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Modeling of transformer-rectifier sets for the energization of electrostatic precipitators using Modelica

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Abstract

Electrostatic precipitators (ESPs) are important parts of many industrial plants. They require high-voltage power supplies. In this paper, transformer/rectifier sets, a particular type of power supplies for the energization of ESPs, are presented and modeled using Modelica. The models have been validated with measurements from existing plants.

Keywords: *Modelica, power supply, electrostatic precipitator, ESP*

1 Introduction

Industrial plants—like coal-fired power plants and plants for the production of steel, pulp and paper, and cement—need to satisfy low and strict emission levels of pollutants in the emitted flue gases. One method to reduce the emission of solid pollutants suspended in gas streams is the use of electrostatic precipitators (ESPs) (Fig. 1). In ESPs, the particles of pollutants are electrically charged and pass through a strong electric field. The charged particles moving within the gas stream are therefore deflected towards collecting plates, to which they stick (Fig. 2). To create the ions that are required to charge the particles and to sustain the required strong electric field, high-voltage power supplies are required. ESPs are normally internally subdivided in electrically isolated sections, which are independently energized and controlled. Different topologies of power supplies which can be used to energize ESPs exist. One of them, also the most traditional, is called transformer/rectifier (T/R) set. T/R sets can be single phase or three phase (von Stackelberg, 2013). The aim of this paper is to model open-loop controlled, single- and three-phase T/R sets coupled to ESPs.

To understand the importance of the voltage shape and voltage level energizing ESPs, the concept of collecting efficiency η is introduced and defined as

$$\eta = \frac{\dot{m}_c}{\dot{m}_i} \quad (1)$$

where \dot{m}_c is the mass flow of collected particles and \dot{m}_i is the mass flow of incoming particles. The efficiency η depends on different geometrical parameters of the ESP—like the physical size and the shape of the electrodes and of the collecting plates—and of different physical parameters of the gas stream—like its density, temperature and velocity.



Figure 1. Example of electrostatic precipitator

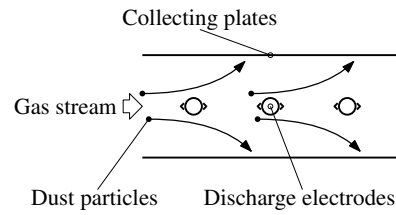


Figure 2. A schematic representation of a portion of an electrostatic precipitator

The influence of the geometrical and physical parameters can be expressed by

$$\eta = 1 - e^{-\frac{A}{Q}\omega} \quad (2)$$

where A is the total collecting area, Q is the flow rate of the gas stream and ω is called particle migration velocity. Under normal operating conditions, the particle migration velocity is proportional to the power P_c injected into the ESP and can be expressed as

$$\omega = k \frac{P_c}{A} \quad (3)$$

where k is a constant that depends on the physical parameters of the particular process (Parker, 1997).

The efficiency η can also be expressed more directly in electrical terms by

$$\eta = 1 - e^{-k_\eta \bar{v} \hat{v}} \quad (4)$$

where k_η is a constant (Bidoggia et al., 2018), and where \bar{v} and \hat{v} are respectively the mean and peak values of the ESP

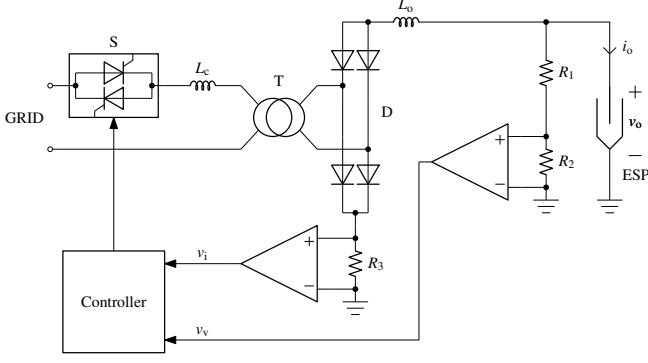


Figure 3. Schematic and block diagram of a single-phase T/R set connected to an electrostatic precipitator (ESP)

voltage. To maximize the collecting efficiency η of an ESP, the T/R-set controller acts on the firing angle of thyristors to keep the highest possible mean (\bar{v}) and peak (\hat{v}) voltage, typically at the limit of the dielectric breakdown voltage of the gas flowing through the ESP.

In this paper, after introducing the main components of single- and three-phase T/R sets (Sec. 2), the Modelica models which have been built will be described (Sec. 3). The simulation results and field measurements are presented and compared in Sec. 4. The conclusions are then presented in Sec. 5.

2 Energization of ESPs with T/R sets

In this section, the main components of single- and three-phase T/R sets are presented (Fig. 3 and 4). Because of the different output voltage they generate, their usage depends on the particular process of which the ESP is part.

All T/R sets are composed of a step-up transformer (T) and a full-wave rectifier (D). The positive connection of the rectifier is connected to ground to obtain a negative voltage across the ESP. The grid voltage is typically in the range 400 V to 690 V and the absolute value of the output voltage v_0 can typically be in the range 80 kV to 150 kV. The output voltage is measured by the voltage divider made of R_1 and R_2 . The average value of the output current i_0 is typically in the range 800 mA to 2000 mA and is measured by the shunt resistor R_0 . Because sparks can occur inside an ESP under normal operation, an external inductor (L_c) is inserted to limit the resulting overcurrent; typical per-unit values for L_c are in the range 30 % to 40 % (Parker, 1997). The voltage and current signals, respectively v_v and v_i are measured by the controller, which regulates the firing angle of the thyristors (S) to regulate the power injected to the ESP. On the output side, the inductor L_0 prevents high-frequency transients created by sparks from entering the T/R set. Because of the high voltage levels, the transformer T, the rectifier D, the resistor R_1 and the inductors L_0 and L_c are immersed in an oil tank. The oil is also used for cooling purposes.

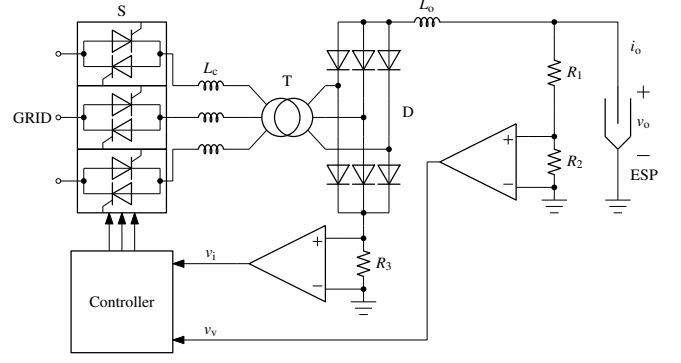


Figure 4. Schematic and block diagram of a three-phase T/R set connected to an electrostatic precipitator (ESP)

2.1 Single-phase T/R set

The output voltage waveform of single-phase T/R sets is characterized by a DC component with a superimposed relatively large ripple, with a frequency twice the grid frequency. This type of waveform is typically used in applications for which the resistivity of the particulate to filter falls in the medium-resistivity range ($1 \times 10^7 \Omega\text{m}$ to $5 \times 10^9 \Omega\text{m}$) (Bidoggia et al., 2018).

2.2 Three-phase T/R set

The output voltage waveform of three-phase T/R sets is characterized by a DC component with a negligible ripple, with a frequency six times the grid frequency. This type of waveform is typically used in applications for which the resistivity of the particulate to filter falls in the low-resistivity range ($< 1 \times 10^7 \Omega\text{m}$) (Bidoggia et al., 2018).

The transformer is typically connected in a configuration with delta connection at the primary side and star connection at the secondary side.

3 Modeling

The Modelica Standard Library and the OpenModelica Connection Editor (OMEdit) have been used to model both single- and three phase T/R sets. The availability of interfaces between different physical domains makes Modelica ideal for modeling multiphysical systems like ESPs. For this work, the following physical domains have been used: *electrical*, for the power electronics stage; *blocks*, for the open-loop control of the power electronics stage; *thermal*, for the calculation of the losses.

In this paper, the model of an ESP has been simplified and represented by an R-C circuit, where the values of resistance and capacitance were based on real installations. With the aim of setting the base for a model as representative as possible of real systems, the voltage divider and the current sensor have also been modeled. The voltage divider is designed to provide a voltage ratio $V_n/10\text{V}$, where V_n is the nominal output voltage of the T/R set. The current shunt is designed to provide a current/voltage ratio $I_n/1\text{V}$, where I_n is the nominal output current of the T/R set.

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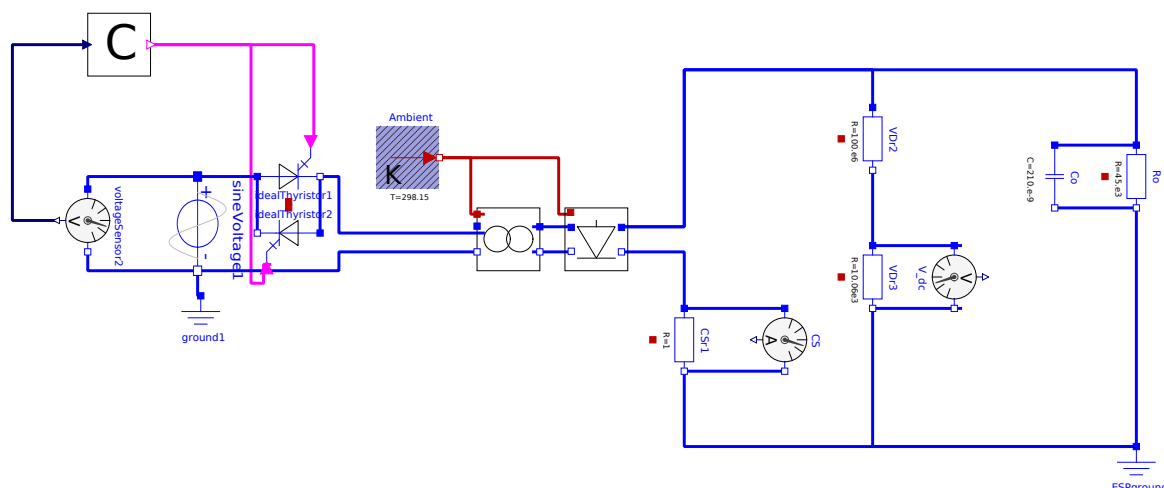


Table 1. Parameters for the models of the single- and three-phase T/R sets

	$R_{\{1 2 3\}}$ [m Ω]	$L_{\{1 2 3\}}$ [mH]	L_m [mH]	R_e [Ω]	n [—]	R_o [M Ω]	C_o [nF]
Single-phase	25	1.8	94	200	1/160	45	210
Three-phase	25	1.8	94	94	1/94	100	100

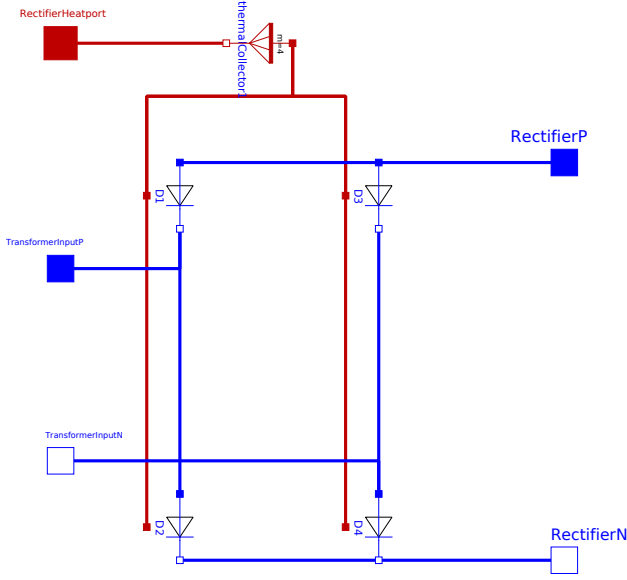


Figure 7. Submodel of the single-phase full-wave rectifier of a T/R set

the two resistances R_1 and R_e , and an ideal transformer with voltage ratio $n = n_1/n_2$.

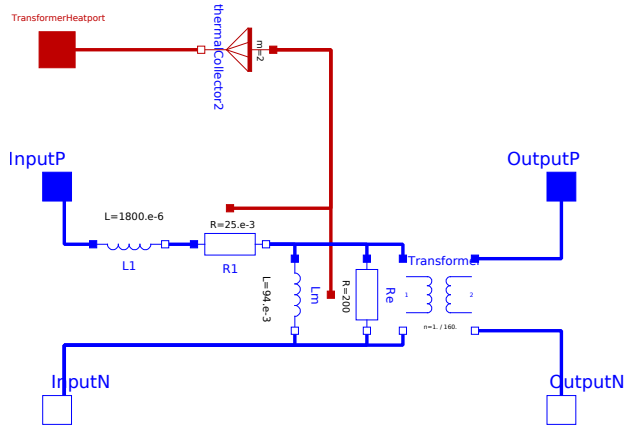


Figure 8. Submodel of the single-phase transformer of a T/R set

The inductance L_m represents the magnetizing inductance of the core of the transformer, while the inductance L_1 is defined as

$$L_1 = L_{1\sigma} + n^2 L_{2\sigma} + L_c + n^2 L_o \quad (5)$$

where $L_{1\sigma}$ is the leakage inductances of the primary side, $L_{2\sigma}$ is the leakage inductance of the secondary side, L_c is the inductance of the external short-circuit inductor and L_o is the inductance of the output inductor.

The resistance R_e represents the losses in the core of the transformer, while the resistance R_1 is defined as

$$R_1 = R_{1w} + n^2 R_{2w} + R_c \quad (6)$$

where R_{1w} is the resistance of the winding of the primary side, R_{2w} is the resistance of the winding of the secondary side, and R_c is the resistance of the external short-circuit inductor.

3.2 Three-phase T/R set

The derived model of a three-phase T/R set is shown in Fig. 9 with its submodels for the controller, the transformer and the rectifier (Tiller, 2017).

The controller model is the same as for a single-phase T/R set but replicated three times.

The choice of the model for the diodes is the same as for the single-phase T/R set. The submodel of the rectifier is shown in Fig. 10.

The submodel of the high voltage transformer is shown in Fig. 11. The inductances and resistances appearing in the model are defined similarly to the homologous ones in the model for the single-phase transformer.

4 Results

In this section, the results of the simulation of the models described in Sec. 3 and the results measured on existing plants are presented. Because of the different parameters and the different nominal values of the simulated and real systems, the results have been normalized so that the waveforms of different systems can be compared.

Fig. 12a presents the primary current for both a single- and a three-phase T/R sets connected to an ESP and measured on existing plants. Fig. 12b presents the simulated primary current for both a single- and three-phase T/R set connected to an ESP.

Fig. 12c presents the secondary current and secondary voltage for a single-phase T/R set connected to an ESP and measured on a real plant. Fig. 12d presents the simulated secondary current and secondary voltage for a single-phase T/R set connected to an ESP.

Fig. 12e presents the secondary current and secondary voltage for a three-phase T/R set connected to an ESP and

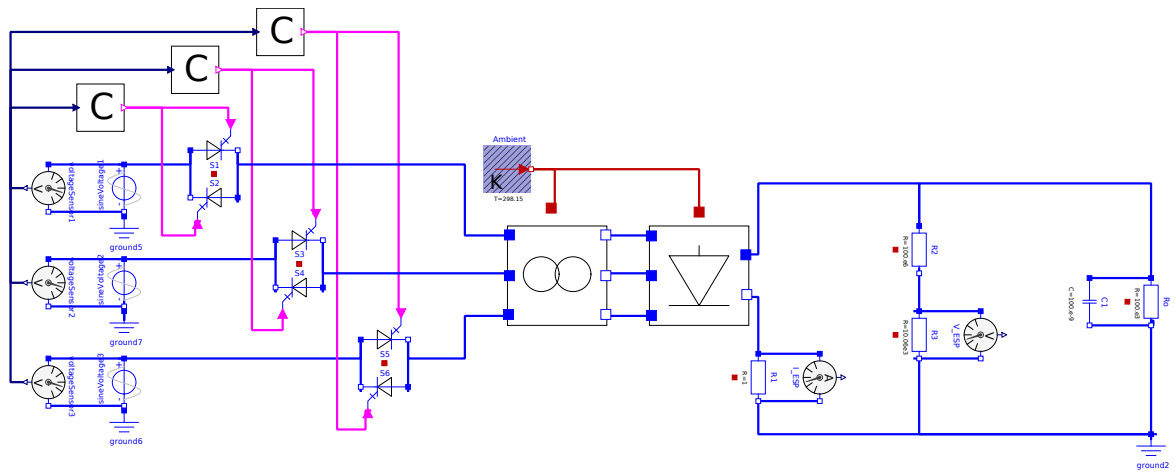


Figure 9. Modelica model of a three-phase T/R set connected to an electrostatic precipitator (ESP)

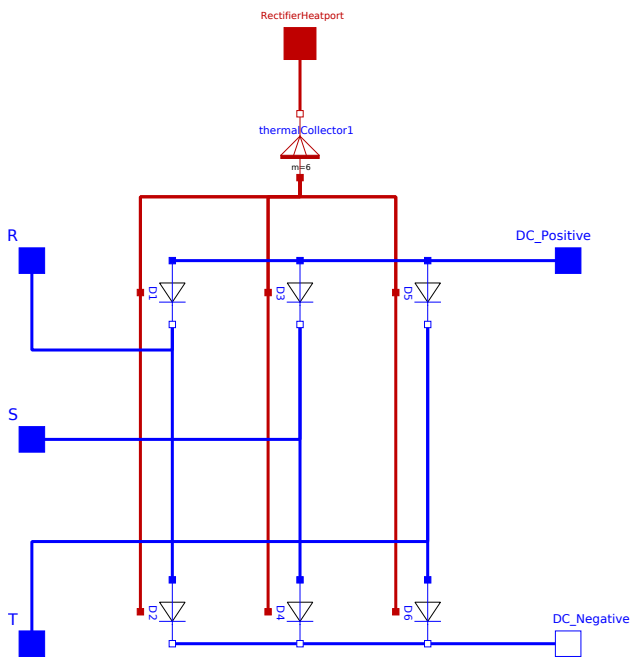


Figure 10. Submodel of the three-phase full-wave rectifier of a T/R set

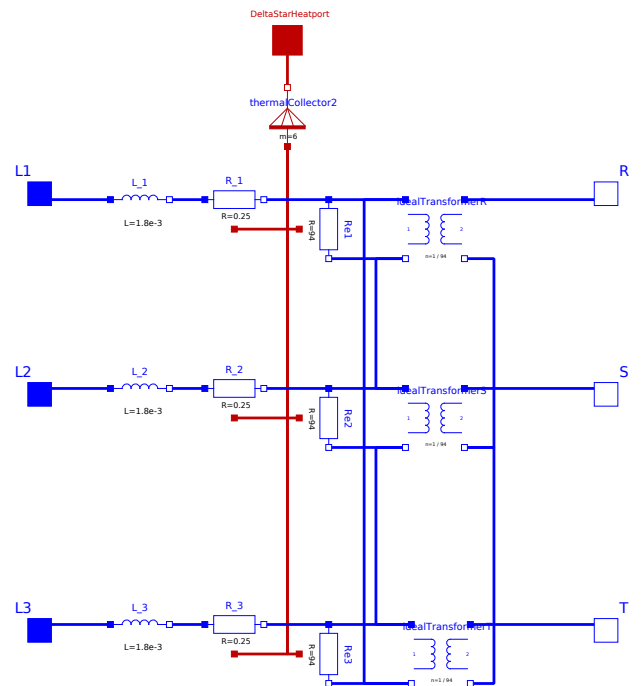


Figure 11. Submodel of the three-phase transformer of a T/R set

measured on a real plant. Fig. 12f presents the simulated secondary current and secondary voltage for a three-phase T/R set connected to an ESP. The amplitude of the voltage ripple is significantly smaller than in the case of the single-phase T/R set.

For all waveforms, the shape of the simulated waveforms is in agreement with the shape of the measured waveforms. The minor differences—in the primary current and in the secondary voltage and current—between the simulated and measured results are mostly related to the nature itself of ESPs. These are loads whose parameters are constantly changing as a function of the physical parameters of the gas streams that they are filtering. Thus, also modeling the ESP itself will be of paramount importance, especially in relationship with a closed-loop control system. Other minor differences—like for example in the primary current—are related to other electrical phenomena, which have not been taken into consideration yet, like the switching transients of the thyristors.

5 Conclusions

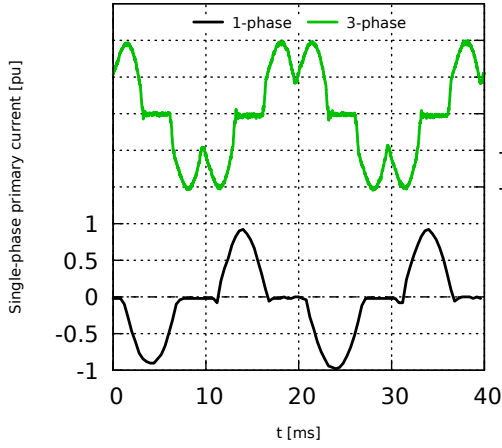
Electrostatic precipitators (ESPs) are important parts of many industrial plants and they require high-voltage power supplies. The goal of the project to which this work belongs is to model a complete ESP system. In this paper, a particular type of power supplies for the energization of ESPs—transformer/rectifier sets—has been presented and simple models have been derived using Modelica. The models have been validated with measurements from existing plants. However, further work will be required, like the derivation of the models of the ESP, of closed-loop controllers and of other topologies of power supplies. The derivation of a complete thermal model for these power supplies is planned.

6 Acknowledgment

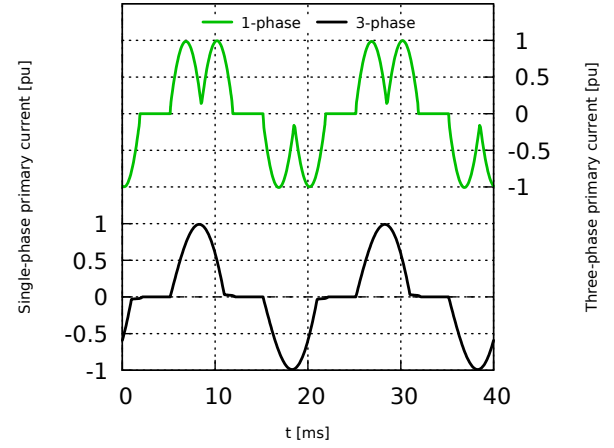
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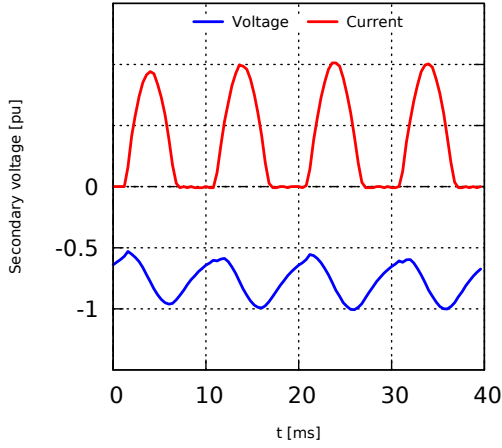
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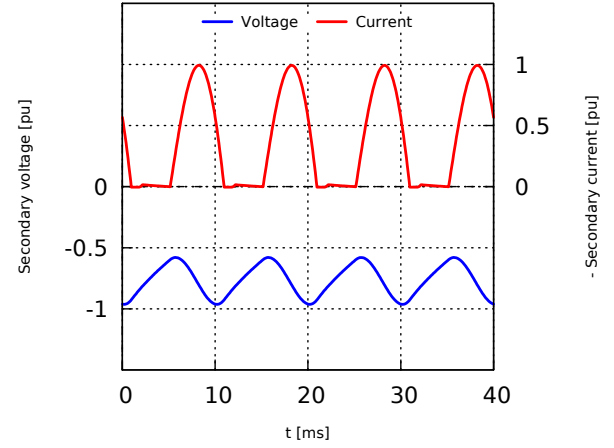
(a) Measured primary current for a single-phase (base current $I_b = 170$ A) and a three-phase (base current $I_b = 160$ A) T/R set



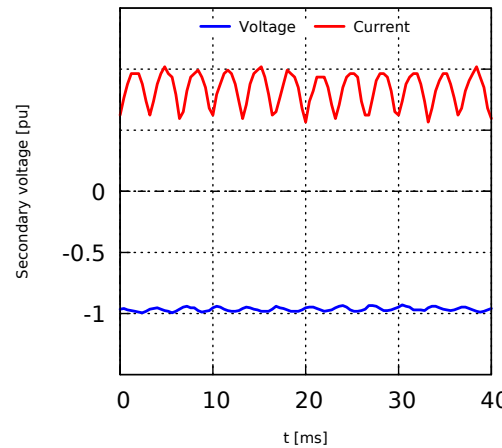
(b) Simulated primary current for a single-phase (base current $I_b = 150$ A) and a three-phase (base current $I_b = 85$ A) T/R set



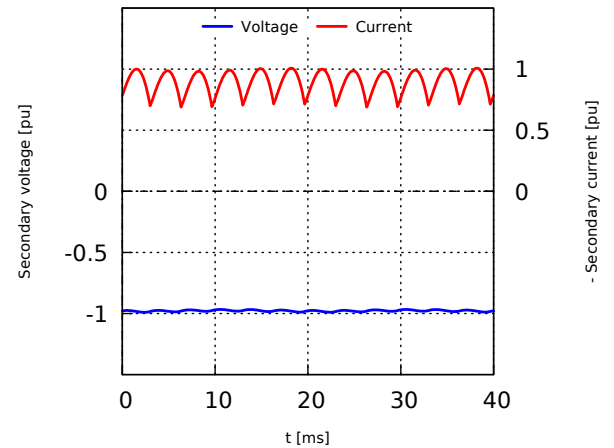
(c) Measured secondary voltage (base voltage $U_b = 76$ kV) and current (base current $I_b = 1800$ mA) for a single-phase T/R set



(d) Simulated secondary voltage (base voltage $U_b = 51$ kV) and current (base current $I_b = 2400$ mA) for a single-phase T/R set



(e) Measured secondary voltage (base voltage $U_b = 76$ kV) and current (base current $I_b = 1200$ mA) for a three-phase T/R set



(f) Simulated secondary voltage (base voltage $U_b = 51$ kV) and current (base current $I_b = 800$ mA) for a three-phase T/R set

Figure 12. Comparison between the main waveforms of measurements and simulation results for single-phase and three-phase T/R sets