)$ we can associate a *dual* structure $G^* = (V^*, E^*, F^*)$ defined as the abstract triple whose vertices V^* correspond to the faces F of G i.e. $V^* = F$, and whose edges E^* are in one-to-one correspondence with the edges E of G , as follows: if two faces U and W share an edge e , then the dual vertices U^* and W^* are connected by the dual edge e^* . The dual faces F^* correspond to the vertices of G i.e. $F^* = V$, with the cycle of faces around a vertex inducing its corresponding dual face. By abuse of language, we may refer to $G^* = (V^*, E^*, F^*)$ as the *dual graph* of $G = (V, E, F)$, although it may have multiple edges.

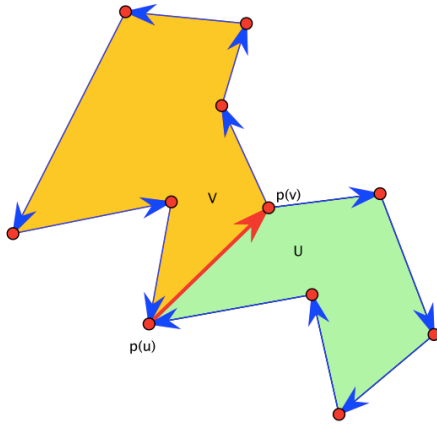


Figure 6: The orientation convention for face edges and vertex edges.

Orientation rule. In a planar non-crossing framework, an edge $\{u, v\}$ induces a segment $[p(u), p(v)]$, and it belongs to the boundary of *exactly two faces*, say U and V . In the dual graph $G^* = (F, E)$ these two faces U and V represent two vertices connected by the un-oriented edge $\{U, V\}$ dual to $\{u, v\}$. Later on, we will need to match an *oriented* edge in the primal graph $G = (V, E)$ with an orientation of its dual edge in $G^* = (F, E)$. We use the following convention. The oriented edge segment $[p(u), p(v)]$ gives opposite senses for going around face U and face V , say counter-clockwise around V and clockwise around U . Then the matching orientation of the edge in the dual graph G^* is from U to V . In short: ‘from clockwise to counter-clockwise’, as illustrated in Figure 6.

The matching orientation described above for elements in the edge set E , when considered as oriented edges in $G = (V, E)$, respectively $G^* = (F, E)$, gives a well-formed double pair $((u, v), (U, V))$, or simply a *tetrad* (u, v, U, V) . In computational geometry, these tetrads are implicit in the quad-edge data structure used for representing general surfaces [29]. Reversing orientation on the edge gives the tetrad (v, u, V, U) . Below, we will refer to cycles (called *face-cycles*) of oriented edges in the dual graph $G^* = (F, E)$: the orientation rule described above gives an unambiguous correspondence with *oriented edges* (u, v) in the primal graph G and their corresponding *edge vectors* $p(v) - p(u)$ in a geometric placement p of G .

¹Note that we use *planar* for the graph, as is customary in graph theory, and *non-crossing* for the framework. Our use of *planar framework* is customary in rigidity theory, and refers to a placement in the *plane*.

Stressed frameworks. An *equilibrium stress* or, shortly, a *stress* on a planar (finite or infinite, possibly crossing) framework² is an assignment $s : E \rightarrow \mathbb{R}$ of scalar values $\{s_e\}_{e \in E}$ to the edges E of G in such a way that the edge vectors incident to each vertex $u \in V$, scaled by their corresponding stresses, are in equilibrium, i.e. sum up to zero:

$$\sum_{e=\{u,v\} \in E} s_e(p(v) - p(u)) = 0, \text{ for fixed } u \in V \quad (1)$$

When all s_e are zero, the stress s is *trivial*; when all $s_e \neq 0$, the stress is called *nowhere zero*. The space of all equilibrium stresses of a framework is a vector space, so if a framework has a non-trivial stress, then it is not unique; in particular, any rescaling of it is also a stress.

Lifting. A lifting of the planar framework (G, p) is a continuous function $H : \mathbb{R}^2 \rightarrow \mathbb{R}$ whose restriction to any face is an affine function. The lifting assigns a height, or altitude $H(q)$ to each point q in \mathbb{R}^2 (seen as the plane $z = 0$ in \mathbb{R}^3), in such a way that the lifted faces are flat (all face cycle vertices lie in the same plane) and connect continuously along the lifted edge segments. The height function is completely determined by the values $H(p(v))$ at the vertices of the framework, and its graph appears as a polyhedral surface or *terrain* over the face-tiling in the reference plane. A lifting is *trivial* if all its faces are lifted in the same plane, that is, when H is affine on \mathbb{R}^2 . A lifting is *strict* if no two adjacent faces are lifted to the same plane.

With these concepts in place, we move on to the correspondences involved in Maxwell's theorem.

Equilibrium stress associated to a lifting. Let H be a lifting of a framework (G, p) . With usual dot product notation, the expression of H restricted to a face U takes the form

$$H(q) = v_U \cdot q + C_U, \text{ for } q \in U \subset \mathbb{R}^2 \quad (2)$$

where $v_U \in \mathbb{R}^2$ is the projection on the reference plane of the *normal* to face U and $C_U \in \mathbb{R}$.

The system of vectors and constants $H \equiv (v_U, C_U)_{U \in F}$ is subject to the compatibility conditions on edges $\{u, v\}$ shared by pairs of adjacent faces $\{U, V\}$:

$$\begin{aligned} v_U \cdot p(u) + C_U &= v_V \cdot p(u) + C_V \\ v_U \cdot p(v) + C_U &= v_V \cdot p(v) + C_V \end{aligned} \quad (3)$$

From this, we infer that the vector $v_V - v_U$ is orthogonal to the edge vector $p(v) - p(u)$. Fig. 7 illustrates the relationship.

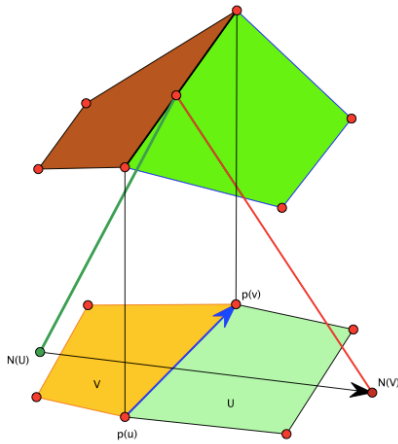


Figure 7: The normals to two adjacent lifted faces induce the dual orthogonal edge.

Given a tetrad (u, v, U, V) of dual edges, and using the notation $(x, y)^\perp = (-y, x)$ for the clockwise rotation with $\pi/2$ of a vector $(x, y) \in \mathbb{R}^2$, we define the *stress factor* on the edge $\{u, v\} \in E$, associated to the lifting H , as being the proportionality factor s_{uv} given by:

$$v_V - v_U = s_{uv}(p(v) - p(u))^\perp \quad (4)$$

Since the sum involves the vectors around a closed polygon (the face-cycle around a vertex), the equilibrium condition (1) is satisfied. This proves:

Proposition 1. *For any lifting H of a planar non-crossing framework (G, p) , there exists a canonically associated equilibrium stress on the framework.*

The correspondence between liftings and stresses described above is essentially the one given by Maxwell, who formulated it through the following geometric construction. The normal direction to the planar region corresponding to a face $U \in F$ in the lifted terrain is given by $N_U = (v_U, -1) \in$

²Also called a *self-stress* in the rigidity theory literature.

\mathbb{R}^3 , $U \in F$. When all these normal vectors are taken through the point $(0, 0, 1)$, they intersect the reference plane $z = 0$ in the system of points $\{v_U \in \mathbb{R}^2 \mid U \in F\}$. The classical “theorem of the three perpendiculars” implies the orthogonality $(v_V - v_U) \cdot (p(v) - p(u)) = 0$ observed above. In Figure 7 we see the normals to two adjacent lifted faces, taken from a point of the lifted common edge. They intersect the reference plane in $N(U)$ and $N(V)$, with vectors $p(v) - p(u)$ and $N(V) - N(U)$ orthogonal.

Reciprocal diagram. A framework (G^*, p^*) associated to the dual graph G^* of a planar framework (G, p) is called a *reciprocal diagram* if the corresponding primal-dual edges are perpendicular. If in the previous construction we join the points $\{v_U \in \mathbb{R}^2 \mid U \in F\}$ by edges dual to the primal ones, we obtain a reciprocal diagram associated to the lifting H . We note that it is possible for several vertices v_U to coincide, and this happens precisely when several planar regions in the lifting have identical normal directions. An extreme case arises for liftings with globally affine functions H . They give a planar (trivial) terrain over the reference plane, have constant v_U and induce the trivial stress $\{s_e\}_{e \in E} = 0$.

From equilibrium stresses to liftings. The direction from stresses to Maxwell liftings requires more work.

Proposition 2. *Let $s = (s_e)_{e \in E}$ be an equilibrium stress for the framework (G, p) . Then there exists a lifting H which induces s , determined up to addition of a global affine function.*

Proof. We have to find a set of parameters (v_U, C_U) , indexed by faces and satisfying the conditions (3) and (4) in terms of the given placement p . Let us choose an initial face U_0 with an arbitrary lifting $(v_{U_0}, C_{U_0}) = (v_0, C_0)$. We show that once this initial choice has been made, the lifting is then uniquely determined by the placement p and the stress values s .

For this purpose, we solve the linear system (3) in a step-by-step manner, progressing from face to adjacent face, starting at U_0 . We remark that an infinite graph induces an infinite such linear system, but nevertheless it can be solved incrementally, as we now show. We consider a *path* through adjacent faces labeled U_0, U_1, \dots, U_n , with corresponding liftings (v_i, C_i) and successive tetrads (p_i, q_i, U_i, U_{i+1}) . Thus, $[p_i, q_i]$ is the common edge between faces U_i and U_{i+1} , with the proper orientation induced by the direction in which we walk through the path of adjacent faces, and the orientation rule described earlier. The given stress on this edge is denoted here by s_i .

We first compute the parameters v_k by unfolding the relationships (4) along the path from U_0 to U_k :

$$v_{k+1} = v_k + s_k(q_k - p_k)^\perp = \dots = v_0 + \sum_{i=0}^k s_i(q_i - p_i)^\perp \quad (5)$$

Similarly, we compute the parameters C_k by unfolding the first of the two relationships (3) along the path from U_0 to U_k , and using (4) at each step:

$$C_{k+1} = C_k - (v_{k+1} - v_k) \cdot p_k = \dots = C_0 - \sum_{i=0}^k s_i(q_i - p_i)^\perp \cdot p_i \quad (6)$$

Using the identity $(q_i - p_i)^\perp \cdot p_i = \det(q_i \ p_i)$ and the notation $|q_i \ p_i| := \det(q_i \ p_i)$ in (5) and (6), the expression (2) of the height function becomes:

$$H(q) = v_n \cdot q + C_n = (v_0 + \sum_{i=0}^{n-1} s_i(q_i - p_i)^\perp) \cdot q + (C_0 - \sum_{i=0}^{n-1} s_i |q_i \ p_i|) \quad (7)$$

It remains to check that the expression (7) is independent of the face-path chosen from U_0 to U_n . To verify this property, we have to check that the following sums vanish for any face-cycle:

$$\sum_{i \in \text{face-cycle}} s_i(q_i - p_i) = 0 \quad \text{and} \quad \sum_{i \in \text{face-cycle}} s_i |q_i \ p_i| = 0 \quad (8)$$

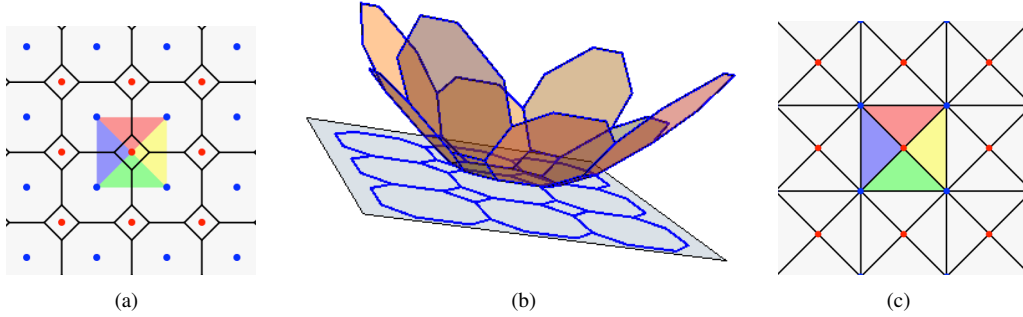


Figure 8: (a) A Delaunay framework (in black) corresponding to a periodic set with four site orbits under maximal translational symmetry. Dual vertices are shown as colored centers of the faces. Primal-dual edge pairs are orthogonal. (b) The equilibrium stress induced by the reciprocal diagram has a non-periodic lifting to the paraboloid $z = x^2 + y^2$. (c) The reciprocal diagram of the periodic graph on the left is the Voronoi diagram of the periodic sites.

It suffices to verify these relations over face-cycles corresponding to simple topological loops. In this case, Jordan's simple curve theorem gives a set of vertices inside the loop. When we sum the equilibrium stress condition (1) over the vertices inside the loop, terms cancel in pairs for adjacent vertices and yield the first identity. For the second part, we observe that the equilibrium stress condition (1) induces the identity $|\sum_{\{u,v\} \in E} s_{uv}(p(v) - p(u)) p(u)| = 0$, for fixed vertex u . Rewriting it as $\sum_{\{u,v\} \in E} s_{uv}|p(v) p(u)| = 0$ and again taking the sum over the vertices inside the loop, we obtain the second identity in (8).

Since the initial choice (v_0, C_0) was arbitrary, the lifting H is determined only up to a global affine function. \square

Mountain-valley edge liftings and stress factor signs. We review now an elementary geometrical criterion for determining the sign of a stress factor s_{uv} in a stress s associated to a lifting. Let us consider the lifted 3D polygonal surface projecting over the faces of the graph in the reference plane, as in Figure 1, and let uv be part of a tetrad (u, v, U, V) . A vertical translation of the whole polygonal surface does not affect the stress considerations. We assume therefore that the lifting of the two faces U and V is above the reference plane. Figure 7 illustrates the case of a negative stress factor s_{uv} , corresponding visually with a lifted edge that looks like a 'mountain ridge'. The normal directions to the lifted faces over U and V are here taken through a point of the lifted common edge and intersect the reference plane in points denoted $N(U)$ and $N(V)$. For the tetrad (u, v, U, V) , the sign of the stress factor is that of the determinant $|p(v) - p(u) N(V) - N(U)|$ and is consistent with the orientation rule described in Section 2.

For the geometrical interpretation, let us look at the *dihedral angle* of the lifted faces, understood as the intersection of the two half-spaces below the respective supporting planes. Then, when the measure of this dihedral angle is less than π , we have a negative stress factor and the visual landscape suggestive of a mountain range, while for a dihedral angle greater than π , we have a positive stress factor and the visual landscape suggestive of a valley. When the dihedral angle is exactly π , the stress factor is zero and the two lifted faces are in the same plane. A non-flat edge in the lifting is therefore said to be a *mountain* edge if the terrain is concave in its neighborhood, and a *valley* otherwise. The correspondence between stresses and liftings is now refined by this well-known property [15]:

Proposition 3. *The Maxwell correspondence between stressed graphs and liftings takes planar edges with a negative stress to mountain edges in the 3D lifting, those with positive stress to valley edges and those with zero stress to the common plane of the two adjacent lifted faces.*

Comment. As mentioned, this correspondence between liftings and stresses is a direct adaptation of the one formulated by Maxwell in the finite setting [35, 36] (see also the expositions given in [30, 15, 43]). The arrangement and presentation given in this section, including the notation, are meant to serve as a preamble for the more elaborate *periodic* version, which relies on notions developed recently in our deformation theory of periodic frameworks [3, 4, 6].

We conclude this section with a noteworthy example, illustrated in Fig. 8, which will be used in the next two sections to illustrate the critical distinction between equilibrium stress and periodic stress.

Example 1. (Delaunay tessellations and Voronoi diagrams of periodic point sets) *The classical Voronoi-Delaunay duality, applied to a (countable locally finite) periodic point set p in \mathbb{R}^2 , yields a dual pair of non-crossing periodic frameworks whose corresponding dual edges are orthogonal. For a fixed point p_i in the given set p , its (open) Voronoi cell is defined as the planar domain made of all the points in \mathbb{R}^2 whose distance to p_i is strictly less than the distance to any other point in the set p . The union of all these cell boundaries give the vertices and edges of the Voronoi framework. The Delaunay framework is its dual, with vertices at the original point set p and with edges orthogonal to those of the Voronoi framework; its faces are convex polygons whose vertices are cocircular, and the circumscribed circles are empty of any other vertices in the given point set [17]. Fig. 8 gives an illustration with periodicity lattice generated by the standard basis. There are four orbits of vertices, with representatives at the corners of one of the diamonds in Fig. 8(a). All faces are inscribed polygons and the centers of the corresponding circumscribed circles give the vertices of the Voronoi diagram.*

3 Equilibrium and periodic stresses on periodic frameworks

We turn now to the main object studied in this paper, the infinite *periodic framework* as defined in [3, 4]. We emphasize from the outset that a periodic graph is not just an infinite graph, as it was in the previous section: the definition *includes* a periodicity group of graph automorphisms. In this paper we focus on the *planar case* $d = 2$ and on *connected non-crossing periodic frameworks*. Some statements and constructions will be valid in broader contexts, but for the sake of a streamlined presentation we will stay within this class.

Planar periodic frameworks. A 2-periodic framework [3, 4], denoted as (G, Γ, p, π) , is given by an infinite graph G , a periodicity group Γ acting on G , a placement p and a representation π . The graph $G = (V, E)$ is simple (has no multiple edges and no loops) and connected, with an infinite set of vertices V and (unoriented) edges E . The *periodicity group* $\Gamma \subset \text{Aut}(G)$ is a free Abelian group of rank two acting on G without fixed vertices or fixed edges. We consider only the case where the quotient multigraph G/Γ (which may have loops and multiple edges) is *finite*, and use $n = |V/\Gamma|$ and $m = |E/\Gamma|$ to denote the number of vertex and edge orbits. The function $p : V \rightarrow \mathbb{R}^2$ gives a specific placement of the vertices as points in the plane, in such a way that any two vertices joined by an edge in E are mapped to distinct points. The *injective group morphism* $\pi : \Gamma \rightarrow \mathcal{T}(\mathbb{R}^2)$ gives a faithful representation of Γ by a *lattice of translations* $\pi(\Gamma) = \Lambda$ of rank two in the group of planar translations $\mathcal{T}(\mathbb{R}^2) \cong \mathbb{R}^2$. The placement is *periodic* in the obvious sense that the abstract action of the periodicity group Γ is replicated by the action of the periodicity lattice $\Lambda = \pi(\Gamma)$ on the placed vertices: $p(\gamma v) = \pi(\gamma)(p(v))$, for all $\gamma \in \Gamma, v \in V$.

Non-crossing planar periodic frameworks $G = ((V, E, F), \Gamma)$ in \mathbb{R}^2 . They have an underlying planar graph $G = (V, E, F)$ with the natural action of the periodicity group Γ . The *dual 2-periodic graph* $G^* = ((V^*, E^*, F^*), \Gamma)$ is obtained from the abstract dual of the infinite graph $G = (V, E, F)$, with the periodicity group Γ acting on it in the same manner as it acts on the sets of the primal graph $F = V^*, E = E^*, V = F^*$. If we denote by $n^* = \text{card}(F/\Gamma)$ the number of face orbits under Γ , then Euler's formula for the torus $\mathbb{R}^2/\Lambda \supset G/\Gamma$ gives the relation:

$$n - m + n^* = 0, \quad \text{that is} \quad n + n^* = m. \quad (9)$$

Γ -invariant equilibrium stress on a periodic framework. An equilibrium stress s of the periodic framework (G, p, Γ, π) is called a Γ -invariant equilibrium stress if it is invariant on edge orbits E/Γ . A Γ -invariant equilibrium stress can be calculated by solving a finite linear system of equations of type (1), where the unknowns are the stresses for the edge representatives in E/Γ and the equations correspond to equilibrium conditions for the vertex representatives in V/Γ .

Preview: periodic stress from periodic lifting. Not all equilibrium stresses of a periodic framework are Γ -invariant. Although we have not yet defined periodic stresses (Definition (6) in the next Section 4), we mention, as a preview, that they must be Γ -invariant. But this will not be sufficient: for some periodic frameworks, the periodic stresses are a *strict* subset of the Γ -invariant ones. Figure 9 illustrates such a situation, using colors to indicate the stress sign (red for positive, blue for negative stress, gray for zero stress) for the various types of stresses that a periodic framework may support (not Γ -invariant, Γ -invariant non-periodic and periodic).

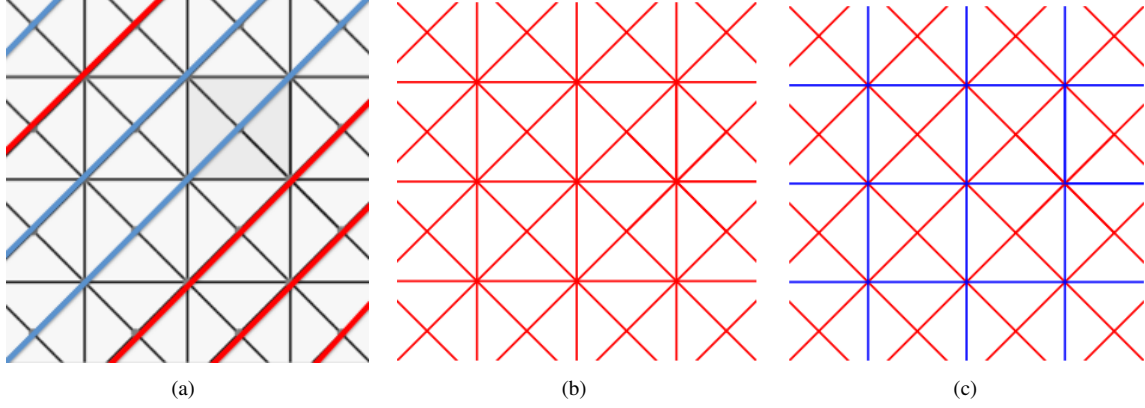


Figure 9: The Voronoi diagram from Fig. 8(c) is a periodic framework supporting different types of stresses. (a) **(Not Γ -invariant)** Each of the “aligned” infinite paths supports a one-dimensional stress (equal on each edge of the path and illustrated here with the oblique colored diagonals). The stress values can be independently chosen on each diagonal path, and thus yield equilibrium stresses, such as the one depicted here, which are not Γ -invariant. (b) **(Non-periodic Γ -invariant)** A Γ -invariant stress assigns the same stress value on all edges in an edge orbit. Illustrated here is a stress where all stress orbits have the same sign; this cannot be a periodic stress. (c) A **periodic stress**, as the one shown here, must have both positive and negative stresses on edge orbits.

We will arrive at periodic stress indirectly, via periodic liftings, defined next. In the rest of this section we show that the stresses corresponding to these periodic liftings must satisfy additional constraints. Then, in the next section, we define periodic stress in rigidity theoretic terms, and show that it coincides with this constrained stress.

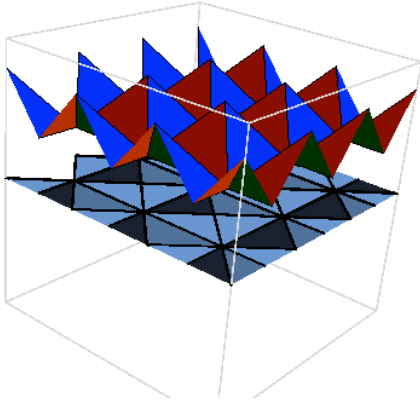


Figure 10: A periodic 3D lifting for the stressed framework in Figure 9(c).

Periodic liftings. A lifting H for the planar periodic framework (G, Γ, p, π) is called periodic when Γ -invariant, that is, when $H(p + \lambda) = H(p)$, for all $p \in \mathbb{R}^2$ and $\lambda \in \Lambda = \pi(\Gamma)$, where translation by periods has been written additively. For a face U and its translate $U + \lambda$, this condition implies that:

$$\begin{aligned} v_{U+\lambda} &= v_U \\ C_U - C_{U+\lambda} &= v_U \cdot \lambda \end{aligned} \quad (10)$$

Fig. 10 illustrates a periodic lifting which corresponds to the stress illustrated in Fig. 9(c).

Since Γ -invariant stresses may not always correspond to Γ -invariant liftings, additional properties are needed to characterize stresses induced by Γ -invariant liftings. We proceed now to find them.

Figure 10: A periodic 3D lifting for the stressed framework in Figure 9(c).

Stress induced by a periodic lifting. When expressed as the system $H \equiv (v_U, C_U)_{U \in F}$, a periodic lifting has constant coefficients v_U on Γ -orbits of faces. Thus, there are at most $n^* = \text{card}(F/\Gamma)$ distinct normal directions to lifted faces.

For a closer investigation of the associated stress, we introduce the following notational conventions. A face-path from a face U to a face V will be indicated by $U \rightarrow V$, in particular, a face-path from U to its translate $U + \lambda$ will be indicated by $U \rightarrow U + \lambda$. Sums over face-paths or face-cycles are assumed to be written according to the orientation rule given through tetrads. With this convention, we rewrite the relations (5) and (6) obtained in Section 2 as:

$$\begin{aligned} v_V &= v_U + \sum_{U \rightarrow V} s_i (q_i - p_i)^\perp \\ C_V &= C_U - \sum_{U \rightarrow V} s_i |q_i p_i| \end{aligned} \quad (11)$$

Applying (10) we obtain the following two conditions on the stress s :

$$\sum_{U \rightarrow U+\lambda} s_i(q_i - p_i) = 0 \quad (12)$$

$$\sum_{U \rightarrow U+\lambda} s_i |q_i - p_i| = C_U - C_{U+\lambda} = \mathbf{v}_U \cdot \lambda \quad (13)$$

We summarize these observations as:

Proposition 4. *If the planar non-crossing periodic framework (G, Γ, p, π) has a periodic lifting $H \equiv (\mathbf{v}_U, C_U)_{U \in F}$, then the associated Γ -invariant equilibrium stress s satisfies conditions (12) and (13) for any face U and period vector $\lambda \in \Lambda = \pi(\Gamma)$.*

From constrained stress to periodic lifting. Our next goal is to show that conditions (12) on a Γ -invariant equilibrium stress are sufficient for determining a periodic lifting. Obviously, relations (13) will serve for identifying the lifting data $H \equiv (\mathbf{v}_U, C_U)_{U \in F}$.

Proposition 5. *Let $s = (s_e)_{e \in E}$ be a Γ -invariant equilibrium stress for the planar non-crossing periodic framework (G, Γ, p, π) . If, for some face U_0 and generators λ_1, λ_2 of the period lattice $\Lambda = \pi(\Gamma)$, s satisfies the additional conditions that:*

$$\sum_{U_0 \rightarrow U_0+\lambda_j} s_i(q_i - p_i) = 0, \quad j = 1, 2 \quad (14)$$

then the lifting $H \equiv (\mathbf{v}_U, C_U)$ defined, for all $\lambda \in \Lambda$, by:

$$\mathbf{v}_U \cdot \lambda = \sum_{U \rightarrow U+\lambda} s_i |q_i - p_i| = C_U - C_{U+\lambda}$$

is a periodic lifting inducing s , determined up to a choice of constant $C_0 = C_{U_0}$.

Proof. Let us assume that $s = (s_i)_i$ is a Γ -invariant equilibrium stress which satisfies (14) for some face U_0 and two generators λ_1, λ_2 of the periodicity lattice $\Lambda = \pi(\Gamma)$. We first show that our assumption implies that condition (12) is satisfied for all U and $\lambda \in \Lambda$. It is clearly satisfied for U_0 and all $\lambda \in \Lambda$ since the edge vectors implicated in the sum are, by periodicity, the same linear combination with integer coefficients as given in $\lambda = n_1 \lambda_1 + n_2 \lambda_2$.

Suppose next that V is adjacent to U_0 and consider the face-cycle $U_0 \rightarrow V \rightarrow V + \lambda \rightarrow U_0 + \lambda \rightarrow U_0$. Again, by periodicity in the framework, the edge vector implicated for $U_0 \rightarrow V$ is the opposite of the edge vector implicated for $V + \lambda \rightarrow U_0 + \lambda$ and (12) holds for V . This is enough for our claim since G and G^* are connected.

As shown in the proof of Prop. 2, for any initial choice $(\mathbf{v}_{U_0}, C_{U_0}) = (\mathbf{v}_0, C_0)$, we obtain a lifting $H \equiv (\mathbf{v}_U, C_U)$ inducing s . We aim at finding a periodic representative in this equivalence class.

Let $H \equiv (\mathbf{v}_U, C_U)$ be the lifting under investigation. Relations (11) will hold. Thus \mathbf{v}_U are constant on Γ orbits in F . We show now that the function

$$\mathcal{N}_U(\lambda) = \sum_{U \rightarrow U+\lambda} s_i |q_i - p_i|$$

is independent of the orbit representative U . Indeed, using (12) we find

$$\begin{aligned} & \sum_{(U+\mu) \rightarrow (U+\mu)+\lambda} s_i |q_i + \mu - p_i + \mu| = \\ &= \sum_{U \rightarrow U+\lambda} s_i |q_i - p_i| + \sum_{U \rightarrow U+\lambda} s_i |q_i - p_i| \mu = \sum_{U \rightarrow U+\lambda} s_i |q_i - p_i| \end{aligned} \quad (15)$$

Moreover, $\mathcal{N}_U(\lambda)$ is linear in λ and by (11):

$$\mathcal{N}_U(\lambda) = C_U - C_{U+\lambda} \quad (16)$$

By comparing $C_V - C_U$ and $C_{V+\lambda} - C_{U+\lambda}$ based on (11), we obtain

$$\begin{aligned} C_{V+\lambda} - C_{U+\lambda} &= - \sum_{U \rightarrow V} s_i |q_i + \lambda \cdot p_i + \lambda| = C_V - C_U - \sum_{U \rightarrow V} s_i |q_i - p_i \cdot \lambda| = \\ &= C_V - C_U - \sum_{U \rightarrow V} s_i (q_i - p_i)^\perp \cdot \lambda = C_V - C_U - (\mathbf{v}_V - \mathbf{v}_U) \cdot \lambda \end{aligned}$$

This gives

$$\mathcal{N}_V(\lambda) = C_V - C_{V+\lambda} = C_U - C_{U+\lambda} + (\mathbf{v}_V - \mathbf{v}_U) \cdot \lambda = \mathcal{N}_U(\lambda) + (\mathbf{v}_V - \mathbf{v}_U) \cdot \lambda$$

and shows that

$$\mathcal{N}_V(\lambda) - \mathcal{N}_U(\lambda) = (\mathbf{v}_V - \mathbf{v}_U) \cdot \lambda \quad (17)$$

This means that if we choose our initial $\mathbf{v}_0 = \mathbf{v}_{U_0}$ by $\mathbf{v}_0 \cdot \lambda = \mathcal{N}_{U_0}(\lambda)$, for all $\lambda \in \Lambda$, the resulting lifting will be periodic. \square

In the next section we prove that this type of constrained stress is precisely the periodic stress implicated in the deformation theory of periodic frameworks introduced in [3].

4 Periodic deformations and stresses

We have arrived at one of the most important aspects of this paper, which brings in the connection with the infinitesimal rigidity or flexibility of a periodic framework. The application to periodic pseudo-triangulations and expansive mechanisms presented in the next section relies on this correspondence.

Periodic deformations. A planar framework (G, Γ, p, π) was defined by a placement of vertices $p : V \rightarrow \mathbb{R}^2$ and a faithful representation $\pi : \Gamma \rightarrow \mathcal{T}(\mathbb{R}^2)$ of the periodicity group by a rank two lattice of translations $\Lambda = \pi(\Gamma)$, with the necessary compatibility relation. In the framework, the edges of the graph are now seen as segments of fixed length, forming what is called in rigidity theory a *bar-and-joint structure*. According to our periodic deformation theory, introduced in [3] and pursued in [4, 6], a *periodic bar-and-joint framework* is said to be *periodically flexible* if there exists a continuous (or equivalently smooth) family of placements, parametrized by time t , $p_t : V \rightarrow \mathbb{R}^2$ with $p_0 = p$, which is not given by global rigid motions and satisfies two conditions: (a) it maintain the lengths of all the edges $e \in E$, and (b) it maintains periodicity under Γ , via faithful representations $\pi_t : \Gamma \rightarrow \mathcal{T}(\mathbb{R}^2)$ which *may change with t and give a corresponding variation of the periodicity lattice $\Lambda_t = \pi_t(\Gamma)$* .

To represent π_t we first choose two generators for the periodicity lattice Γ . The corresponding lattice generators $\lambda_1(t)$ and $\lambda_2(t)$ at time t may be viewed as the columns of a non-singular 2×2 matrix denoted, for simplicity, with the same symbol $\Lambda_t \in GL(2)$. The infinitesimal deformations of the placement (p_t, π_t) are described using a complete set of n vertex representatives for V/Γ , i.e. the vertex positions are parametrized by $(\mathbb{R}^2)^n$. The m representatives for edges mod Γ are then expressed using the vertex parameters and the periodicity matrix Λ . An edge representative β originates in one of the chosen vertex representatives $i = i(\beta)$ and ends at some other vertex representative $j = j(\beta)$ plus some period Λc_β , where c_β is a column vector with two integer entries. The edge vectors e_β , $\beta \in E/\Gamma$ thus have the form:

$$e_\beta = (x_j + \Lambda c_\beta) - x_i, \quad \beta \in E/\Gamma \quad (18)$$

By taking the squared length of the m edge representatives, we obtain a map:

$$(\mathbb{R}^2)^n \times GL(2) \rightarrow \mathbb{R}^m \quad (19)$$

and the differential of this map at the point under consideration (i.e. the point of $(\mathbb{R}^2)^n \times GL(2) \subset \mathbb{R}^{2n+4}$ corresponding to the framework (p, π)), seen as a matrix with m rows and $2n + 4$ columns is called the *rigidity matrix* $\mathbf{R} = \mathbf{R}(G, \Gamma, p, \pi)$ of the framework. The row corresponding to the edge described above has the form:

$$(0 \dots 0 -e'_\beta \ 0 \dots 0 e'_\beta \ 0 \dots 0 c^1_\beta e'_\beta \ c^2_\beta e'_\beta) \quad (20)$$

where e'_β is the transpose of the column edge vector e_β and an obvious grouping convention is used for the columns.

The vector space of *infinitesimal periodic motions* (or *infinitesimal periodic deformations*) of the given framework (G, Γ, p, π) can be described as the *kernel* of the rigidity matrix \mathbf{R} and the vector space of *periodic stresses* can be described as the *kernel* of the transpose \mathbf{R}^t . It is understood that a stress described on the m representatives for E/Γ is extended by periodicity to all edges.

Thus, non-trivial periodic stresses express linear dependences between the rows of the rigidity matrix \mathbf{R} . Grouping these dependences over groups of columns corresponding to vertex representatives, we obtain immediately the fact that a periodic stress is necessarily a Γ -invariant equilibrium stress as defined earlier in this paper. However, there are two *additional* vector conditions imposed by the columns corresponding to the infinitesimal variation of the periods.

This sets the stage for a comparison of the periodic stresses reviewed here and the stresses induced by periodic liftings. It is useful to restate now the definition.

Definition 6. A periodic stress for the framework (G, Γ, p, π) is a stress induced from an element in the kernel of the transposed rigidity matrix \mathbf{R}^t , that is, a Γ -invariant equilibrium stress s satisfying the conditions

$$\sum_{\beta \in E/\Gamma} s_\beta c^j_\beta e_\beta = 0 \quad j = 1, 2 \quad (21)$$

with integer coefficients c^j_β as given in the edge description (18).

Remarks. The fact that periodic stresses do not depend on the choices of representatives used in expressing the rigidity matrix follows from the fact that the image of the map (19) and the image of its differential do not depend on these choices. Periodic stresses give the orthogonal complement in \mathbb{R}^m for the image of the differential.

There is an equivalent form for the periodic stress conditions (21), which refers directly to the periods $\lambda_\beta = \Lambda c_\beta$ implicated in the edge descriptions (18). It can be given in terms of tensor products, namely:

$$\sum_{\beta \in E/\Gamma} s_\beta \lambda_\beta \otimes e_\beta = 0 \quad (22)$$

The equivalence follows from a straightforward linear algebra verification.

For a comparison of conditions (14) and (21), we verify first the *persistence of periodic stresses under relaxation of periodicity* from Γ to a subgroup of *finite index* $\tilde{\Gamma} \subset \Gamma$.

Proposition 7. Let $s = (s_\beta)_{\beta \in E}$ be a periodic stress for the periodic framework (G, Γ, p, π) . Let $\tilde{\Gamma} \subset \Gamma$ be a subgroup of finite index. Then s remains a periodic stress for the framework with relaxed periodicity $(G, \tilde{\Gamma}, p, \pi|_{\tilde{\Gamma}})$. Moreover, if a Γ -invariant equilibrium stress becomes periodic for a relaxed periodicity $\tilde{\Gamma} \subset \Gamma$, it is already periodic for Γ .

Proof. A Γ -invariant equilibrium stress is obviously $\tilde{\Gamma}$ -invariant. We look at the columns related to periods in the two rigidity matrices.

Let $\rho = \text{card}(\Gamma/\tilde{\Gamma})$ denote the index of relaxation of periodicity. For the relaxed case we use the following representatives. We first choose representatives in Γ for the elements of the quotient group $\Gamma/\tilde{\Gamma}$. Then, a complete set of vertex representatives mod $\tilde{\Gamma}$ will consist of the representatives chosen mod Γ translated by the periods corresponding to the representatives chosen for $\Gamma/\tilde{\Gamma}$. The subscripts for the relaxed case take the form of pairs i, γ , with the ρ representatives γ covering $\Gamma/\tilde{\Gamma}$.

The proof amounts to verifying identities which can be better controlled when using a tensor product expression for the stress condition on the periodicity columns as in [3], page 2641 and as recalled above in (22). Altogether, with representatives for periodicity Γ given in coordinates as

$$x_i, \quad i = 1, \dots, n$$

$$e_\beta = x_j + \mu_\beta - x_i, \quad i = i(\beta), j = j(\beta), \mu_\beta \in \Lambda$$

we have representatives for periodicity $\tilde{\Gamma}$ given in coordinates as

$$x_{i,\gamma} = x_i + \gamma$$

$$e_{\beta,\gamma} = (x_j + \gamma) + \mu_\beta - (x_i + \gamma) = e_\beta$$

where, for simplicity, no further notational distinction has been made for $\gamma \in \Gamma$ and its image by π . Now, we must take into account that we have unique expressions

$$\mu_\beta = \gamma_\beta + \tilde{\lambda}_\beta \quad (23)$$

with γ_β among the chosen representatives for $\Gamma/\tilde{\Gamma}$ and $\tilde{\gamma} \in \tilde{\Gamma}$. Moreover, as we add representatives, we must record relations of the form

$$\gamma + \gamma_\beta = \lambda_{\beta,\gamma} + \hat{\lambda}_{\beta,\gamma} \quad (24)$$

with $\lambda_{\beta,\gamma}$ among the chosen representatives for $\Gamma/\tilde{\Gamma}$ and $\hat{\lambda}_{\beta,\gamma} \in \tilde{\Gamma}$.

The periodic stress condition for Γ reads

$$\sum_{\beta} s_{\beta} \mu_{\beta} \otimes e_{\beta} = 0 \quad (25)$$

and the one for $\tilde{\Gamma}$ reads

$$\sum_{\beta,\gamma} s_{\beta} (\tilde{\lambda}_{\beta} + \hat{\lambda}_{\beta,\gamma}) \otimes e_{\beta} = 0. \quad (26)$$

In order to see that these conditions are equivalent, we notice that (23) gives

$$\sum_{\beta,\gamma} s_{\beta} \tilde{\lambda}_{\beta} \otimes e_{\beta} = \rho \sum_{\beta} s_{\beta} \mu_{\beta} \otimes e_{\beta} - \rho \sum_{\beta} s_{\beta} \gamma_{\beta} \otimes e_{\beta} \quad (27)$$

Similarly, from (24), we obtain

$$\sum_{\beta,\gamma} s_{\beta} \hat{\lambda}_{\beta,\gamma} \otimes e_{\beta} = \sum_{\beta,\gamma} s_{\beta} (\gamma + \gamma_{\beta} - \lambda_{\beta,\gamma}) \otimes e_{\beta}. \quad (28)$$

Now, we take into account the identity:

$$\sum_{\beta,\gamma} s_{\beta} (\gamma - \lambda_{\beta,\gamma}) \otimes e_{\beta} = 0 \quad (29)$$

which follows from the fact that when operating with an element of a group, one obtains a permutation of the elements in the group. Here, for any β , the two lists γ and $\lambda_{\beta,\gamma}$ of representatives for $\Gamma/\tilde{\Gamma}$ are made of the same elements.

Thus, equations (27), (28) and (29) imply

$$\sum_{\beta,\gamma} s_{\beta} (\tilde{\lambda}_{\beta} + \hat{\lambda}_{\beta,\gamma}) \otimes e_{\beta} = \rho \sum_{\beta} s_{\beta} \mu_{\beta} \otimes e_{\beta} \quad (30)$$

and establish the equivalence of (25) and (26). Our proposition is proven. \square

Comment. Tedious as it may be, this verification has the important consequence that upon relaxation of periodicity, *the dimension of the space of periodic stresses can only go up or stay the same.*

We recall (from [3], page 2641) the relation

$$\sigma - \delta = m - 2n - 4 \quad (31)$$

connecting periodic stresses and infinitesimal deformations, where σ denotes the dimension of the space of periodic stresses and δ is the dimension of the space of infinitesimal periodic deformations. Subtracting the trivial infinitesimal deformations induced by infinitesimal isometries, we obtain:

$$\sigma = \phi - 1 + (m - 2n) \quad (32)$$

where ϕ denotes the dimension of the space of infinitesimal flexes $\phi = \delta - 3$. This formula will be relevant for evaluating behavior under relaxations, with σ and ϕ non-decreasing and the term $(m - 2n)$ multiplied by the index of relaxation ρ .

The last ingredient needed for the proof of our Main Theorem is Lemma 8 below, which can be summarized as saying that *for sufficiently relaxed periodicity $\tilde{\Gamma}$, a complete set of edge representatives can be found that are either inside a fundamental parallelogram $P_{\tilde{\Gamma}}$ or cross the border with an endpoint in a neighboring parallelogram, intersecting one of two prescribed spanning sides.* The Lemma gives a more transparent interpretation for the conditions (21) satisfied by periodic stresses, in terms of a sufficiently large relaxation of periodicity.

Lemma 8. *Let (G, Γ, p, π) be a planar non-crossing periodic framework. One can find generators λ_1, λ_2 for the lattice of periods $\Lambda = \pi(\Gamma)$ and large enough positive integers r_1 and r_2 such that the relaxation of periodicity given by the sublattice $\tilde{\Gamma}$ of index $\rho = r_1 r_2$ of Γ corresponding to the two generators $\tilde{\lambda}_j = r_j \lambda_j$, ($j = 1, 2$) allows the following setup:*

- (a) *a choice of fundamental parallelogram $P_{\tilde{\Gamma}}$ spanned by λ_1, λ_2 such that its boundary avoids vertices and its vertices avoid the framework;*
- (b) *a representation of the associated fundamental parallelogram $P_{\tilde{\Gamma}}$ for $\tilde{\Gamma}$, spanned by $\tilde{\lambda}_j = r_j \lambda_j$, ($j = 1, 2$) as tiled by $\rho = r_1 r_2$ translated copies of the previous parallelogram;*
- (c) *using as representatives of vertex-orbits for Γ all the vertices inside the fundamental parallelogram $P_{\tilde{\Gamma}}$ and then as representatives of vertex-orbits for $\tilde{\Gamma}$ all the vertices inside the fundamental parallelogram $P_{\tilde{\Gamma}}$, a description of edge-orbits as used for the two rigidity matrices (for Γ and the relaxation $\tilde{\Gamma}$) involving, for $\tilde{\Gamma}$, all edges inside the parallelogram in (b) and those crossing the two spanning sides given by $\tilde{\lambda}_j$, $j = 1, 2$;*
- (d) *the $\tilde{\Lambda}$ periods implicated in the description of the above crossing edges are either $-\tilde{\lambda}_1$ or $-\tilde{\lambda}_2$ or possibly their sum $-(\tilde{\lambda}_1 + \tilde{\lambda}_2)$.*

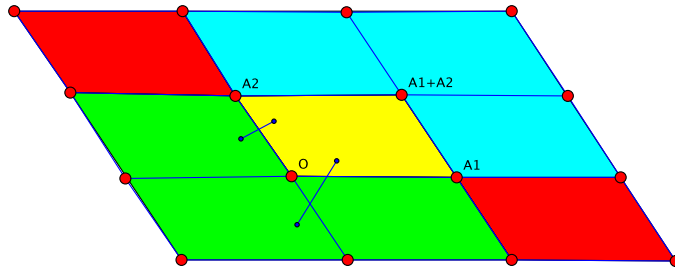


Figure 11: After a first relaxation one obtains the yellow parallelogram as fundamental domain and all edges with one end in it have the other end in it or in one of the eight neighbours.

Comment. The intention, content and principle of proof of this lemma can be elucidated by referring to Figure 11. The aim is to show that convenient choices of lattice generators and relaxation can provide a setting where a fundamental

parallelogram for the relaxed lattice $\tilde{\Lambda}$ is the central (yellow) zone, marked $OA_1(A_1 + A_2)A_2$, with all representatives for edge-orbits contained in the union of the central zone with the three neighbours (in green) around the O corner. With this corner taken as the origin, the two generators $\tilde{\lambda}_j, j = 1, 2$ of $\tilde{\Lambda}$ are represented by vectors $OA_j, j = 1, 2$, we see that any edge in the union of the central zone and the blue zone around $A_1 + A_2$ has, by translation with $-(\tilde{\lambda}_1 + \tilde{\lambda}_2)$, an equivalent representative in the desired union (of yellow and green). Thus, the lemma can be proven by showing that convenient choices lead to a setting with no edges crossing from the central (yellow) zone to the remaining two (red) zones abutting corners A_1 and A_2 . In fact, by translation with $\tilde{\lambda}_2 - \tilde{\lambda}_1$, it is enough to insure that no edge crosses from the central parallelogram to the (red) neighbor abutting at A_1 .

Proof. A generic choice of origin O will easily satisfy the avoidances desired in (a) when we represent the periodicity vectors as emanating from O . Assuming such a choice, *rational* will refer to the common rational grid determined by the initial periodicity lattice (and containing all its relaxations).

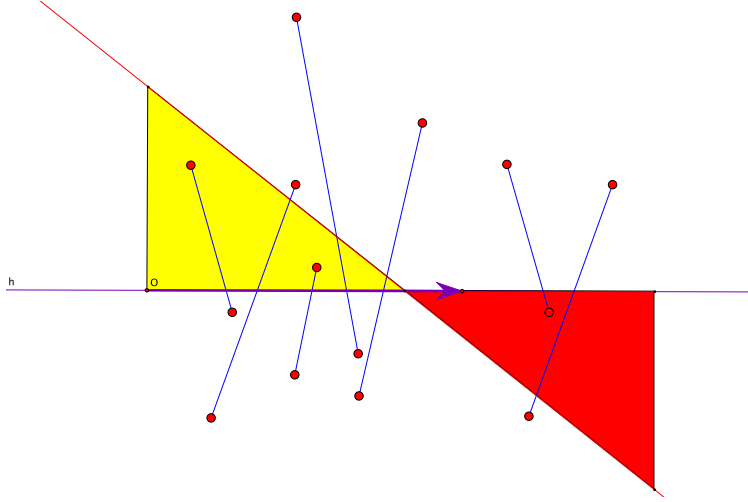


Figure 12: The horizontal line h intersected by edges. The marked vector is a period along h . Since all edges have nearly vertical directions a sufficiently more slanted line achieves the property that no edge crosses from the yellow zone to the red zone.

Since there is a finite number of edge vectors, their length is bounded and it is clear that for any initial choice of fundamental parallelogram P_Γ we can find a relaxation with all edges originating in P_Γ ending either in itself or one of the eight neighboring translated copies. Thus, what remains to be argued is how to obtain the additional property that no edge crosses from the central parallelogram $P_\Gamma = OA_1(A_1 + A_2)A_2$ to the (red) neighbor abutting at A_1 .

For this purpose, we remark that our problem is not affected by a rational linear transformation and we may use this invariance to arrange and assume that all our edge vectors are, in direction, sufficiently close to a single direction, which we designate as our “vertical”. We look now at the line through O which is orthogonal to our vertical and refer to it as our “horizontal” line.

Let us depict (with their periodicity along this horizontal) all the edges crossing it, as illustrated in Figure 12. Then, we can take a more slanted rational line with respect to the vertical as our direction for $\tilde{\lambda}_2$. Under our assumptions, this choice obtains the property that no edge crosses from the yellow region to the red region. We can find first Γ -periods along the horizontal and slanted directions. In fact, by the relative freedom we have when choosing the slanted direction, we may assume that we obtain generators $\lambda_j, j = 1, 2$. As already explained, a relaxation $\tilde{\Gamma}$ can be found which satisfies the setting in Figure 11 and the additional property that all edge representatives for $\tilde{\Gamma}$ can be found in the union of the four parallelograms around O . This completes the proof of our lemma. \square

All the elements for the correspondence between periodic liftings and periodic stresses are now in place to prove:

Main Theorem *Let (G, Γ, p, π) be a planar non-crossing periodic framework. A stress induced by a periodic lifting is a periodic stress and conversely, any periodic stress is induced by a periodic lifting, determined up to an arbitrary additive constant. The correspondence relates the stress signs to the mountain/valley types of the lifted edges.*

Proof. We use Proposition 7 and the setting described in Lemma 8 obtained after an adequate relaxation of periodicity $\tilde{\Gamma} \subset \Gamma$ with generators related by $\tilde{\lambda}_j = r_j \lambda_j, j = 1, 2$. We first observe that, for periodicity $\tilde{\Gamma}$ the stated correspondence between periodic liftings and periodic stresses becomes obvious, since conditions (21) and (14) ask exactly the same thing: that the stress-weighted sums of edges implicated along $U \rightarrow U + \tilde{\lambda}_j, j = 1, 2$ be zero. The case of full periodicity Γ now follows from Proposition 7 and the corresponding fact that a Γ -invariant lifting which is $\tilde{\Gamma}$ -periodic for some relaxation $\tilde{\Gamma} \subset \Gamma$, must be already Γ -periodic, as immediately seen from conditions (14). The sign relationship follows from Proposition 3. \square

This concludes the proof. We turn now to applications of our Main Theorem.

5 Periodic pointed pseudo-triangulations

In this section we define *periodic pointed pseudo-triangulations* or, for short, *periodic pseudo-triangulations*. We prove properties analogous to those possessed by their finite counterparts [47, 48], with respect to expansive motions. In addition, we show some entirely new properties, specific to the periodic setting, related to *ultrarigidity*.

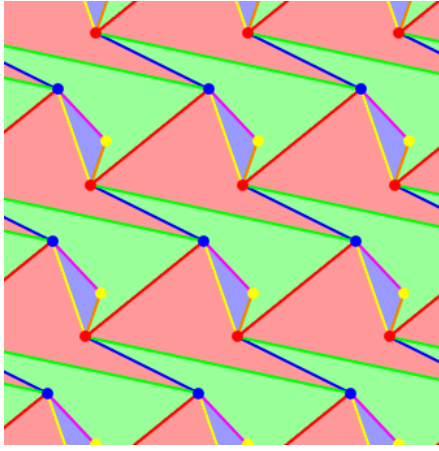


Figure 13: A periodic pseudo-triangulation with $(n, m, n^*) = (3, 6, 3)$.

A *pseudo-triangle* is a simple closed planar polygon with exactly three internal angles smaller than π . A set of vectors is *pointed* if there is no linear combination with strictly positive coefficients that sums them to 0. Equivalently, a set of pointed vectors lie in some half-plane determined by a line through their common origin. A planar non-crossing periodic framework (G, Γ, p, π) is a *periodic pointed pseudo-triangulation* when all faces are pseudo-triangles and the framework is pointed at every vertex. Thus, at every vertex, the incident edges lie on one side of some line passing through the vertex. As in the finite case, pointedness at every vertex is essential. Pseudo-triangular faces mark the ‘saturated’ stage where no more edge orbits can be inserted without violating non-crossing or pointedness. An illustration for $n = 3$ is given in Figure 13. We show that periodic pointed pseudo-triangulations, viewed as bar-and-joint mechanisms, satisfy two remarkable rigidity-theoretic properties: they have the right number of edges to be flexible mechanisms with exactly one degree of freedom (in the finite case [47, 48], the flexible mechanisms were obtained after removing a convex hull edge), and they encounter no singularities in their deformation for as long as they remain pseudo-triangulations.

Proposition 9. *A periodic pseudo-triangulation has $m = 2n$, that is, the number of edge orbits $m = \text{card}(\mathcal{E}/\Gamma)$ is twice the number of vertex orbits $n = \text{card}(\mathcal{V}/\Gamma)$.*

Proof. The proof combines Euler’s formula on the torus (9) with counting the *corners* of pseudo-triangular faces. A corner is an angle smaller than π at some vertex of a given face.

We denote by d_v the degree of a vertex (valency) in the quotient multi-graph G/Γ , and use the classical formula $\sum_{v \in G/\Gamma} d_v = 2m$ relating the degree sum to the number of edges in a graph. Since there are $d_v - 1$ corners incident to each vertex, we obtain a second relation:

$$\sum_{v \in G/\Gamma} d_v = n + 3n^*, \text{ hence } 2m = n + 3n^*$$

Combined with Euler’s formula (9) $n - m + n^* = 0$ between the number of vertex, edge and face orbits, this yields $m = 2n = 2n^*$. An illustration for $n = 3$ is given in Figure 13. \square

Comment: Since for pseudo-triangulations we have $m = 2n$, formula (32) relating the dimensions ϕ and σ of the spaces of periodic flexes and respectively periodic stresses implies that:

$$\sigma = \phi - 1 \tag{33}$$

Moreover, the relation remains unaffected by relaxations of periodicity of finite index. We will make use of this observation further down and in the next section.

Proposition 9 shows that periodic pointed pseudo-triangulations have the right number of edges to provide smooth one-degree-of-freedom periodic mechanisms. The next proposition shows that this is actually the case. The argument amounts to showing that they have no non-trivial periodic stress.

Proposition 10. *A periodic pseudo-triangulation cannot have nontrivial periodic stresses. The local deformation space is therefore smooth and one-dimensional and continues to be so as long as the deformed framework remains a pseudo-triangulation. The same statement holds true for any relaxation of periodicity $\tilde{\Gamma} \subset \Gamma$ of finite index.*

Proof. A nontrivial stress would give, by our Main Theorem, a periodic lifting. Such a lifting must have at least one vertex achieving the global maximum and another achieving the global minimum. However, with an angle exceeding π on some face around each vertex, neither a maximum nor a minimum is possible. Thus, the edge length conditions are infinitesimally independent and the implicit function theorem gives a local deformation space which is smooth and of dimension one. \square

We present now a proof of a most remarkable property of periodic pseudo-triangulations.

Theorem 11. (Periodic pointed pseudo-triangulations have expansive 1dof flexes) *Let (G, Γ, p, π) be a planar periodic pseudo-triangulation. Then the framework has a one-parameter periodic deformation, which is expansive for as long as it remains a pseudo-triangulation.*

Proof outline. We compare the infinitesimal variation of the distance between two pairs of vertices (which do not belong to rigid subcomponents) and show that one cannot increase while the other decreases. An argument already used by Maxwell in [37] shows that it is enough to reason with two pairs of vertices which do not create self-crossing when inserted as edges (and replicated by periodicity). After one edge insertion, the framework becomes infinitesimally rigid and after the second edge insertion it becomes periodically stressed, with a one dimensional periodic stress space. Since either pointedness or non-crossing of edges is violated only by the newly inserted edges, and since a pointed vertex cannot be a local extremum for the height function, we infer that the associated periodic lifting must have its global maximum and global minimum at two of the vertices in the two added edges. Considerations of stress sign and of the related mountain/valley type of the lifted edges, as summarized in Prop. 3) show that the new edge orbits have stress factors of opposite signs. This in turn implies (by linear programming duality) that the infinitesimal variation of the distance between the two pairs of vertices is of the same kind: expansion or contraction.

Proof details. We develop our arguments in a sequence of Lemmas. First, we consider what happens after one edge is inserted in a non-crossing manner.

Lemma 12. *The periodic framework obtained by inserting a new Γ -orbit of non-crossing edges in a periodic pointed pseudo-triangulation is minimally rigid, that is, infinitesimally rigid with $2n + 1$ edge orbits.*

Proof. Relation (32) for the extended framework implies that the dimension of the space of periodic flexes equals the dimension of the space of periodic stresses, i.e. $\sigma = \phi$. We argue now that no nontrivial periodic stress exists, i.e. $\sigma = 0$. Indeed, a nontrivial periodic stress would give a nontrivial periodic lifting. The latter must have a global maximum vertex and a global minimum vertex. Since pointed vertices cannot be either maxima or minima, the two extrema must occur at the endpoints of the new edge. However, a maximum vertex requires at least three non-pointed ‘mountain’ edges and a minimum vertex requires at least three non-pointed ‘valley’ edges. The new edge would have to be a ‘mountain’ because of the maximum at one end and would have to be a ‘valley’ because of the minimum at the other end. This contradiction proves the lemma. \square

We analyze now what happens after a non-crossing second edge orbit insertion. By inserting this new edge and its Γ -orbit in the minimally rigid framework obtained above, we must have a one-dimensional space of periodic stresses since the space of infinitesimal flexes remains null.

Lemma 13. *If we add two new edge orbits to a periodic pseudo-triangulation, then we cannot have the same sign for the stress factors on the two new edge orbits inserted in the pseudo-triangulation.*

Proof. We argue first for the case of no common vertex mod Γ for the two new edges. Then, as shown above in Lemma 12, we cannot have the maximum and the minimum at the two ends of the same new edge. Thus the edge reaching to the maximum is a ‘mountain’ and the other one, reaching to the minimum, is a ‘valley’.

In case the two new edges share a vertex, we note that at least one extremum must be at some unshared vertex. But then the other extremum cannot be at the shared vertex and must be at the other unshared vertex. Thus, as above, the two edges must be a ‘mountain’ and a ‘valley’. \square

With opposite signs confirmed for the stress factors on the two new edges, we look now at the infinitesimal displacement induced by the infinitesimal deformation of the pseudo-triangulation on these same edges.

For the framework with two new edge orbits, the non-zero stress vector must be orthogonal on the image of the corresponding rigidity matrix. In particular, it must be orthogonal on the image vector obtained by evaluating the rigidity matrix on the infinitesimal displacement induced by the pseudo-triangulation. But all entries corresponding to ‘old’ edge orbits, that is, edge orbits in the pseudo-triangulation, will be zero. With opposite stress signs for the two new edges, orthogonality requires the *same* sign for the two non-zero entries. This means: simultaneous infinitesimal expansion or simultaneous infinitesimal contraction.

By now, the following result has been established.

Proposition 14. *Let (G, Γ, p, π) be a planar pseudo-triangulation. Let two pairs of vertices be such that both corresponding distances vary infinitesimally under the infinitesimal deformation of the pseudo-triangulation. Assume that inserting the corresponding two edges (and their Γ orbits) does not produce self-crossing. Then, the two edges vary infinitesimally in the same way: both expand or both contract.*

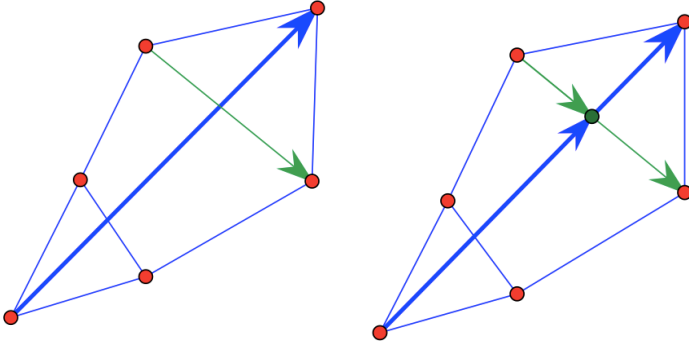


Figure 14: Bow’s method allows a reduction of stress considerations to a non-crossing case. One step is illustrated above and another one would eliminate self-crossing.

As a final step to complete the proof of Theorem 11, we want to remove the assumption that the two new edges maintain the non-crossing nature of the periodic framework, and thus to prove the full expansive character of the pseudo-triangulation mechanism. In fact, because we are comparing the stresses and infinitesimal flexes of pairs of edges, it suffices to assume that the first one is not crossing the rest, hence we only need to remove the non-crossing assumption for the second inserted edge.

Figure 14 illustrates the (descending) inductive step whereby stress considerations in a

situation where an edge intersects several other edges can be reduced to an equivalent situation without self-crossing. In [37] the procedure is called Bow’s method.

We briefly review the nature of the argument by explaining the stress correspondence for the step shown in Figure 14. A new vertex has been inserted at the last crossing of the marked edge vectors. With obvious notations (by which an edge α is split into two edges α_1 and α_2 , and similarly for the edge β), we have, for the corresponding edge vectors:

$$e_\alpha = e_{\alpha_1} + e_{\alpha_2} \quad \text{and} \quad e_\beta = e_{\beta_1} + e_{\beta_2}$$

Geometric stress conditions at the new vertex require

$$s_{\alpha_1} e_{\alpha_1} = s_{\alpha_2} e_{\alpha_2} \quad \text{and} \quad s_{\beta_1} e_{\beta_1} = s_{\beta_2} e_{\beta_2}$$

and the correspondence of stresses (valid for periodic stresses as well) is expressed through the formulae:

$$s_\alpha e_\alpha = s_{\alpha_1} e_{\alpha_1} = s_{\alpha_2} e_{\alpha_2} \quad \text{and} \quad s_\beta e_\beta = s_{\beta_1} e_{\beta_1} = s_{\beta_2} e_{\beta_2} \quad (34)$$

with all other stress factors (on edges different from α and β) remaining the same.

Relations (34) show that in this isomorphic correspondence of stresses, the sign of the stress factors along the fragmented edges is the same as in the initial framework, hence the argument given in Lemma 13 carries over. Thus, whether crossing or not crossing other edges, the insertion of a second new orbit of edges in a periodic pseudo-triangulation produces a stressed framework with opposite signs for the stress factors on the two added edge orbits. As shown, this implies the same type of infinitesimal variation of the two corresponding vertex distances when deforming the periodic pseudo-triangulation. The limit case, when the inserted edge passes through one or several vertices of the framework is treated similarly. In fact, the step for crossing through a vertex is simpler and only requires the splitting of the inserted edge into two edges. This concludes the proof of Theorem 11. \square

Comment. We retain from this section the conspicuous property of periodic pseudo-triangulations of maintaining the same deformation space under arbitrary relaxations of periodicity of finite index. We make use of this property in the final section, where we uncover the ultrarigidity of a family of frameworks obtained from pseudo-triangulations.

We conclude the paper with two applications motivated by questions arising in materials science.

6 Expansive and auxetic paths

Periodic pseudo-triangulations determine a large, yet distinctive class of planar periodic frameworks. We have presented above some of their remarkable properties: their local deformation space is smooth and one-dimensional and this deformation path is *expansive* as long as the framework remains a pseudo-triangulation, that is, for the proper sense of variation of the parameter, all distances between pairs of vertices increase or stay the same. Moreover, a relaxation of periodicity to a subgroup of finite index does not change these characteristics.

In this section we emphasize, from a *purely geometric perspective*, the relevance of periodic pseudo-triangulations and their expansive paths for what has been termed *auxetic behavior* in materials science.

In materials science, the term *auxetic*, suggestive of increase or growth, refers to solids with a negative Poisson's ratio [32, 21]. Quoting from [33]: “A negative Poisson's ratio in a solid defines the counter-intuitive lateral widening upon application of a longitudinal tensile strain.” For anisotropic solids, such as single crystals, “the variation of elastic moduli with direction is also relevant” (*ibid.* p.6445). Thus, auxetic behavior is primarily defined in terms of physical characteristics of the material under consideration. However, in many instances with pronounced geometric structural underpinnings, geometrical explanations have been proposed [51, 24, 25, 39].

In our context, which is that of periodic frameworks and their deformations, we must rely on a comprehensive but strictly geometrical concept of auxetic path. This concept is introduced in our companion paper [8] and will be briefly reviewed here.

The geometric approach to auxetics presented in [8] is formulated in arbitrary dimension d and addresses one-parameter deformations of a given periodic framework in \mathbb{R}^d . Two aspects may be emphasized from the start: (i) that when present, the auxetic property refers to the deformation path under consideration and not the framework itself, which oftentimes allows other deformation paths which need not be auxetic and (ii) the auxetic character is an expression of a particular type of variation of the periodicity lattice along the deformation path.

Mathematically, we rely on the notion of *contraction operator* in a Hilbert space, which we recall below. For our purposes, \mathbb{R}^d with the standard norm $|x| = (x \cdot x)^{1/2}$, will suffice. Let $T : \mathbb{R}^d \rightarrow \mathbb{R}^d$ be a linear operator. Then, the operator norm, or simply the norm of T is

$$\|T\| = \sup_{|x| \leq 1} |Tx| = \sup_{|x|=1} |Tx|$$

T is called a contraction operator, or simply a contraction, when $\|T\| \leq 1$.

Comment. From $|Tx| \leq \|T\| \cdot |x|$ it follows that contraction operators are characterized by the property of taking the unit ball to a subset of itself. For a *strict contraction* one requires $\|T\| < 1$.

Let us assume now that we have a *one-parameter* deformation $(G, \Gamma, p_\tau, \pi_\tau)$, $\tau \in (-\varepsilon, \varepsilon)$ of a periodic framework in \mathbb{R}^d . The corresponding periodicity lattices $\Lambda_\tau = \pi_\tau(\Gamma)$, offer by themselves a way to compare any two sequential moments $\tau_1 < \tau_2$ by looking at the *unique linear operator* $T_{\tau_2\tau_1}$ defined by

$$\pi_{\tau_1} = T_{\tau_2 \tau_1} \circ \pi_{\tau_2} \quad (35)$$

Definition 15. A differentiable one-parameter deformation $(G, \Gamma, p_\tau, \pi_\tau), \tau \in (-\varepsilon, \varepsilon)$ of a periodic framework in \mathbb{R}^d is called an *auxetic path*, or simply *auxetic*, when for any $\tau_1 < \tau_2$, the linear operator $T_{\tau_2 \tau_1}$ defined by (35) is a contraction.

In [8] we prove the equivalence of this *geometric criterion for auxetic paths* with the following characterization involving the evolution of the Gram matrix of a generating basis for the period lattice of the framework. With conventions already used in previous sections, after choosing an independent set of generators for Γ , the image $\pi_\tau(\Gamma)$ is completely described via the $d \times d$ matrix Λ_τ with column vectors given by the images of the generators under π_τ . The associated Gram matrix will be

$$\omega(\tau) = \Lambda_\tau^t \Lambda_\tau.$$

Proposition 16. A deformation path $(G, \Gamma, p_\tau, \pi_\tau), \tau \in (-\varepsilon, \varepsilon)$ is auxetic if and only if the curve of Gram matrices $\omega(\tau)$ defined above has all its tangents in the cone of positive semidefinite symmetric $d \times d$ matrices.

Remarks. This infinitesimal characterization of auxetic paths is easily seen to be independent of the choice of generators used for obtaining the Gram matrices. There is an obvious analogy here with *causal lines* in special relativity. Causal paths must have all their tangents in the *light-cone* of Minkowski space-time. Likewise, auxetic paths must have all their tangents $\frac{d\omega}{d\tau}(\tau)$ in the cone $\Omega(d)$ of positive semidefinite symmetric matrices. For the geometry and linear symmetries of this cone see [26, 1].

This criterion is particularly convenient when frameworks and deformations are described as in [6] using parameters in $(\mathbb{R}^d)^{n-1} \times \Omega(d)$. The coordinates in $(\mathbb{R}^d)^{n-1}$ describe the position of $(n-1)$ chosen representatives for vertex orbits relative to the periodicity basis Λ which can be retrieved, up to orthogonal transformations from its Gram matrix $\omega = \Lambda^t \Lambda \in \Omega(d)$. The orbit of a first vertex representative is identified with the periodicity lattice.

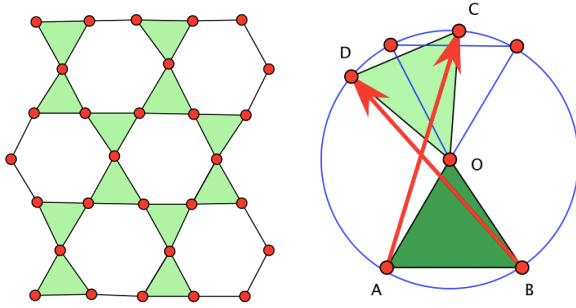


Figure 15: (Left) The Kagome framework. (Right) Parametrizing the deformation of the Kagome framework. Triangle OAB is fixed, and triangle OCD rotates with an angle θ from the standard position. The two generators of the periodicity lattice are marked as arrows.

subset. Since some integer multiple of such a point is a period at moment τ_2 , and this period, as a distance between two vertices in a vertex orbit, can only decrease or preserve its norm when mapped by $T_{\tau_2 \tau_1}$ to the corresponding period at moment τ_1 , we see that a dense subset of points in the unit ball must be mapped to the unit ball. This is enough to conclude that $\|T\| \leq 1$. \square

We now address the comparison of expansive and auxetic paths.

Theorem 17. Let $(G, \Gamma, p_t, \pi_t), t \in (-\varepsilon, \varepsilon)$ be a one-parameter deformation of a periodic framework in \mathbb{R}^d . If the path is expansive, that is, if the distance between any pair of vertices increases or stays the same for increasing t , then the path is also auxetic. However, auxetic paths need not be expansive.

Proof. As emphasized earlier, the auxetic property depends only on the curve $\omega(\tau)$ and it will be enough to use the expansive property on one orbit of vertices. We have to verify that the operator $T_{\tau_2 \tau_1}$ which takes the period lattice basis Λ_{τ_2} to the period lattice basis Λ_{τ_1} is a contraction for $\tau_2 > \tau_1$.

Let us observe that in the unit ball of \mathbb{R}^d , the vectors with rational coordinates relative to the basis Λ_{τ_2} give a dense subset. Since some integer multiple of such a point is a period at moment τ_2 , and this period, as a distance between two vertices in a vertex orbit, can only decrease or preserve its norm when mapped by $T_{\tau_2 \tau_1}$ to the corresponding period at moment τ_1 , we see that a dense subset of points in the unit ball must be mapped to the unit ball. This is enough to conclude that $\|T\| \leq 1$. \square

The fact that small auxetic deformations need not be expansive is to be expected from the fact that the relative motion of different vertex orbits is not sufficiently constrained by the auxetic property. A simple example is offered by the Kagome framework in dimension two. The Kagome framework is a familiar planar example and has been explored from various points of view [27, 28, 31, 19, 49]. The auxetic character of its one-parameter deformation is frequently

mentioned [24, 38, 39]. The brief review here is meant to offer a simple illustration of our geometric criterion for auxetic paths and to distinguish the expansive portions of this deformation.

Example 2. (Deforming the Kagome framework) *The basic elements for describing the framework are shown in Figure 15. The parametrization for the deformation is described in Figure 15. Triangles OAB and OCD are assumed congruent and equilateral. With origin at O , coordinates may be chosen so that $A = (-1, 0)$ and $B = -1/2(1, \sqrt{3})$. The resulting Gram matrix for the marked periods and a rotation of triangle OCD with angle θ from the standard position is:*

$$\omega(\theta) = (1 + \cos \theta) \begin{pmatrix} 2 & 1 \\ 1 & 2 \end{pmatrix} \quad (36)$$

with:

$$\frac{d\omega}{d\theta}(\theta) = -\sin \theta \begin{pmatrix} 2 & 1 \\ 1 & 2 \end{pmatrix} \quad (37)$$

The image of the deformation path in the positive semidefinite cone $\Omega(2)$ for $\theta \in (-\pi, \pi)$ is the segment from the null matrix to $\omega(0)$, covered twice. The standard position $\theta = 0$ is a maximum for the area of a fundamental parallelogram. Proposition 16 shows immediately that the symmetric paths obtained for θ running from π to 0, respectively $-\pi$ to 0, are auxetic.

The range of θ corresponding to periodic pseudo-triangulations is the union $(-2\pi/3, -\pi/3) \cup (\pi/3, 2\pi/3)$. Expansive behavior cannot occur beyond this range, since the distance variation between the two pairs of vertices (A, D) and (B, C) has opposite character when θ is in the complement: when one segment increases, the other one decreases.

The framework shown in Fig. 5 is one of the emblematic illustrations of auxetic behavior in dimension two. It is called a *reentrant honeycomb* in [42]. It is often used to illustrate auxetic behavior: a vertical stretch involves a necessary horizontal expansion.

Example 3. (The “reentrant honeycomb”) *The framework in Fig. 5 has two degrees of freedom and not all deformations paths are auxetic. The expansive possibilities can be explained in terms of the two possible refinements to periodic pseudo-triangulations shown in Fig. 16.*

The framework with all edges of the same length may be obtained by deforming the 2-diamond framework (the regular hexagonal structure) [9]. An auxetic path would result from a ‘vertical stretch’ which visibly entails a horizontal expansion as well. However, an understanding of all expansive infinitesimal deformations within all auxetic possibilities requires some elaboration [10]. Here, we limit our discussion to the following remarks on the basic role of periodic pseudo-triangulations.

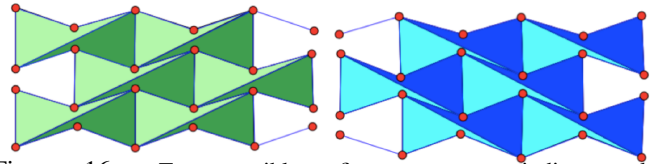


Figure 16: Two possible refinements to periodic pseudo-triangulations of the ‘reentrant’ structure of hexagons in Figure 5.

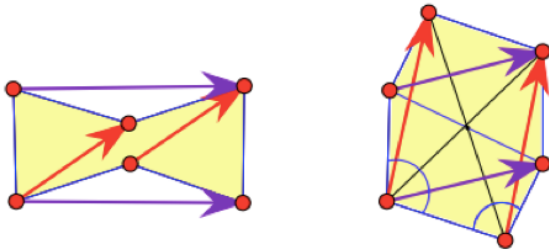


Figure 17: For the ‘reentrant’ structure of hexagons in Figure 5, which has two degrees-of-freedom, the figure on the right marks two angles which may be used as parameters. By maintaining the central symmetry of the hexagon, the two depicted pairs of periods remain equal vectors.

The local deformation space of the framework is smooth and two-dimensional. Indeed, by pointedness at every vertex, there can be no periodic stress. Since $n = 2$ and $m = 3$, there are two degrees of freedom. Figure 16 marks the two angles which may be used as parameters. By maintaining the central symmetry of the hexagon, the two depicted pairs of periods remain equal vectors. The framework can be refined in two ways to a periodic pseudo-triangulation by insertion of an additional orbit of edges. It can be shown that the expansive infinitesimal deformations determined by these two pseudo-triangulations give the extremal rays of the infinitesimal expansive cone of the framework. For the larger auxetic cone, we refer to [8].

7 Ultrarigidity

In this final application we discuss the relevance for ultrarigidity of the other remarkable feature of periodic pseudo-triangulations, namely the invariance of their local deformation space under arbitrary relaxations of the periodicity group to subgroups of finite index $\tilde{\Gamma} \subset \Gamma$.

The deformation theory of periodic frameworks, as founded and developed in [3, 4, 6], is formulated for periodic graphs understood as pairs (G, Γ) : the periodicity group Γ is an essential structural part of the data. The study of phenomena involving changes in periodicity or asymptotic behavior under successive relaxations of periodicity may be intricate. We have recently proposed [5] the notion of *ultrarigidity* for expressing the property of a periodic framework (G, Γ, p, π) of being infinitesimally rigid and remaining so under any relaxation of periodicity to $\tilde{\Gamma} \subset \Gamma$ of finite index.

Ultrarigidity is easily recognized in frameworks made of some rigid finite parts which are rigidly connected between themselves. However, this is not the general case, as the following constructions, based on planar periodic pseudo-triangulations, will demonstrate.

Let (G, Γ, p, π) be a periodic pseudo-triangulation. Then, the local deformation space is a smooth curve. The infinitesimal deformation corresponding to this one degree of freedom mechanism must induce on some pairs of vertices a non-trivial infinitesimal variation of length. Then, as argued above in Lemma 12, by selecting such a pair of vertices and by inserting the corresponding orbit of edges, we obtain a *minimally rigid framework*, that is, an infinitesimally rigid framework with $m = 2n + 1$.

In fact, the resulting framework is *ultrarigid*. Indeed, for any relaxation of periodicity to a subgroup $\tilde{\Gamma} \in \Gamma$ of finite index, the older framework with relaxed periodicity remains a pseudo-triangulation and has the same local deformation space. Thus, the distance between the selected pair of vertices varies infinitesimally and the same argument applies, showing that insertion of the corresponding $\tilde{\Gamma}$ edge-orbit already yields an infinitesimally rigid framework. This concludes the proof of the following result.

Proposition 18. *Let (G, Γ, p, π) be a periodic pseudo-triangulation in which we consider a pair of vertices with a non-trivial infinitesimal variation in distance under the infinitesimal deformation of the framework. Then the insertion of the corresponding Γ orbit of edges results in an ultrarigid framework.*

Thus, periodic pseudo-triangulations and insertion choices provide endless examples of ultrarigid frameworks.

Example 4. (An ultrarigid periodic framework) *The framework illustrated in Figure 18 is ultrarigid. The colors of the vertex orbits indicate the periodicity lattice of the pseudo-triangulation used in this construction. The pseudo-triangulation itself is a deformed 2-diamond framework with an additional edge orbit [9]. The edge orbit which turns the periodic pseudo-triangulation into an ultrarigid framework creates the rigid quadrilaterals shown in the picture.*

It is worth remarking that a finite fragment of the framework may be covered by a fragment resembling the one depicted in the figure. Such fragments, as finite linkages, are flexible and can accommodate small variations of the segments A_1A_2, A_2A_3 etc. However, larger assemblies of these stacked rows of rigid quadrilaterals will have smaller leeway for variation of deformation parameters. In the limit, as an infinite periodic framework, the structure is rigid.

In conclusion, we anticipate that our periodic version of Maxwell's Theorem and the expansive nature of periodic pseudo-triangulations will find, like their finite counterparts, further applications in discrete and computational geometry. In the larger scientific context, applications are expected in new materials and mechanism design.

An extended abstract of this work has appeared in [7].

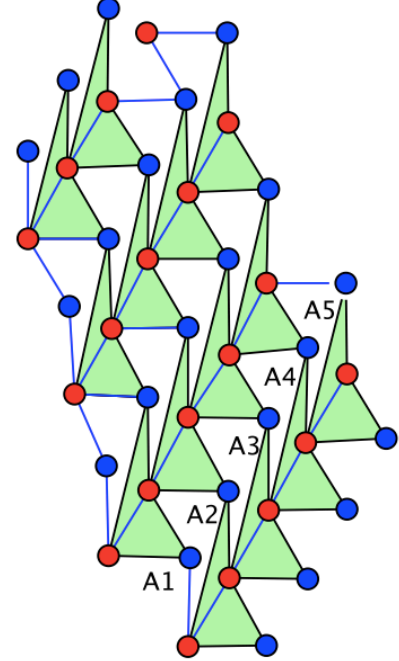


Figure 18: An ultrarigid framework obtained from a periodic pseudo-triangulation with an additional edge orbit. When ignoring periodicity, finite fragments are flexible.

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C. Borcea

Department of Mathematics, Rider University, Lawrenceville, NJ 08648, USA

I. Streinu

Department of Computer Science, Smith College, Northampton, MA 01063, USA