

# High-temperature stability of improved AIGaN/AIN/GaN HEMT with pre-gate metal treatment

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**Abstract:** This study proposes the investigation of using the  $(NH_4)_2S_x$  solution to form the AlGaN surface passivation on the AlGaN/GaN high electron mobility transistors (HEMTs). Both treatment schemes are implemented on separate pieces of the same HEMT wafer, including  $(NH_4)_2S_x$  pregate and post-gate metal treatments. Temperature-dependent characteristics of the HEMTs are also studied. Experimental results demonstrate that by the surface treatment prior to metal, the performance of the studied HEMTs can be improved, including thermal stability, dc and high-frequency characteristics. Furthermore, the interface state density (D<sub>it</sub>) of the studied HEMT is studied by the subthreshold slope method. To the best of our knowledge, this is the first report on comparison of AlGaN/AlN/GaN HEMTs with pre-gate and post-gate metal treatments.

**Keywords:** GaN, HEMT, passivation, sulfide treatment, interface state density, subthreshold slpoe

Classification: Electron devices, circuits and modules

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#### 1 Introduction

III-nitride high-electron-mobility transistors (HEMTs) are of significant interest for next-generation power devices [1, 2, 3, 4, 5]. Remarkable progress of both the AlGaN/GaN materials quality and device performance has been achieved. GaNbased Schottky-gate field-effect transistors suffer from the problem of high leakage current. Integration of a gate dielectric in metal-insulator-semiconductor field-effect transistors (MISFETs) has been demonstrated to offer remarkably decreased gate leakage current [3, 4, 5]. An alternative approach for reducing the leakage current is to passivate the surface of the devices. Through the surface passivation and Schottky gate metals engineering, the device characteristics and thermal stability can be improved. Additionally, passivation of heterojunction bipolar transistors (HBTs) [6] and heterostructure field-effect transistors (HFETs) [7, 8, 9, 10] has been investigated. However, the comparison of GaN-based HEMTs with surface treatments before and after gate metal deposition has not yet to be exploited. Consequently, the effects of (NH<sub>4</sub>)<sub>2</sub>S<sub>x</sub> treatments before or after gate metal deposition are evaluated with regard to the electrical characteristics of the HEMTs in this study.





There is a necessity for high-temperature electronics in microwave communication system. Transistors with high-temperature characteristics and excellent thermal stability are important for high frequency and high power applications. Many research groups have reported on the high-temperature performance of the GaAs-based HEMTs [7, 8, 9, 11]. Nevertheless, little attention has been devoted to investigating the thermal stability of GaN-based HEMTs. In this study, improved device characteristics and thermal stability of the HEMTs are obtained to perform surface treatment and passivation prior to the gate metal deposition.

### 2 Device structure and experiments

The epitaxial growth of the studied HEMT was performed in a metalorganic chemical-vapor deposition (MOCVD) system. The top layer was an  $Al_{0.25}Ga_{0.75}N$ , followed by a 1.5 nm AlN layer, and a 1.5  $\mu$ m GaN layer, and a buffer layer on a silicon substrate.

Mesa isolation was achieved by inductively coupled-plasma reactive ion etcher (ICP-RIE) with  $Ar/Cl_2$  plasma reactive ion etching, followed by source/drain ohmic metallization using Ti/Al/Au (10/100/50 nm) stack deposition and rapid thermal annealing in a N<sub>2</sub> atmosphere. Gate metal stack, 100 nm Ni followed by 50 nm Au, is then deposited by electron beam and lifted-off in acetone. Ni has high work function so that it can increase the Schottky barrier height to suppress the leakage current to obtain high breakdown voltage. Au was used for preventing oxidation of Ni.

The samples were soaked in the ammonia-sulfide solution  $((NH_4)_2S_x, 6\%)$  for 10 minutes at room temperature and then rinsed in deionized water followed by blown dry N<sub>2</sub> gas. The HEMTs used in this exploration were treated in two different methods. The first HEMT was passivated with  $(NH_4)_2S_x$  before the gate metal deposition. The second HEMT was passivated with  $(NH_4)_2S_x$  after gate metal deposition. The third control HEMT without passivation treatment was also studied. The gate length and source-drain spacing of the studied HEMTs are 1 and 5  $\mu$ m, respectively.

#### 3 Results and discussion

Many features are worth noting in comparing the current–voltage characteristics for the three studied HEMTs. Fig. 1 shows the two-terminal gate-drain characteristics of our studied HEMTs. We defined the values of leakage current density at the -20 V of gate-drain voltage. The relevant device parameters at 300 K are summarized in Table I. At 300 K, the I<sub>g</sub> value in the HEMT with pre-gate treatment is suppressed by over two orders of magnitude compared to that in the untreated HEMT.

The two-terminal gate-to-drain reverse breakdown voltage ( $BV_{GD}$ ) is measured at a reverse gate-to-drain current of 1 mA/mm. The values of  $BV_{GD}$  for the HEMT with pre-gate treatment are 109 V, 96 V, 87 V, 76 V at 300 K, 360 K, 420 K, 480 K, respectively. Consequently, the temperature coefficient of  $BV_{GD}$  ( $\partial BV_{GD}/\partial T$ ) of the HEMT with pre-gate treatment is -0.18 V/K. Temperature coefficients of the device characteristics of the studied HEMTs are tabulated in Table II. This pre-gate







Fig. 1. Two-terminal gate-drain characteristics of the (a) untreated HEMT, (b) HEMT with post-gate treatment, and (c) HEMT with pre-gate treatment at various temperatures.

metal treatment results in a large reduction in the gate leakage, improved breakdown voltages, and thermal stability of  $BV_{GD}$ .

Fig. 2 shows the temperature dependence of the extrinsic transconductance (g<sub>m</sub>) and drain current versus gate bias for the studied HEMTs between 300 and 480 K. The values of g<sub>m,max</sub> for the HEMT with pre-gate treatment are 136.6 mS/ mm, 124.1 mS/mm, 109.5 mS/mm, 95.2 mS/mm at 300 K, 360 K, 420 K, and 480 K, respectively. Therefore, the temperature coefficient of g<sub>m,max</sub> ( $\partial g_{m,max}/\partial T$ ) for the pre-gate treatment HEMT is -0.23 mS/mm-K. From Table II, the results demonstrate that the magnitude of the  $\partial g_{m,max}/\partial T$  value for the HEMTs with pre-gate treatment is smallest of the studied HEMTs. The gate voltage swing (GVS), defined as the gate voltage range where a 10% down from its maximum g<sub>m</sub>, is 2.5 V at 300 K for the HEMT with pre-gate treatment. Furthermore, the On/Off drain current ratio (I<sub>on</sub>/I<sub>off</sub>), determined as I<sub>on</sub> at V<sub>GS</sub> = 2 and I<sub>off</sub> at V<sub>GS</sub> = -6 V, is 10<sup>6</sup> for the untreated HEMT and  $2 \times 10^7$  for the HEMT with pre-gate treatment, at V<sub>DS</sub> = 7 V. From Table I, the On/Off drain current ratio of the HEMT with pre-gate treatment is largest due to its reduced gate leakage current [3, 12].

The values of subthreshold slope (SS) for the HEMT with pre-treatment are 132 mV/dec, 181 mV/dec, 195 mV/dec, 212 mV/dec at 300 K, 360 K, 420 K, and 480 K, respectively. The temperature coefficient of SS ( $\partial$ SS/ $\partial$ T) for the HEMT with pre-treatment is 0.44  $\frac{mV}{dec \cdot K}$ . From Table II, the HEMT with pre-gate treatment has the smallest SS and  $\partial$ SS/ $\partial$ T variation because it has the smallest leakage current in our studied HEMTs [3, 12].







**Fig. 2.** Drain current and extrinsic transconductance versus gate-tosource voltage of the (a) untreated HEMT, (b) HEMT with postgate treatment, (c) and HEMT with pre-gate treatment, at a fixed drain bias of 7 V.

The interface state density  $(D_{it})$  under the gate of the HEMTs is characterized by the subthreshold slope (SS) method. By analogy with metal-oxide-semiconductor field-effect transistors (MOSFETs) [3], the subthreshold slope for HEMTs is given by [13, 14, 15]





$$SS = \frac{kT}{q}\ln(10)(1+\varsigma)$$
(1)

where  $\varsigma$  is a non-ideality factor that is related to the interface trap density; *k* is the Boltzmann constant; *q* is the electronic charge, and T is the temperature (K). From Table I, the SS value of the HEMT with pre-gate treatment is lowest among of the HEMTs studied here. This suggests that the pre-gate treatment significantly reduces the interface trap density at the AlGaN surface. A further important point arising from Eq. (1) is that the SS value increases with the temperature. The theoretical relation is consistent with our above temperature-dependent SS values.

The values of threshold voltage (V<sub>th</sub>) for the HEMT with pre-treatment are -2.70 V, -2.77 V, -2.81 V, -2.87 V at 300 K, 360 K, 420 K, and 480 K, respectively. Therefore, the  $\partial V_{th}/\partial T$  value for the HEMT with pre-gate treatment is -0.94 V/K. From Table II, the  $\partial V_{th}/\partial T$  variation can be significantly suppressed due to the (NH<sub>4</sub>)<sub>2</sub>S<sub>x</sub> pre-gate metal treatment.



Fig. 3. Three-terminal off-state breakdown characteristics of the (a) untreated HEMT, (b) HEMT with post-gate treatment, and (c) HEMT with pre-gate treatment at various temperatures.

Fig. 3 shows the three-terminal off-state breakdown characteristics of our studied HEMTs. The criterion of the three-terminal off-state breakdown voltage (BV<sub>off</sub>) is set to be an off-state drain current of 1 mA/mm. The values of BV<sub>off</sub> for the HEMT with pre-gate treatment are 96.9 V, 92.2 V, 73.3 V, 60.3 V at 300 K, 360 K, 420 K, 480 K, respectively. Consequently, the temperature coefficient of BV<sub>off</sub> ( $\partial$ BV<sub>off</sub>/ $\partial$ T) of the HEMT with pre-gate treatment is -0.20 V/K. From Table II, (NH<sub>4</sub>)<sub>2</sub>S<sub>x</sub> pre-gate metal treatment can significantly increase BV<sub>off</sub> and





reduce the magnitude of  $\partial BV_{off}/\partial T$ . Table I and Table II list the summary of device performance data for our studied HEMT.

	Untreated HEMT	HEMT with post-gate treatment	HEMT with pre-gate treatment
Ig (mA/mm)	$3.74 \times 10^{-2}$	$1.52 \times 10^{-3}$	$2.2 \times 10^{-4}$
BV <sub>GD</sub> (V)	96	105	109
g <sub>m,max</sub> (mS/mm)	122	122.6	136.6
$I_{on}/I_{off}$	10 <sup>6</sup>	$8.75 \times 10^{6}$	$2 \times 10^{7}$
SS (mV/dec)	150	140	132
V <sub>th</sub> (V)	-2.82	-2.73	-2.7
GVS (V)	2.2	2.3	2.5
BV <sub>off</sub> (V)	90.9	94.0	96.9

Table I.	Summary	of the	studied	device	characteristics	at	300 K.
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**Table II.** Temperature coefficients of  $g_{m,max}$ , SS,  $V_{th}$ ,  $V_{off}$ , and  $V_{GD}$  for our studied HEMTs.

	Untreated HEMT	HEMT with post-gate treatment	HEMT with pre-gate treatment
$\frac{\partial \mathrm{BV}_{\mathrm{GD}}}{\partial T} \left( \frac{\mathrm{V}}{\mathrm{K}} \right)$	-0.27	-0.23	-0.18
$\frac{\partial g_{m,\max}}{\partial T} \left(\frac{\mathrm{mS}}{\mathrm{mm} \cdot \mathrm{K}}\right)$	-0.27	-0.25	-0.23
$\frac{\partial SS}{\partial T} \left( \frac{mV}{\text{dec} \cdot K} \right)$	1.15	0.63	0.44
$\frac{\partial \mathbf{V}_{\mathrm{th}}}{\partial T} \left( \frac{\mathbf{V}}{\mathbf{K}} \right)$	-1.5	-1.1	-0.94
$\frac{\partial \mathrm{BV}_{\mathrm{off}}}{\partial T} \left( \frac{\mathrm{V}}{\mathrm{K}} \right)$	-0.27	-0.22	-0.2

On-wafer RF measurements are done on our studied HEMTs in the frequency range of 0.2–25 GHz using an HP8510C network analyzer. Fig. 4 shows the smallsignal short-circuit current gain and maximum stable/available gain (MSG/MAG) measured from the studied HEMTs. The  $f_{\rm T}$  values of 8.2, 8.8, and 11.2 GHz are measured for the untreated HEMT, HEMT with post-gate treatment, and HEMT with pre-gate treatment, respectively. Furthermore, the  $f_{\rm max}$  values are 9, 10.8, and 14.8 GHz for the untreated HEMT, HEMT with post-gate treatment, and HEMT with pre-gate treatment, respectively. The experimental results demonstrate that the (NH<sub>4</sub>)<sub>2</sub>S<sub>x</sub> pre-gate treatment significantly improves the high-frequency characteristics.







Fig. 4. Forward current gain and maximum stable gain/maximum available gain (MSG/MAG) plotted versus frequency.

## 4 Conclusion

In summary, the beneficial influence of  $(NH_4)_2S_x$  treatment on AlGaN/AlN/GaN HEMTs is demonstrated. The surface treatment with  $(NH_4)_2S_x$  before the gate metal deposition greatly reduces the gate leakage current. Furthermore, the HEMT with  $(NH_4)_2S_x$  pre-gate metal treatment shows the improved device characteristics, high temperature operation capability, and relatively temperature-insensitive behaviors. These advantages suggest that the proposed sulfide treatment have high potential for the fabrication of AlGaN/GaN HEMTs.

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